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LANDSAT-1 AND LANDSAT-2 FLIGHT EVALUATION REPORT 23 OCTOBER 1975 TO 23 JANUARY 1976

Prepared By
GE LANDSAT OPERATIONS CONTROL CENTER

For

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Goddard Space Flight Center
Greenbelt, Maryland 20771





(Not Exts)

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Contract NAS5-21808

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INTRODUCTION

This is the fifteenth report in a continuing series of documents issued at launch, and thereafter quarterly, to present flight performance analysis of the Landsat-1 Spacecraft. Previously issued documents are:

72SD4255	ERTS-1 Launch and Flight Activation Evaluation Report 23 to 26 July 1972	18 October 1972
72SD4262	ERTS-1 Flight Evaluation Report 23 July 1972 to 23 October 1972	28 November 1972
72SD4224	ERTS-1 Flight Evaluation Report 23 October 1972 to 23 January 1973	27 February 1973
73SD4249	ERTS-1 Flight Evaluation Report 23 January 1973 to 23 April 1973	29 May 1973
73SD4260	ERTS-1 Flight Evaluation Report 23 April 1973 to 23 July 1973	10 August 1973
73SD4274	ERTS-1 Flight Evaluation Report 23 July 1973 to October 1973	28 November 1973
74SD4205	ERTS-1 Flight Evaluation Report 23 October 1973 to 23 January 1974	26 February 1974
74SD4217	ERTS-1 Flight Evaluation Report 23 January 1974 to 23 April 1974	18 May 1974
74SD4236	ERTS-1 Flight Evaluation Report 23 April 1974 to 23 July 1974	15 August 1974
74SD4255	ERTS-1 Flight Evaluation Report 23 July 1974 to 23 October 1974 .	31 December 1974
75SDS4222	Landsat-1 Flight Evaluation Report 23 October 1974 to 23 January 1975	30 April 1975
75SDS4228	Landsat-1 and Landsat-2 Flight Evaluation Report 23 January 1975 to 23 April 1975	15 August 1975
75SDS4255	Landsat-1 and Landsat-2 Flight Evaluation Report 23 April 1975 to 23 July 1975	10 October 1975
758DS4266	Landsat-1 and Landsat-2 Flight Evaluation Report 23 July 1975 to 23 October 1975	1 December 1975

This report contains analysis of performance for Orbits 16550 to 17830 for Landsat-1.

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SECTION 1 SUMMARY - LANDSAT-1 OPERATIONS

SUMMARY LANDSAT-1 OPERATIONS

Landsat-1 continues to perform its mission nominally.

The Landsat-1 spacecraft was launched from the Western Test Range on 23 July 1972, at 18:08:06.508Z. The launch and orbital injection phase of the space flight was nominal and deployment of the spacecraft followed predictions. Orbital operations of the spacecraft and payload subsystems were satisfactory through Orbit 147, after which an internal short circuit disabled one of the Wideband Video Tape Recorders (WBVTR-2). Operations resumed until Orbit 196, when the Return Beam Vidicon failed to respond when commanded off. The RBV was commanded off via alternate commands. Landsat-1 continued to perform its imaging mission with the Multispectral Scanner and the remaining Wideband Video Tape Recorder providing image data. The remaining Wideband Tape Recorder experienced four suspensions of operation, the last being in Orbit 9881 on 2 July 1974, and has not been used operationally since. In Orbit 4396, an integrated circuit chip in the TMP failed, disabling four TLM functions. COMSTOR "B" has an intermittent problem with cell 12, which is not being used operationally. The "B" section of the USB with full power output of 1,5 watts was substituted for the "A" section in Orbit 10068 because of excessive decline of transmitter power. The pitch flywheel stopped for 2 minutes in Orbit 8040; and for 8 hours, 2 minutes m Orbits 11125 to 11130. It has been kept close to zero speed ever since, using pitch-bias control. The RMP was switched from B to A in Orbit 11257 as a precautionary measure after RMP B began showing current variations. The DCS subsystem was turned off after Orbit 12690 and the function assumed by DCS in Landsat-2. Narrow Band Recorder 2 became noisy and was turned off in Orbit 13015. Operation of NBR 2 resumed in Orbit 14116 until failure in Orbit 15253, when its operation was terminated. Battery 6 was turned off between Orbits 13346 and 14100 due to electrical characteristics causing high temperatures. Between Orbits 14780 and 15467, Battery 6 was turned off again due to high temperature. Because high current transient occurred at Battery 6 turn on in Orbit 15467 the battery turn-on command is temporarily suspended from use. Battery 8 was turned off in Orbit 15588 due to electrical characteristics causing high temperature and will not be returned to service because of the battery "ON" command problem. The pitch flywheel stopped again for 45 minutes in Orbit 15309 and 3 minutes in Orbit 15312. Pitch flywheel motor driver duty cycle remained high from Orbit 15191 to Orbit 15393 when it returned to normal. MSS operation was suspended during the pitch flywheel anomaly between Orbit 15309 and 15393. See Table 1-1 for a summary of payload m-orbit operation.

Table 1-1. In-Orbit Payload System Performance Launch Thru Orbit 17804 (1/21/76) Landsat-1

	<u> </u>		
RBV	Total Scenes Imaged		1690
	AVG. Scenes/Day		139
	Total Area Imaged (millions of sq. mi.)		14.7
	ON TIME (hr.)		14.0
	ON/OFF Cycles		91
	% Real Time Images		57
	% Recorded Images		43
MSS	Total Scenes Images		206,093
	AVG. Scenes/Day		176
	Total Area Imaged		1,797
	(millions of sq. n. mi.)		
	ON TIME (hr.)		2,172
	ON/OFF Cycles		16,090 78
	% Real Time Images % Recorded Images		22
	_		
DCS	Messages at OCC		1, 152, 045
	Non-Perfect MSGS		90,691
	Max. DCP's ACTIVE/DAY		114 44
	Users		181
	Avg. MSG/ACTIVE Orbit ON TIME (hr.)		21,820.2
	` .		•
WPA-1	% Real Time Mode		55 45
	% Playback Mode		45 31.9
	ON TIME (hr.) ON/OFF Cycles		312
	•		
WPA-2	% Real Time Mode		78.
	% P/B Mode		22
	ON TIME (hr.) ON/OFF Cycles		2,106 13,802
WBVTR-1	% Record Mode		38
	% Playback Mode		41
	% Rewind Mode		20 1
	% Standby Mode Minor Frame Sync		Ŧ
	Error Count in P/B	Failed Orb.	9881
	Time Head-Tape Contact	a gardu Or Ne	732.8
	(hr.)		
	Cycles Head-Tape Contact		11,954
	ON TIME (hr.)		927.6
WBVTR-2	% Record Mode		38
	% Playback Mode		41
]	% Rewind Mode		20
	% Standby Mode	Failed Orb.	1 148
1	MFSE Count in P/B Time Head-Tape Contact	railed Orb.	5, 1
	(hr.)		0, ±
	Cycles Head-Tape Contact		44
	ON TIME (hr.)		6.5
	· · ·		

ORBITAL PARAMETERS

ORBITAL PARAMETERS

Landsat-1 launch and injection was satisfactory. After several 18-day ground trace repeat cycles, orbit maintenance burns were made in Orbits 938, 2416, 6390, 7826, 11367, 11464, 13611 and 14365. An unplanned orbit change occurred due to freon gas expended during the pitch flywheel emergency (Orbits 11125 and 11130).

No orbit maintenance burn occurred during this report period.

The orbital parameters are given in Table 2-1. Figure 2-1 shows the longitude error as a function of time and orbit maintenance burns. The longitude error has been maintained within ± 10 nm in the east-west direction at the equator as planned. Figure 2-2 shows the change of sun time at the descending node. Appendix B gives ground trace repeat cycle predictions.

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Table 2-1. Landsat 1 Brouwer Mean Orbital Parameters

Element	Apogee (km)	Perigee (km)	Inclination (Deg.)	Semi Major Axis (km)	Eccentricity	Two Body Period (Min)	Nodal Period (Min)	Argument of Perigee (Deg)	Right Ascension (Deg)	Mean Anomaly (Deg)
25 Oct 1972	917.3	898.1	99.103	7285.850	0.00132	103.152	103.268	93.721	1.060	86.484
25 Jan 1973	922.3	893.1	99.090	7285.865	0.00200	103.153	103.268	133.693	91.805	52.797
25 Apr 1973	911.056	888.763	99,073	7285.767	0.00073	103.151	103.267	168.857	181.41 1	11.098
25 Jul 1973	914 341	900.810	99.068	7285.741	0.00093	103.150	103.266	95.602	268.944	84.301
25 Oct 1973	922.913	893.229	99.056	7285.786	0.00198	103.151	103.266	65.071	0.291	301.002
25 Jan 1974	915.873	899.111	99.041	7285.657	0.00115	103 148	103.264	160.866	88.606	19.049
24 Apr 1974	920.090	912.672	99.023	7285.691	0.000802	103.149	103.265	117.631	176.743	62.319
23 Jul 1974	922.363	892.629	99.017	7285.661	0.002041	103.148	103.264	109.225	269.779	70.540
23 Oct 1974	918.657	896.316	99.004	7285.652	0.00153	103.148	103.264	150.750	354.743	29.110
24 Jan 1975	914.18	900.67	98.990	7285.590	0.000928	103.147	103.262	278.848	85. 403	261 138
24 Apr 1975	914.74	900.05	98.972	7285.559	0.001008	103 146	103.262	37.047	173, 043	142.764
25 Jul 1975	915.12	899.63	98.964	7285.541	0.001063	103.145	103.261	138.138	262.528	41.661
23 Oct 1975	914.19	900.54	98.951	7285.531	0.000937	103.145	103.261	250.370	349.952	289.612
24 Jan 1976	914.39	900.32	98.936	7285.523	0.000966	103.145	103.261	2.826	80.147	177.049

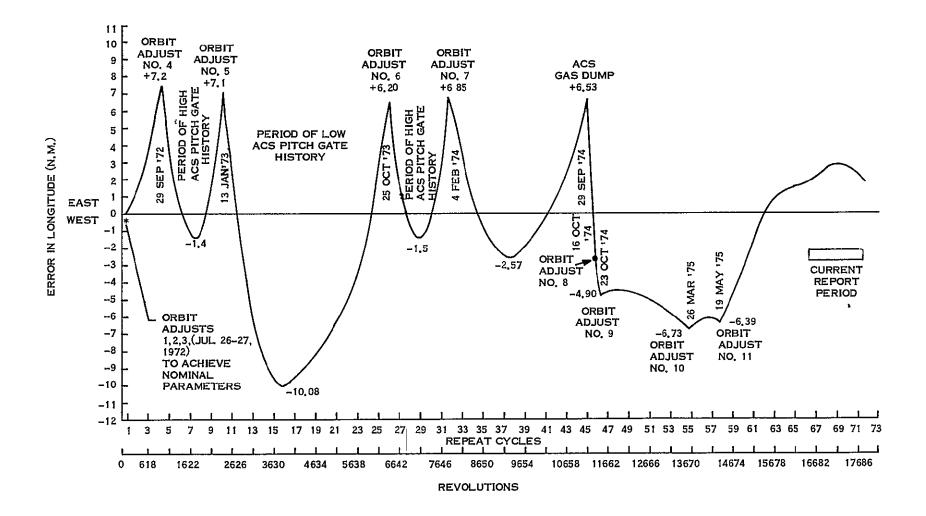


Figure 2-1. Effect of Orbit Adjusts on Landsat-1 Ground Track

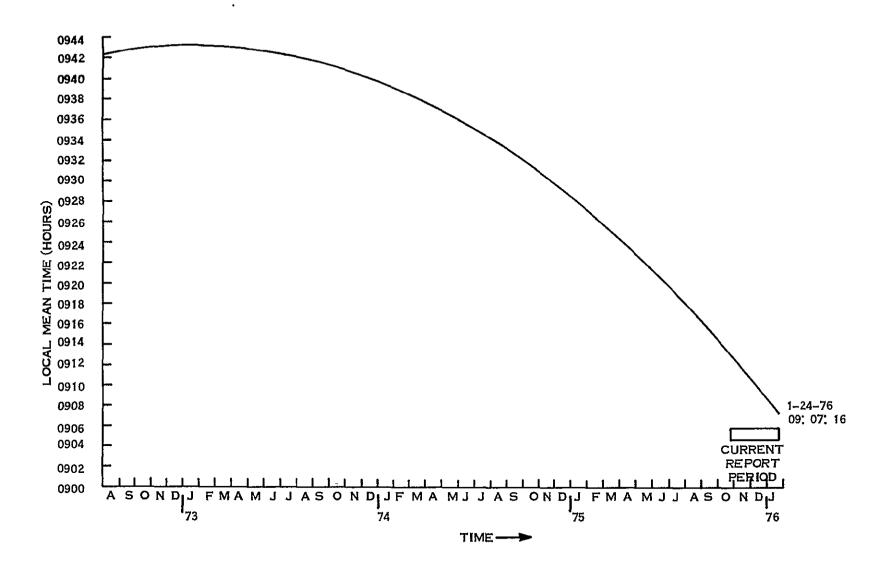


Figure 2-2. Local Mean Time of Descending Node

POWER SUBSYSTEM (PWR)

POWER SUBSYSTEM (PWR)

The solar array continued to provide excess energy for the payload and spacecraft load throughout this report period. Compensation loads and auxiliary loads dissipated the excess power above the battery and load requirements using Landsat-1 power management procedures. Solar array degradation was -28.3% at the end of 42 months in orbit. The power subsystem is predicted to have adequate power through 1976 for the present Landsat-1 payload configuration, and may extend to 1977 depending on the electrochemical degradation of the battery packs and the effect of increasing sun angle on array tracking (see Section 4 also).

A plot of measured and predicted midday solar array current is shown in Figure 3-1. Figure 3-2 shows actual and predicted midday solar array degradation. Figure 3-3 shows actual sun angles to the spacecraft and solar panels. Figure 3-4 is a prediction of the variation of sun angle through 1977 for Landsat-1 and 2.

It is noted in Figure 3-1 that the high noon solar array current is slightly lower than predicted. This is due to slightly different solar panel sun angles and operating point high noon solar array degradation than initially predicted.

During Orbits 16702 and 16703 (3 November 1975) Landsat-1 passed through the partial solar eclipse over the Southern Hemisphere. Real-time adjustments to the auxiliary loads were made to compensate for the loss in array energy.

Battery 8 switched off in Orbit 15588 (15 August 1975), remained off-line throughout this report period. The battery probably discharged to zero volts around 1 December 1975, though telemetry verification is impossible because the sensor threshold is 19.33 volts.

Beginning in Orbit 15794, (30 August 1975) an adjustment to the power management program has kept the batteries slightly undercharged to keep them within acceptable temperature limits.

Temperature spread between batteries has ranged from 7.5 to 12.5°C during the current report period, battery 5 in bay 14 having the highest temperature. The wider range and higher peak in temperature was caused by increased sun intensity and sun angle as well as a possible malfunction of the thermal shutter for bay 14. (See Section 11 also.) Battery packs averaged a typical 8.0 to 9.3% Depths of Discharge (DOD) with fairly good charge and discharge characteristics for individual batteries.

The power system electronics performed well in this report period with all voltages stable. Table 3-1 shows major power subsystem parameters and Table 3-2 shows power subsystem telemetry for selected orbits. Some parameters in Table 3-2 may be slightly different from Table 3-1, because Table 3-1 uses a power management time span (night followed by a day); whereas, the time span used in Table 3-2 is the playback period for the NBR. The Shunt Limiter has not operated since Orbit 3 because the unregulated voltage has been held below cut-in voltage by power management.

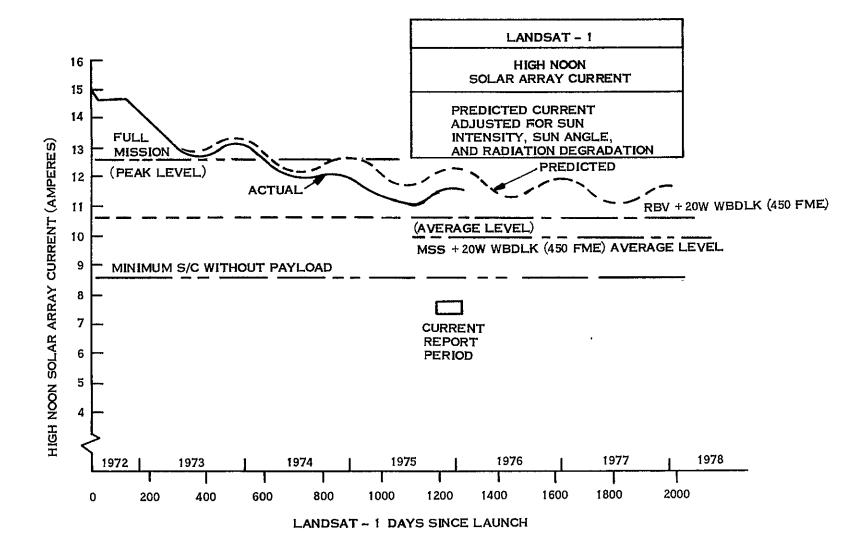


Figure 3-1. Midday Solar Array Current

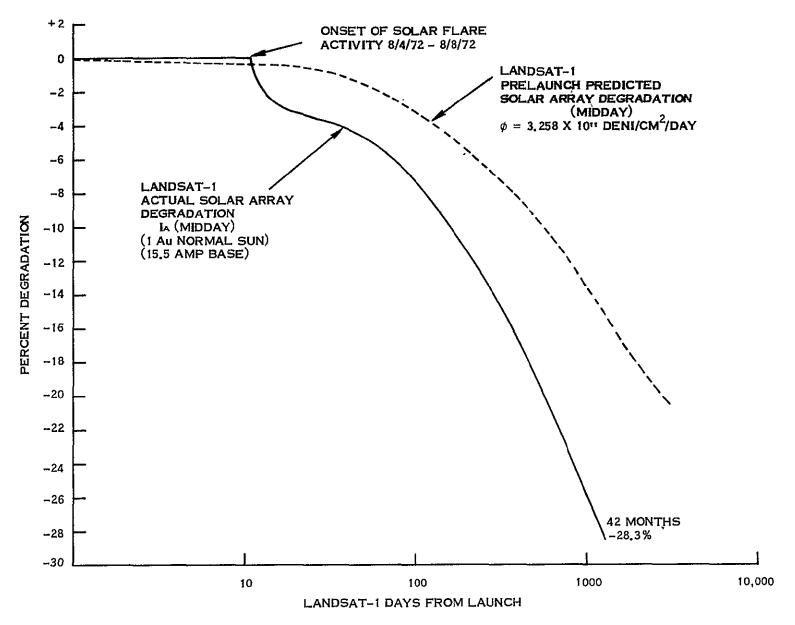


Figure 3-2. $I_{\mbox{\scriptsize A}}$ (Midday) Degradation vs. Days

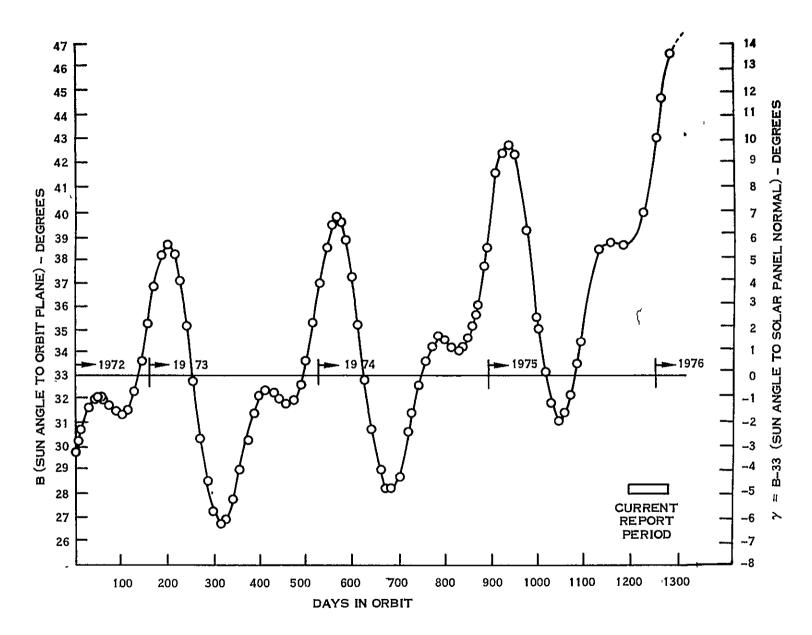


Figure 3-3. Actual β and γ (Paddle) Sun Angles, Landsat-1

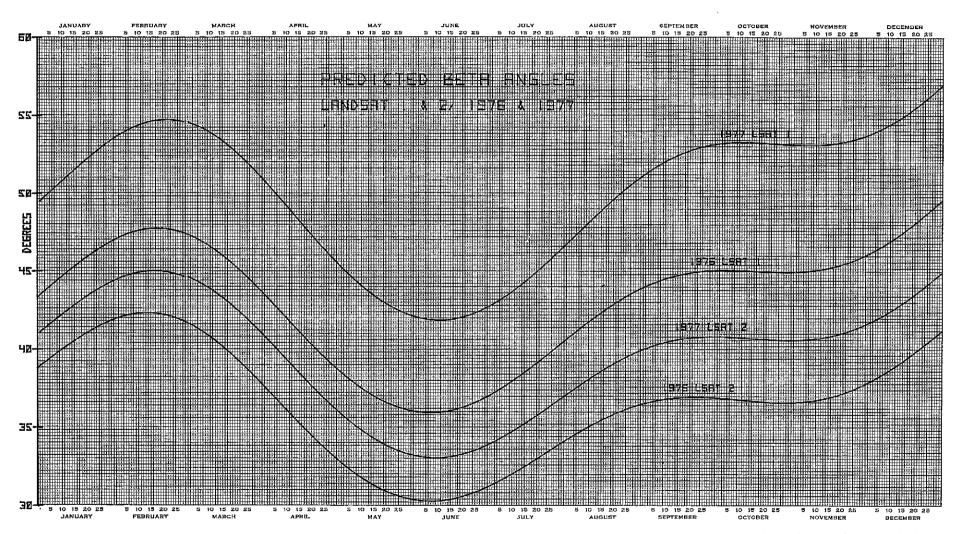


Figure 3-4. Predicted Beta Angles, Landsat 1 & 2, 1976 & 1977

Table 3-1. Landsat-1 Major Power Subsystem Parameters

10178

5098

26

ORBIT NO.

15254

17003

17393

17853

Battery 6 turned off in Orbit 14780 was returned to service in Orbit 15467.

Battery was turned off in Orbit 15588 and remained off through the end of this report period.

⁺ Average of batteries on-line.

				ma = :	1615-	Orbits	10001	77954	1205
Function	Description	Unit	26	5089	10182	15254	17004	17894	17854
600I	BATT 1 DISC	AMP	0.94	0,81	0.81	0.91	0.85	0.80	0.75
6002	2		0.95	*	*	*	*	*	*
6003	3		0,84	0.78	0.80	0,86	0.79	0.79	0.70
6004	4		0,93	0,86	0.86	0,92	0.86	0.83	0.79
6005	5	<u> </u>	0.92	0.82	0, 62	0,87	0.79	0.77	0.81
6006	6++		0.91	0.78	0,72	0.00	0,88	0.87	0,82
6007	7	<u> </u>	0,94	0.82	0,80	0,85	0,79	0,77	0.76
6008	8**	<u> </u>	0.91	0.77	0,78	0.80	0.00	0,00	0.0
6011	BATT 1 CHG	AMP	0,58	0.58	0,69	0, 52	0,41	0,34	0.3
6012	2	<u> </u>	0.57	*	4	*	*	*	*
6013	8	<u> </u>	0.50	0,48	0,60	0.46	0,37	0, 32	0.3
6014	4		0.54	0.51	0,60	0.48	0.89	0, 33	0.3
6015	5		0.54	0,50	0,58	0.48	0,38	0, 32	0.3
6016	611		0.57	0.52	0,56	0.00	0,45	0, 38	0.4
6017	7		0.55	0,58	0,60	0.46	0.36	0, 31	0,3
6018	81*	<u> </u>	0.55	0,52	0,58	0.49	0.00	0,00	0.0
6021	BATT 1 VOLT	VDC	30.87	31,24	31,64	31,62	31.08	30, 81	80,8
6022	2	<u> </u>	30.87	31, 25	31,66	31,62	31.07	30.80	30.8
6023	3		30.87	31,25	31,66	31,62	31.07	30.79	80,8
6024	4	L	30,90	81.28	31.70	31,65	31,10	30.83	30.8
6025	- 6		30.95	31, 33	31,75	31,71	31.16	30,90	30,9
6026	6 ++	ļ	30.86	81.24	31,65	28, 18	31.06	30.79	30,6
6027	7	<u> </u>	30.89	31,27	31,68	31,64	31,10	30.83	30,8
6028	8**		30,89	31, 27	31,68	31, 63	21,81	-	<u> </u>
6031	BATT I TEMP	DGC	21,17	24.48	26.09	28,02	22,17	22,60	23,2
6032	2	<u> </u>	18.80	21, 29	22,81	19,28	18,36	18,43	18,4
6033	8	ļ	18,76	20.17	21.26	18,76	17.35	17, 38	17.5
6034	4		21.57	23, 04	23.93	22,69	22,24	22,47	22.7
6035	5	<u> </u>	21,84	23, 77	24.78	23,64	25, 22	26,74	30,6
6036	6++		21,24	24,27	25.78	22.08	24.56	25,85	29.0
6037	7	<u> </u>	21,43	24.88	26,09	23,67	24,06	25, 15	27.4
6038	8**	<u> </u>	21,86	25, 02	26, 21	24.51	23,13	23, 91	25,1
6040	RT PAD TEMP	DGC	25.82	27, 22	27,16	27,29	32,08	33,45	33.3
6041	R PAD V N	VDC	33.40	38.85	84.36	34, 18	33,09	32, 56	31,7
6042	R PAD V M	VDC	33,29	33.50	33,60	82,92	31,85	31,46	31,(
6044	LT PAD TEMP	DGC	14,14	16,61	19,11	19.84	25, 57	27, 30	28,9
6045	L PAD V F	VDC	33,69	34.16	34.67	34,63	33,82	38, 50	88,4
6046	L PAD V G	VDC	33,68	34, 19	34.72	84.68	38,87	38, 54	35.4
6050	S/C UR BUS V	VDC	31,24	31.68	32.60	32,07	31,52	31, 22	81.2
6051	S/C RG BUS V	VDC	24.54	24, 55	24.55	24.54	24.54	24,54	24.0
6052	AUX REG A V	VDC	23.41	23.48	23,47	23.49	28,50	23,49	28,4
6053	AUX REG B V	VDC	23.50	23,50	23.50	23.50	28.50	23, 50	28.5
6054	SOLAR I	AMP	14.87	12,69	11.60	10.83	11,14	11, 10	10.7
6055+	s/C RG BUS I	AMP	7,11	6, 27	6.80	5.63	5.04	5.03	5.0
6056+	S/C RG BUS I	AMP	7,11	6, 27	6.79	5.62	5.03	5, 01	5.0
6058	PC MOD T 1	DGC	21.82	22, 23	23.22	20.63	19.72	19.70	19.7
6059	PC MOD T 2	DGC	21.68	22.53	23.00	21.17	20.39	20, 39	20.5
6070	P/L RG BUS V	VDC	24,66	24,68	24,68	24,68	24,67	24,66	24,6
6071	P/LUR BUS V	VDC	31.08	31, 53	31,92	31, 92	31.36	31 06	31. (
6072+	P/LRG BUSI	AMP	0.57	0,56	0,36	0.36	0.37	0.37	0.3
6073	PAUXAV	VDC	23.51	23.51	23.50	23.50	23.50	23, 50	23.5
6074	P AUX B V	VDC	23.51	23, 51	23.50	23,50	23.50	23,50	23, 6
6075	PR MOD T 1	DGC	21.50	23.13	23.62	21.44	20.92	20.92	21.1
6076	PR MOD T 2	DGC	20.34	21,45	21.84	19.88	19.59	19.59	19.8
6079	FUSE BLOW V	VDC	24.56	24.57	-24.60	24.59	24,58	24,59	24.5
6080	SHUNT 1 I	AMP	0.00	0.00	0.00	0.00	0,00	0.00	0.0
6081	SHUNT 2 I	AMP	0,00	0.00	0.00	0.00	0.00	0.00	0, (
6082	SHUNT 3 I	AMP	0.00	0,00	0.00	0,00	0,00	0,00	0.0
6083	SHUNT 4 I	AMP	0.00	0.00	0.00	0.00	0.00	0, 00	0.1
6084	SHUNT 5 I	AMP	0-00,	0.00	0.00	0,00	0,00	0, 00	0.0
6085	SHUNT 6 I	AMP	0.00	0,00	0.00	0.00	0.00	0.00	0.0
6086	SHUNT 7 I	AMP	0,00	0,00	0.00	0.00	0.00	0,00	0.0
6087	SHUNT 8 I	AMP	0.00	0.00	0,00	0.00	0.00	0,00	0,0
6100	P/L RG BUS I	AMP	0.58	0.56	0.36	0.36	0.37	0.37	0.2

^{*}Function 6002, 6012, missing data resulted from disabled telemetry resulting from IC chip failure which affected charge current directly and discharge current indirectly.

LS-1

⁺FUNC 6055, 6056, 6072 data is derived from Pseudo FUNC 6155, 6156, 6172 used after charge to Mode 11.

⁺⁺Battery 6 turned off in Orbit 14780 was returned to sorvice in Orbit 15467.

^{**}Battery 8 was turned off in Orbit 15588 and remained off through the end of this report period.

ATTITUDE: CONTROL SYSTEM (ACS)

ATTITUDE CONTROL SYSTEM (ACS)

Landsat-1's ACS system accurately maintained the spacecraft's attitude even though the Pitch Flywheel was malfunctioning during the first days of this report period.

With the exception of Orbits 16557 (24 October 1975) through 16613 (28 October 1975), the Pitch Flywheel performed normally and its duty cycle averaged less than 7%. During Orbits 16557 through 16613, the Pitch Flywheel's duty cycle rose about 45% and several short term 100% duty cycles resulted in momentary Pitch Flywheel stoppages. The condition cleared itself without intervention in Orbit 16614 (28 October 1975); MSS activities were not affected during this interval.

Use of pneumatics to stabilize the spacecraft during the Pitch Flywheel anomaly was not required.

Due to the Pitch Flywheel's malfunction history, the ACS system is commanded into the Normal mode only during the six consecutive daily orbits of MSS activity. During the remaining daily orbits of non-MSS activity, the ACS system is commanded into the Roll Diff Tach High Gain mode to unload Roll momentum and conserve freon.

Positive 0.60 Pitch Position Bias is employed to limit the Pitch Wheel's speed between -10 RPM and -100 RPM and to prevent it from "siezing" with an excess of stored momentum.

Since continuous NBTR coverage is no longer available to account for all pneumatic gating, Figure 4-1 was prepared to approximate average gating frequency. The approximate slope of the curve in Figure 4-1 indicates a gating frequency of approximately 4, -Roll gates per day. Figure 4-1 also shows that the freon pressure dropped the fastest between Orbits 17000 (24 November '75) and 17160 (6 December '75). These orbits occurred during Landsat 1's seasons of maximum gating activity, and the pressure drop this period is consistent with Landsat 1's seasonal gating history.

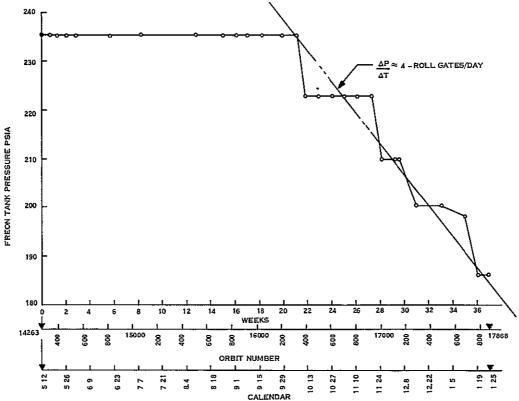


Figure 4-1. Landsat-1 Freon History, Orbits 14263 (5-12-75) to 17868 (1-25-76)

Figure 4-2 predicts Landsat-1's remaining freon life as a function of gating frequency and Figure 4-3 plots remaining Roll gates as a function of tank pressure.

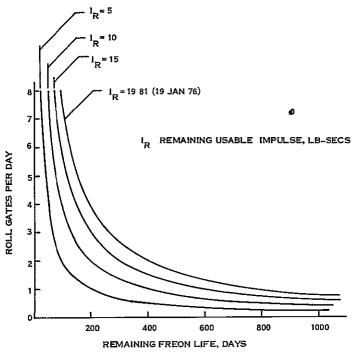


Figure 4-2. Landsat-1 Remaining Freon Life vs. Gating Frequency

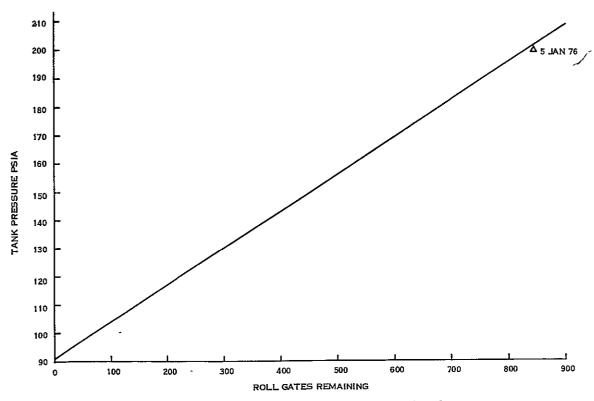


Figure 4-3. Landsat-1 Pressure - Roll Gate, Prediction

During early January, 1976, (approximately Orbit 17660, 11 January 1976) solar array tracking errors began to appear due to the increasing value of Beta angle. As Beta increased, the sun sensors' field of view for optimum response is exceeded, particularly with the ACS in the Normal mode where sun sensor shadowing exists. When the ACS is commanded into the Roll Diff Tach High Gain mode, the spacecraft assumes a minus Roll attitude error which causes the Right Sun Sensor to rotate toward the sun. The Sun Sensor receives more exposure and drives the Right Solar Array into alignment with the sun. Left Solar Array tracking error is relatively constant at 6° to 8° lagging, regardless of ACS mode.

Maximum values of Beta angle increase cyclically with time and during this season, should peak at 47.80 on 18 February 1976. The effect of solar array misalignment on payload operations during this season should be minimal; however, as maximum Beta angle values continue to increase in the future, solar arry tracking will degrade accordingly.

RMP 1 is functioning normally. Pressure/temperature ratios have all been satisfactory.

The forward scanner pressure decreased from 2.81 in Orbit 16530 (21 October 1975) to 2.80 in Orbit 17868 (25 January 1976) and is following the leak pattern described in previous reports.

Tables 4-1, 4-2 and 4-3 are a summary of Landsat-1's Attitude Control Subsystem Telemetry.

Table 4-1. Landsat-1 ACS Temperature and Pressure Telemetry Summary

					Orbit			
Function	Units	31	5099	10182	15254	16530	17408	17826
1084 RMP 1 Gyro Temperature	DGC	44.5	23,06	21, 22	42.40	43.11	43,83	43.32
1094 RMP 2 Gyro Temperature	DGC	74.3	75,10	43.45	24,05	25.15	26 08	25.68
1222 SAD RT MTR HSING Temp	DGC	21.1	22,00	20.55	22,89	23,69	24,54	23.57
1242 SAD LT MTR HSING Temp	DGC	27.0	30.38	28.18	29.53	30 79	31.74	31 31
1223 SAD RT MTR WNDNG Temp	DGC	25 3	26.54	24 63	27,06	27.45	28 10	27.15
1243 SAD LT MTR WNDNG Temp	DGC	28.7	32,92	30 32	31 98	33,44	34.52	83,94
1228 SAD RT HSG Pressure	PSI	76	7.35	7.12	6.88	6 88	6 85	6 80
1248 SAD LT HSG Pressure	PSI	7.0	6 86	6 47	6,18	6.18	6 13	6,10
1007 FWD Scanner MTR Temp	DGC	19.8	19.88	18 46	20,36	20.63	21.14	20,67
1016 Rear Scanner MTR Temp	∼ DGC	20 5	19.83	17 86	19,24	20.02	20 68	20, 19
1003 FWD Scanner Pressure	PSI	4,6	4 02	3,50	3,00	2,81	2 80	2,80
1012 Rear Scanner Pressure	PSI	7.8	7.87	7.44	6 97	6,96	6.96	6 96
1212 Gas Tank Pressure	PSI	1988, 0	1702 34	1454, 19	235 44	223 05*	202,86	186,06
1210 Gas Tank Temperature	DGC	22 6	24 30	22.56	24,36	25,20	25, 88'	25, 30
1213 Manifold Pressure	PSI	56.7	57 44	58.73	61,67	61,30	61,65	61.67
1211 Manifold Temperature	DGC	21 9	23,62	21.77	23,82	24,78	25, 59	24 97
1059 CLB Power Supply Card Temp	DGC	37.1	40.54	38.83	40.58	41,46	42 19	41.66
1260 ACS Baseplate 1	DGC	25,4	27.93	25, 36	26, 54	27,84	28, 87	28, 57
1261 ACS Baseplate 2	DGC	22,9	24,73	23.00	25 05	26 14	27.04	26, 65
1262 ACS Baseplate 3	DGC	23,4	23,69	21, 97	24,95	25,85	26 66	26.00
1263 THO1 STS	DGC	-6 8	-0.97	-3,41	1,22	5,29	6 91	7,58
1264 THO2 STS	DGC	-14.6	-9,42	-8, 27	-4,50	-1.96	~1, 17	1 74
1265 THO3 STS	DGC	-3,1	9.31	7.58	12.92	15,91	17.84	19,67
1266 THO4 STS	DGC	-13.9	2.85	-1.85	2.40	5 29	7.61	7.06
1267 THO5 STS	DGC	-8.9	-1.16	-5.17	2,92	9 37	11,62	13,56
1224 SAD R FSST	DGC	39 5	60, 21	63, 25	64 74	66.72	66.83	64.16
1244 SAD L FSST	DGC	27.1	51.11	53, 21	54,69	57,40	58,99	59,65

^{*}Pressure OROP due to PCM count step, not to loss of freon

Table 4-2. Landsat-1 ACS Voltages and Currents

*	-				Or	bit		
Function y	Units	31	5099	10182	15254	16530	17408	17826
, 1057 CLB Power Supply Volts	TMV	2,8	2,78	2.78	2.78	2.8	2.78	2.78
1081 RMP 1 MTR Volts	VDC	OFF	OFF	OFF	-30.14	-30.14	-30,14	-30.14
1082 RMP 1 MTR Current	Amps	OFF	OFF	OFF	.11 .	.11	.11	,11
1080 RMP 1 Supply Volts	Dav	OFF	OFF	OFF	-23,78	-23.78	-23.76	-23.76
1091 RMP 2 MTR Volts	VDC	-29.7	-29.63	-29.63	OFF	OFF	OFF	OFF
1092 RMP 2 MTR Current	Amps	0 10	['] 0.10	0 11,	OFF	OFF	OFF	OFF _
1090 RMP 2 Supply Volts	VDC	-23 4	-23 41	≟23. 50	OFF	OFF	OFF '	OFF
1320 SAD RT MTR WNDNG Volts	νασ	-4 8	-4.25	-3 89	-3.85	-3,67	-3.64	-3 65
1240 SAD LT MTR WNDNG Volts	VDC	-4.8	-4.09	-3, 36	-3.43	-3.50	-3.39	-3,37
1227 SAD RT -15 VDC Conv.	VDC	14.9	14 88	14.89	14 87	14.87	14.87	14.87
1247 SAD LT -15 VDC Conv.	VDC	15 2	15, 13	15, 14	15.06	15.10	15.09	15 10
1056 CLB <u>+</u> 6 VDC	TMV	2.4	2 35	2.35	2.35	2.35	2,35	2.35
1055 CLB <u>+</u> 10 VDC TMV	TMV	2.75	2.75	2.74	2,74	2 74	2,74	2.74

Table 4-3. Landsat-1 ACS Attitude Errors and Driver Duty Cycles

	<u> </u>	<u> </u>			Orbits			
Function `	Units	13198	13569	14001	15254	16530	17408	17826
1141 Pitch Fine-Error	DEG	- 0.40	- 0 08	- 0 02	- 2 13	- 82	79	80
1143 Pitch Flywheel Speed	RPM	- 10.49	- 26.86	- 1.21	12.92	- 43.34	- 76 11	- 66 00
1038 Pitch MTR DRVR CCW	PCT	4.96	5 81	4.55	3.28	5.19	3.30	2.52
1039 Pitch MTR DRVR CW	PCT	2.29	2.17	5.10	19.65	1.65	1.52	. 58
1030 Roll Fine Error	DEG	- 2.25	- 0.20	- 0.20	- 2.52	- 2.53	- 2.50	- 2.86
1127 Roll Rear Flywheel Speed	RPM	715.78	756.92	782.08	714.05	716.75	726.87	734.39
1126 Roll Fwd Flywheel Speed	RPM	641 82	674.47	693 31	641 32	642.77	646.51	643.76
1022 Roll Rear MTR DRVR CCW	PCT	0.01	0.68	0.90	.13	.03	.01	.00
1025 Roll Rear MTR DRVR CW	PCT	4.26	5.22	5, 52	4.17	4 15	4.45	4.57
1023 Roll Fwd MTR DRVR CCW	PCT	0.01	0.66	0.72	.08	.03	.02	.00
1024 Roll Fwd MTR DRVR CW	PCT	4.15	4.94	5.35	4.24	4.13	4,01	4.11
1035 Yaw Tach	RPM	-206.08	-116.50	- 93.72	-169.52	-202.90	-216.35	-199.31
1033 Yaw MTR DRVR CW	PCT	0.04	1.53	1.84	.09	.04	08	. 05
1034 Yaw MTR DRVR CCW	PCT	0.07	1.60	1.76	.~68	.68	62	. 57
1221 SAD Right Tach	DEG/MIN	3.37	3.37	2.81	3.37	3.38	3.37	3.41
1241 SAD Left Tach	DEG/MIN	2 80	2.81	2 81	2.79	2 77	2.78	2.76

NOTE: Tabulation of these functions began after the pitch flywheel anomaly (stopped) in Orbit 11125.

COMMAND CLOCK SUBSYSTEM (CMD)

COMMAND CLOCK SUBSYSTEM (CMD)

The Command Clock Subsystem operated nominally in this report period. On January 1, 1976, during Orbit 17516, the spacecraft clock was advanced by approximately 4 seconds. This over-compensation was adjusted on 2 January during Orbit 17542 by moving the clock back by about 4 seconds. Figure 5-1 shows the history of the S/C clock drift since launch.

Figure 5-2 shows the cumulative drift since launch (15.5 seconds slower in 39 months). The rate of drift is also shown. The rate now is increasing, having bottomed out at the end of 3 years at -0.55 milliseconds per orbit. Table 15-1 shows typical telemetry values since launch. All are nominal.

5-1

ĽS-1

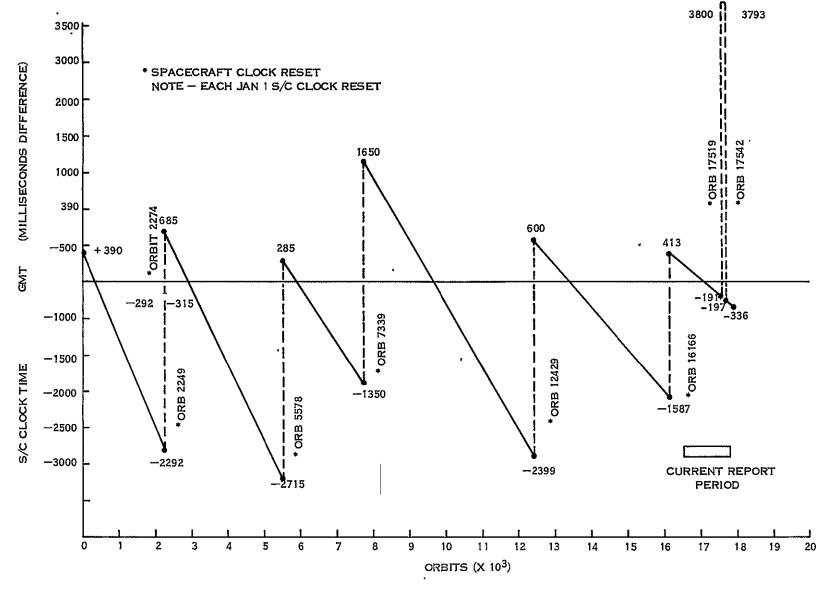


Figure 5-1. Landsat-1 Spacecraft Clock Drift History

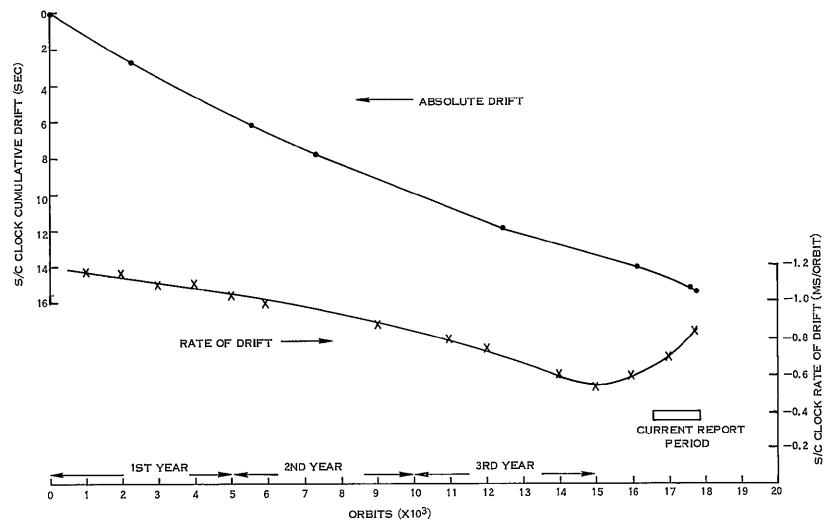


Figure 5-2. Landsat-1 Spacecraft Drift and Drift Rate

Table 5-1. Landsat-1 Command Clock Telemetry Summary

Dunati						Orbit			
Function No	Name	Mode	Units	35	5099	10182	16987	17405	17824
8005	Pri. Power Supply Temp	_	°C	37, 31	39, 37	39.50	38 19	38 17	37,63
8006	Red. Power Supply Temp	_	°C	35 73	38 08	38 38	37 05	37 01	36 99
8007	Pri. Osc Temp	_	°C	31.14	31.98	32 11	31 11	31 14	31 11
_8008	Red. Osc Temp	_	°c	30 47	31, 39	31.42	30 48	30,48	30 4B
8009	Pri. Osc Output	<u>-</u>	TMV	0 95	0 96	0,97	0 97	0 97	0 97
8010	Red! Osc. Output	-	TMV	**	**	**	**	**	**
8011	100 kHz	PriRed.	TMV	3, 11	3.10	3 11	2 96	3, 11	3 12
8012	10 kHz	Pri, -Red.	TMV	3 10	3 07	3 08	3 08	3 07	3 08
8013	2 5 kHz	Pri -Red	TMV	2 95	2 95	2 95	2 96	2 95	2 96
8014	400 Hz	Prı -Red	TMV	4 40	4 40	4 40	4 40	4 40	4 40
8015	Pri +4 V Power Supply	Pri Clk ON	VDC	4 10	4 10	4 10	4 10	4 10	4 10
8016	Red +4 V Power Supply	Red Clk ON	VDC	3 95	3 95	3 95	3 95	3 94	3 94
8017	Pri +6 V Power Supply	Pri Cik ON	VDC	6 06	6 07	6 07	6 10	6 09	6 10
8018	Red +6 V Power Supply	Red. Clk ON	VDC	6 00	5 94	5 94	5 96	5 95	5 96
8019	Pri -6 V Power Supply	Pri Cik ON	VDC	-6 02	-6 02	-6 03	-6 04	-6 03	~6 03
8020	Red -6 V Power Supply	Red Clk ON	VDC	-5 99	-6 00	-6 00	-6,01	-6 00	-6 00
8021	Pri -23 V Power Supply	Pri Clk ON	VDC	-22.88	-22.89	-22 89	-22,93	-22, 92	-22 92
8022	Red -23 V Power Supply	Red Clk ON	ADC	-22 98	-23 00	-23 01	-23 04	-23 05	-23 04
8023	Pri -29 V Power Supply	Pri Clk ON	VDC	-29 13	-29.16	-29 15	-29, 14	-29 13	-29.13
8024	Red -29 V Power Supply	Red, Clk ON	VDC	-29 07	-29 21	-29 21	-29,21	-29 21	-29 21
8101	CIU A -12 V	CIA A ON	VDC	-12 33	-12 33	-12 34	-12, 35	-12 35	-12 35
8102	CIU B -12 V	CIU B ON	VDC	-12 26	-12 26	-12 23	-12 26	-12 26	-12 26
8103	CIU A -5'V	CIU A ON	VDC	-5 32	-5 3 <u>4</u>	-5 34	-5 34	-5 34	~5 34
8104	CIUB-5V	CIU B ON	VDC	-5 31	-5 31	-5 31	-5 31	-5 31	-5 31
8105	CIÚ A Temp	CIU A ON	°C	24 47	24 77	25 04	. 24 41	24 61	24 58
8106	CIU B Temp	CHU BON	°C	24 96	25 31	25,45	24.81	24 99	24.92
8201	Receiver RF-A Temp	-	oC.	**	**	28.67	27 28	27 32	27.14
8202	Receiver RF-B Temp	- [°C	27 98	28 22	**	**	**	**
8203	D MOD A Temp	-	°C	25 41	25.73	37 98	36,79	36 99	36 87
8204	D MOD B Temp	-	°C	35 03	35 61	26. 12	25 00	25 00	24 89
8205	Receiver A AGC	Receiver A ON	DBM	**	**	-96 77	-94 72	-83,77	-89.11
8206	Receiver B AGC	Receiver B ON	DBM	-94.74	-84 67	**	**	**	**
8207	Amp A Output	Receiver A ON	TMV	**	**	2 31	2 54	2 74	2 81
8208	Amp B Output	Receiver B ON	TMV	2 81	3,22	**	**	**	**
8209	Freq. Shift Key A OUT	Receiver A ON	TMV	**	**	I 10	1 10	1 10	1 10
8210	Freq Shift Key B OUT	Receiver B ON	TMV	1 10	1 11	**	**	**	**
8211	Amp A Output	Receiver A ON	TMV	t skak	*x*	1 10	1 12	1 10	1 11
8212	Amp B Output	Receiver B ON	TMV	1 13	1,13	**	**	**	**
8215	D MOD A -15 V	Receiver A ON	TMV	**	**	5 00	5.00	5 00	5 00
8216	D MOD B -15 V	Receiver B ON	TMV	5 00	5 00	**	**	**	**
8217	Regulator A ~10 V	Receiver A ON	TMV	**	**	5 40	5 39	5 39	5 39
8218	Regulator B -10 V	Receiver B ON	TMV	5. 50	5.50	**	**	**	**

^{**}Units not in use

TELEMETRY SUBSYSTEM

TELEMETRY SUBSYSTEM (TLM)

The Telemetry Subsystem has performed nominally in this report period. Table 6-1 shows typical telemetry values since launch. Telemetry values are nominal despite the drift upwards of temperatures. As seen in Section 11, spacecraft temperatures reached all-time high values during this period. These temperatures are expected to subside to prior levels as the earth's distance from the sun increases in its yearly orbit. Functions 1011, 6012, 7010 and 12238 remain inoperative.

Memory, Section 11, continues to be used in the telemetry matrix.

Table 6-1. TLM Telemetry Summary

Function						Orbit			
No.	Function Name	Unit	35	5099	10592	15233	16987 ~	17405	17824
9001	Memory Sequencer A Converter	VDC	6 35	6,33	6 33	6 33	6 33	6 33	6 33
9002	Memory Sequencer B Converter	VDC	**	**	**	**	**	**	**
9003	Memory Sequencer Temp	°C	19,59	21 06	21.30	21 94	20 72	20 00	22 97
9004	Formatter A Converter	ADC	5 99	5,99	5,99	5 99	5 99	5 99	6 02
9005	Formatter B Converter	VDC	**	**	**	**	**	**	**
9006	Dig, Mux A Converter	VDC	10,01	10 04	10.07	10 07	10 07	10 07	10 07
9007	Dig. Mux B Converter	VDC	**	**	**	**	**	**	**
9008	Formatter/Dig, Mux Temp	°c	22,50	24 89	25.00	23.55	25 79	26 15	32 03
9009	Analog Mux A Converter	VDC	26,01	21.18	26.20	26 32	26 34	26 35	26 35
9010	Analog Mux B Converter	VDC	**	**	**	**	**	**	**
9011	A/D Converter A Voltage	VDC	10.00	10.07	10.07	10 07	10 07	10 07	10 07
9012	A/D Converter B Voltage	VDC	**	**	**	**	**	**	**
9013	Analog Mux A/D Converter Temp	°c	25,00	26.83	27 49	25 63	26 38	27 25	29 10
9014	Preregulator A Voltage	VDC	19 93	19.95	19 94	19 98	19 99	19 98	19 99
9015	Preregulator B Voltage	VDC	**	**	**	**	**	**	**
9016	Reprogrammer Temp	°c	22.00	22,50	22,53	22 50	23 50	23 35	27 41
9017	Memory A Converter	VDC	6 00	5.99	6.00	5 97	5 97	5.97	6 00
9018	Memory A Temp	°c	17,51	17 50	17.50	17 50	17.17	15 95	17 59
9019	Memory B Converter	VDC	**	**	**	**	**	**	**
9020	Memory B Temp	o _C	17,68	17.63	17,51	17 50	16 32	16 15	18 30
9100	Reflected Power (Xmtr A)	ďBm	11.95	12.32	12.38	11.37	12 53	12 25	13 10
9101	Xmtr A -20 VDC	VDC	-19,75	-19 76	-19.75	-19 84	-19 82	-19 83	-19 82
9102	Xmtr B -20 VDC	VDC	**	**	**	**	**	**	**
9103	Xmtr A Temp	°c	20 95	21 14	22.01	21 98	23 82	24 17	31 92
9104	Xmtr B Temp	°c	21.69	21,95	22 76	22 91	25 30	25 37	33 54
9105	Xmtr A Power Output	dBm	25, 12	25.35	25,24	25,00	24 88	24 86	25 00
9106	Xmtr B Power Output	ďBm	**	**	**	**	**	**	**

^{**} Units not used since prelaunch

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ORBIT ADJUST SUBSYSTEM (OAS) LANDSAT-1

ORBIT ADJUST SUBSYSTEM (OAS)

The Orbit Adjust Subsystem has been fired eleven times, seven times using the -X thruster and four times using the +X thruster. Three -X firings were for initial orbit correction and four -X for orbit maintenance. The four +X firings were for orbit maintenance.

No orbit adjustment was made during this report period.

The subsystem pressure/temperature parameters continue to be normal. During this report, there has been a considerable rise in the temperature of the -Y thrust chamber due to increased sun intensity and sun angle (See Section 11 Also). There is 64.85 pounds of hydrazine fuel remaining from an initial prelaunch load of 67.00 pounds. Figure 2-1 shows spacecraft ground track drift from standard orbit tracks and the effects of orbit adjustment. Table 7-1 is a summary of OAS performance to date, and Table 7-2 gives average telemetry values for the off quiescent state. In Table 7-2, it should be noted that the first four sample orbits occurred in periods of low sun intensity.

Table 7-1. Landsat-1 Orbit Adjust Summary

Orbit	Orbit Adjust No.	Ignition Epoch	Burn Duration (Seconds)	+Δa (Meters)	Engine Performance Efficiency	Fuel ¹ Used (Lbs)	Tank Pressure (PSIA)	Tank Temperature (^O F)	Axıs Thruster
38	1.	26 Jul 72 11.25.0.0	4,8	12	60 %		540	75	-x
44	2.	26 Jul 72 21 44 46	250.0	1975	103.4%	2.15	${ t u}^2$	v^2	-X
59	3.	27 Jul 72 23 34:45	313.0	2391	101.5%)	516	73.9	-x
938	4.	29 Sep 72	12 8	98	110.0%	0,039	v^2	υ ²	-x
2316	5.	13 Jan 73 00:21:30	20.4	154	106.0 %	0.071	489.4	75.4	-X
6390	6.	25 Oct 73 00:04:10.8	14.8	110	100,0 %	0,048	486,8	73.9	-x
7826	7.	4 Feb 74 23·27:10.4	14.7	112	101.8 %	0.048	490.59	75.4	-x
11367	8.	16 Oct 74 22:42:10,8	8,0	-65	106.0 %	0.026	490,59	74,0	+:X
11464	9.	23 Oct 74 21 40 00 4	8.4	-66	102,0 %	0,027	490.58	73,9	+X
13611	10.	26 Mar 75 19:39:00.8	2,8	-22,6	101 8%,	0 01	490 09	72.5	+X
14365	11.	19 May 1975 21 19 00.8	1,6	-13	102,4 %	0 01	486,84	71.6	÷Χ

¹ Initial Fuel Capacity - 67 lbs.

² Unavailable

Table 7-2. Landsat-1 OAS Telemetry Values

Function						Orbit			
No.	Name	Units	35	5099	10182	15254	17004	17394	17854
2001	Prop. Tank Temp.	°C	22.03	22.86	23.28	21.62	22,03	22.69	24.07
2003	Thrust Chamber No. 1 (-x) Temp. **	°c	29.57	29.93	30.55	30.52	29.83	28,93	26.52
2004	Thrust Chamber No. 2 (+x) Temp. **	°C	38.76	40.28	38.91	36.25	37.99	37.53	35.93
2005	Thrust Chamber No. 3 (-y) Temp. **	°C	34.55	34.41	36.09	38.45	46.35	50.05	57.50
2006	Line Pressure	psia	539.29	486.87	490.61	486.87	490.51	490.83	494.55

^{**} Wide spread of temperature is due to nozzle locations and satellite day/night transitions relative to data averaged. Typical orbital range is from 19 to 59 DGC.

MAGNETIC MOMENT COMPENSATING ASSEMBLY (MMCA)

MAGNETIC MOMENT COMPENSATING ASSEMBLY (MMCA)

The spacecraft was corrected for unbalanced magnetic moments in Orbits 73, 85, 110, 220, 11181, 11185, and 11186, as reported in early reports. Adjustments were made in the yaw negative dipole in Orbit 11186 and the pitch positive dipole in Orbit 220. A short roll dipole test was performed in Orbit 11185, with roll dipole returned to near zero. No adjustments were made in this report period.

The current dipole values are:

Pitch +2950 Pole-Cm Roll -500 Pole-Cm Yaw -3600 Pole-Cm

Telemetry measurement shown in Table 8-1 shows that the dipoles are holding steady without drift.

Table 8-1. MMCA Telemetry Summary (Landsat-1)

			Orbits							
Number	Name	Units	35	5099	10182	15254	17004	17394	17854	
4001	A1 Board Temp	°C	19.77	19.03	19.11	17.59	17.20	17.20	17.59	
4002	A2 Board Temp	°C	23.58	23.05	23.13	21.83	21.46	21.47	21.79	
4003	Hall Current	TMV	3.48	3.48	3,48	3.47	3.48	3.48	3.47	
4004	Yaw Flux Density	TMV	3.11	3.11	3.15	4.02	4.03	4.03	4.03	
4005	Pitch Flux Density	TMV	3.13	2.51	2.52	2,52	2.52	2.52	2.52	
4006	Roll Flux Density	TMV	3.19	3.19	3.20	3.28	3.28	3.27	3,28	

UNIFIED S-BAND/PREMODULATION PROCESSOR (USB/PMP)

UNIFIED S-BAND/PREMODULATION PROCESSOR (USB/PMP)

The USB Subsystem has operated nominally in this report period.

Table 9-1 shows telemetry values since launch. Telemetry values are nominal despite the drift upwards of temperatures. As seen in Section 11, spacecraft temperatures reached all-time high values during this period. These temperatures are expected to subside to prior levels as the earth's distance from the sun increases in its yearly orbit.

Figure 9-1 shows the USB power output history since launch. In Orbit 10068, the B Section of the transmitter was substituted, restoring full power output to the System. Figure 9-2 shows AGC readings at Goldstone for a constant reference orbit in each cycle since launch. The scatter of data points reflect variations in the ground station calibration and readout.

Table 9-1. Landsat-1 USB/PMP Telemetry Values

	Functions	·				Orbit			
No.	Name	Umts	35	5099	10592	15233	16987	17405	17824
11001	USB Reyr AGC	DBM	-122 78	-131.99	-129.81	-105 41	-97 18	-98,05	-114,78
11002	USB Xmtr Pwr	wts	1.60	0.29	1.54	1,53	1.52	1 47	1,55
11003	USB Revr Error	KHZ	21.79	-21.32	-23,25	-18.01	-13.98	-9.69	-17,52
11004	USB Xpond Temp	DGC	22,92	22.64	25 64	25,11	26 58	29.45	32.19
11005	USB Xpond Press	PSI	15,91	15.91	15.92	15.94	16.04	16.14	16.34
11007	USB Xmtr A -15V	VDC	-15.20	-15.20	**	**	0.0	0,0	0.0
11008	USB Xmtr B -15V	VDC	**	**	-15.20	-14.96	-15.20	-15,20	-15,20
11009	USB Range15V	VDC	-14.76	-14.76	-14.58	-14.58	-14.58	-14, 58	-14.58
11101	PMP Pwr A Volt	VDC	-15, 12	-15.18	**	**	0.0	0.0	0.0
11102	PMP Pwr B Volt	VDC	**	**	-15.12	-14.82	-14.78	-14 75	-14.81
11103	PMP Temp A	DGC	30.44	30.23	26,60	26,09	28.50	31.86	36.90
11104	PMP Temp B	DGC	**	**	31,64	31,67	33,42	37.10	42.29

^{**} Units Not in Use

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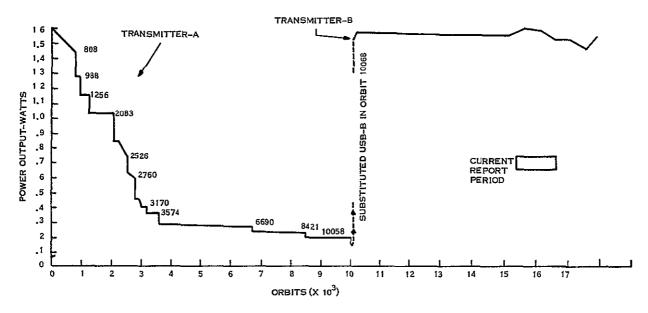


Figure 9-1. USB Power Output History (Landsat-1)

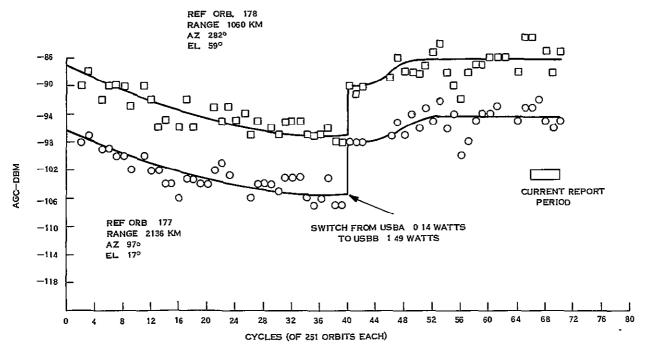


Figure 9-2. USB (Link 4) AGC Readings at Goldstone with 30' Antenna, Landsat-1

ELECTRICAL INTERFACE SUBSYSTEM

ELECTRICAL INTERFACE SUBSYSTEM (EIS)

Auxiliary Processing Unit (APU) consisting of Search Track Data, Time Code Data, and Backup Timers, operated satisfactorily throughout this report period. Telemetry for the APU is shown in Table 10-1. The APU is in Normal mode.

Table 10-1. Landsat-1 APU Telemetry Functions

	-					Orbit			
Functions	Description	Unit	7	5098	10182	15254	17004	17394	17854
13200	APU, -24.5 VDC	VDC	-24.90	-24.90	-24.91	-24.90	-24.90	′-24.90	-24.90
13201	APU, ~12 Volts	VDC	-12.08	-12.08	-12.07	-12.06	-12.06	-12.06	-12.06
13202	APU Temp.	DGC	25.49	26.95	27.15	26.82	28,20	29.14	31.49

The Power Switching Module (PSM), containing the switching relays for power to Orbit Adjust, MSS, WBVTR No. 1 and No. 2., RBV and PRM, functioned normally. The MSS power circuits have been operating on a regular basis throughout this report period. The power relay for the RBV remained in a failed closed condition since Orbit 196.

The Interface Switching Module (ISM) performed all switching normally during this report period.

SECTION 11 THERMAL SUBSYSTEM LANDSAT-1

THERMAL SUBSYSTEM (THM)

The Thermal Subsystem on Landsat-1 has maintained adequate control of spacecraft temperatures since launch. However, temperatures along bay 11 through 17 reached all-time peaks during this report period. The following factors have contributed to the unusual rise in temperature.

- 1. The sun intensity increased from 1.012 of the mean value at the beginning of this report period to a peak of 1.034 during the first week of January. Though the intensity declined slightly since then, it still has a high value of 1.032 at the end of this report period.
- 2. By 23 January 1976 the sun angle increased to 46.20 compared to 41.60 for the same time a year ago. This increased the intercept of solar flux on bays 11 through 17 which are normally warmer than others.
- 3. The length of satellite day increased more than 2 minutes above the span a year ago. This increased the time for heat absorption and reduced the time for heat rejection.
- 4. A possible malfunction of the thermal shutter for bay 14. Telemetry for shutter position for bay 14 has shown a constant value of 58,5° since 5 January 1976, although the bellows temperature has risen to about 31.6° (orbital average) by the end of the current report period. It has not been possible to determine whether this is caused by a telemetry failure or a shutter malfunction.

The temperatures are expected to decrease with decreasing sun intensity and sun angle.

Table 11-1 shows average analog telemetry values from data recorded on the NBTR. Figure 11-1 shows a typical thermal profile for average bay temperatures of the sensory ring in this report period.

No switching of the compensation loads was made during this report period. A history of all switchings of the compensation loads is given in Table 11-2.

	Function					Orbits			
No.	Description	Unit	26	5098	10182	15254	17004	17894	17854
7001	THM THO1 ST1	DGC	19.52	20.85	21.65	19.48	19.45	19.79	20.58
7002	THM THO2 SBO	DGC	18.60	19.95	20.60	18.62	18.37 17.75	18.41	18.52 18.30
7003 7004	THM THO3 STI THM TH10 TCB	DGC DGC	18.48 19.47	20.16	20.87	18.11 19.76	20.52	17.85 21.06	22.35
7004	THM THO4 STI	DGC	18.39	19.71	20.35	17.86	17.51	17.61	17.91
7006	THM THO5 SBO	DGC	17.57	18,39	18.81	17.20	16.62	16.61	16.78
7007	OA-X THRUSTER	DGC	21.95	22.95	22.90	22.25	22,11	22.06	21.98
7008	THM THOS STO THM THOS SBI	DGC DGC	15.95 19.38	16.61 20.35	16.90 20.93	15.34	14.77 18.14	14.78 18.21	14.92 18.52
7009 7010	THM THOY STI	DGC	18.61	*	*	*	**	**	**
7011	THM THOS STO	DGC	21.78	22.77	22, 88	22.03	21.81	21.79	21.65
7012	THM TH09 SBI	DGC	21.81	22.87	23.08	22,20	22.31	22.52	22.97
7013	THM THIO SBO	DGC	18.73	19.53	19.64	19.00	19.22 23.73	19.50 24.43	20.07 26.10
7014 7015	THM TH11 STI THM TH12 SBO	DGC	22.37 22.37	23.35 23.17	28.57 23.03	22.80 22.86	24.60	25.86	28.89
7016	THM THIS STI	DGC	20.95	22.02	22.47	22.00	23.74	25.15	28.77
7017	rby beam otr ln	DGC	21.53	22,62	22.84	21.88	22,41	22.84	23.87
7018	THM THI4 STO	DGC	20.38	21,40	21.93	21.88	23.96	25, 89	30.96
7019 7020	NBR RAD OUTBD B4 THM TH15 SBI	DGC DGC	5.09 21.14	5.86 23.24	6,00 28,99	4,37 22.18	3.76 23.98	3.89 25.46	4.37 29.63
7021	THM THIS SEI	DGC	20.73	22.90	23.68	21.64	22.66	23.78	26.82
7022	THM TH17 SBI	DGC	20.22	22.76	23, 56	21.47	21.76	22.69	24.88
7023	THM TH18 SBO	DGC	21.90	24.29	25, 19	23.47	23.57	24.20	25.44
7030 7031	THM THOS BUR THM THOS BUR	DGC DGC	16.05 13.59	17.07 14.17	17.42 14.28	15.35 12.87	15.05 12.31	15.00 12.32	15.09 12.40
7032	THM THOS BUR	DGC	19.92	20.75	20.74	20.17	20,28	20.38	20.56
7033	THM TH12 BUR	DGC	21.51	22.16	22.76	22.65	24.66	26.02	29.42
7034	THM TH15 BUR	DGC	19.70	21.67	22,38	21.33	23.35	24.86	28.86
7035	THM TH18 BUR THM TH01 TCB	DGC	20.11	21.36	22, 02	20.54	21.01 19.21	21.43 19.49	22.17 19.94
7040 7041	THM THOI TCB .	DGC	19.27	20.46 19.23	21.26 19.89	19.19 17.80	17.51	17.55	17.70
7042	THM THOS TCB	DGC	18.34	19,94	20,92	17.79	17.48	17.50	17.64
7043	THM TH04 TCB	DGC	18.95	19.94	20.26	18.60	18.23	18,23	18,44
7044	THM THOS TCB	DGC	16.27	16,98	17.32	15.90	15.36	15.38	15.57
7045 7046	THM TH07 TCB THM TH09 TCB	DGC	18.41 19.38	19.21 20.37	19.45 20.64	18.25 19.85	17.86 19.73	17.87 19.89	18.01 20.13
7048	THM THIL TCB	DGC	21.98	22.94	23.18	22.80	24.05	24.88	26,85
7049	THM THI2 TCB	DGC	21.92	22,46	22.35	22.30	24.21	25.73	29.54
7050	THM TH13 TCB	DGC	21.21	21.99	22.29	22.26	24.38	26,28	31,21
7051	THM THI4 TCB	DGC	21.38	22.88	23.62	22.74	24.64	26,50 25,11	31.57
7052 7053	THM THIS TCB THM THIT TCB	DGC DGC~-	21.30 -21.73	28,95 24,08	25.13 25.02 -	22.68 -28.33	23.99 ~22.87	23.59	28.17 25.17
7054	THM TH18 TCB	DGC	20.02	22.20	23.35	21.04	20.86	21.25	21.79
7060	THM SHUTTER BY 1	DEG	25.85	33.12	38.62	24.41	24.30	27.26	31.45
7061	THM SHUTTER BY 2 THM SHUTTER BY 3	DEG DEG	6.62 10.96	8.65	13.28 30.24	1.73	0.0	0.58 13.35	1.17
7062 7063	THM SHUTTER BY 4	DEG	30.60	23.58 35.71	37.92	17.30 29.50	13.32 26.97	27.00	27.75
7064	THM SHUTTER BY 5	DEG	15,03	16.25	15.00	8.08	3,46	5.19	5.19
7065	THM SHUTTER BY 7	DEG	17.14	24.64	21.96	14.50	8.50	9.00	9,00
7067	THM SHUTTER BY 9	DEG	33.26	38.44	39.50	38.24	38.26	38.44	38.83
7068 7069	THM SEUTTER BY 10 THM SHUTTER BY 11	DEG DEG	24,68 39,66	28.68 46.89	27.31 48.96	26.03 46.97	27,35 53,10	\$2.50 56.94	40.69 62.45
7070	THM SHUTTER BY 12	DEG	43.81	46.63	45.68	45.95	57.92	64.89	70.31
7071	THM SHUTTER BY 13	DEG	40.39	46,38	44,79	42,84	51.83	60.51	62.63
7072	THM SHUTTER BY 14	DEG	84.20	39.70	41.91	34.28	46.51	56.41	58,50
7073 7074	THM SHUTTER BY 15 THM SHUTTER BY 16	DEG DEG	45.40 24.50	58.74 48.46	64.79 53.54	55.15 38.76	69.16 46.86	76.95 54.50	82.15 64.40
7075	THM SHUTTER BY 17	DEG	39.06	54.96	61.88	51.06	46.99	52.21	63.68
7976	THM SHUTTER BY 18	DEG	29.70	43.15	51.20	35.12	33.09	36.30	40.95
7 0 80	THM Q1 T ZENER V THM Q2 T ZENER V	ADC	8.19	8.19	8.19	8.19	8.19	8, 19	8.19
7081 7082	THM Q2 T ZENER V THM Q3 T ZENER V	VDC VDC	8.40 8.31	8.40 8.31	8.40 8.32	8.40 8.31	8.40 8.31	8,40 8,31	8,40 8,31
7083	THM Q1 S ZENER V	VDC	8.31	8.32	8.35	8.31	8.32	8.32	8.35
7084	THM Q2 S ZENER V	VDC	8, 19	8,19	8.20	8.19	8,19	8,19	8,20
7085	THM Q3 S ZENER V	VDC	8.15	8.15	8.15	8.15	8.15	8.15	8.15
7090 7091	THM PSM MOUNT THM IND ATTITUDE	DGC DGC	21.60 19.40	22.54 20.42	22.98 20.88	21.43 19.13	21.91 18.66	22.48 18.75	24.02 19.16
7092	THM RBV RADIATOR	DGC	15.40	17.22	17.47	16.55	17.23	17.67	18.68
7093	THM RBVC CTR BM	DGC	20.30	21.61	21.87	20.73	21.49	21.97	23.24
7094	THM WBYTR ROOT	DGC	12.96	15.71	16.07	13.77	12.82	13.27	14.42
7095	THM WBVTR RAD CT	DGC	4.81	8.17	8,68	6.99	6.83	7.12	7.56
7096 7097	THM WBVTR STRAP THM WB MT BAY 1	DGC DGC	16.62 20.56	19.32 19.52	19.66 21.37	17.29 16,97	15.56 17.32	16.00 17.55	17.07 18.23
7098	THM WB MAT BAY 1	DGC	20.22	18.90	20.39	17.12	17.66	18.00	18.89
7099	THM WBYTR SEP 3	DGC	18,60	20.55	21.05	18.45	17.69	17.90	18.49
7100	THM WBVTR SEP 17	DGC	21.31	28.66	24.23	22.02	21.89	22.68	24.61
7101 7102	THM WBVTR 1 CENT	DGC	21.49	23.72	24.01	21.63	19.03	19.50	20.67
7102 7103	THM WBVTR 2 BAY THM WBVTR 2 BY 15	DGC DGC	17.46 21.00	18.92 23.16	19,32 23,82	17.23 21.73	16.77 22.28	16.97 23.38	17.55 26.34
71.04	THM WBVTR 2 CTR	DGC	19.35	21.51	21.81	19.54	18.39	18.97	20.59
7105	THM NBTR B SEP 6	DGC	18.06	19.30	19,79	17.82	17.30	17.50	18.32
7106	THM NBTR B SEP 1	DGC	20.82	22.35	22.89	21.61	22.92	24.25	27.72
7107 7108	THM NBTR BM CTR THM MSS MOUNT 14	DGC DGC	19.37 19.18	21.04	21.34	19,51	19.76	20,29	21.93
7108 7109	THM MSS MOUNT 14 THM OA -Y THRUSTER	DGC	19.18 22.21	21, 15 23, 80	21.70 24.69	20.06 24.40	21.54 27.33	22.88 29.36	26.45 34.20
	THM MSS WBVTR BM	DGC	18.14	20.06	20.53	18,18	18.09	18,42	19.56
7110									
7110 7111 7130	THM OA +X THRUSTER THM AUX P1 T	DGC DGC	20.30 15.69	19, 92 8, 49	21.22 -18.90	18,07 9,68	18.60 19.51	18.86 25.64	19.48 21.76

Table 11-2. Landsat-1 Compensation Load History

		Co	mpensat	ion Load	Status*			
Orbits	1	2	3	4	5	6	7	8
Launch	0	0	0	0	0	0	0	0
2	0	0	х	x	x	0	х	x
6	х	x	х	x	x	0	x	х
118	0	0	0	0	0	0	0	0
156	x	x	х	x	x	0	x	х
194	0	0	0	0	0	0	0	0
197	x	x	х	x	x	0	х	х
701	x	x	0	x	x	0	x	х
1410	х	x	0	x	x	0	0	x
3484	х	x	x	x	x	0	0	х
3644	х	x	0	x	x	0	0	х
3646	x	x	x	x	x	0	0	х
4177	х	х	0	x	х	0	0	х
6872	х	х	х	x	x	0	0	x
6966	х	х	0	x	x	0	0	x
8291	х	x	х	x	х	0	0	x
8348	x	x	0	x	х	0	0	x
8449	x	х	х	х	x	0	0	х
8472	х	x	0	x	x	0	0	x
8538	x	x	x	x	х	0	0	х
8928	х	x	0	х	x	0	0	х
9898	x	x	x	х	х	0	0	x
10410	x	x	0	x	х	0	0	х
11125	0	0	0	0	0	0	0	0
11126	х	х	0	x	х	0	0	х
11127	0	0	0	0	0	0	0	0
11133	x	х	0	x	х	0	0	х
12604	x	х	х	х	x	0	0	х
13206	x	x	0	х	x	0	0	0
15584	x	x	0	0	х	0	0	0

* Note: x = ON

0 = OFF

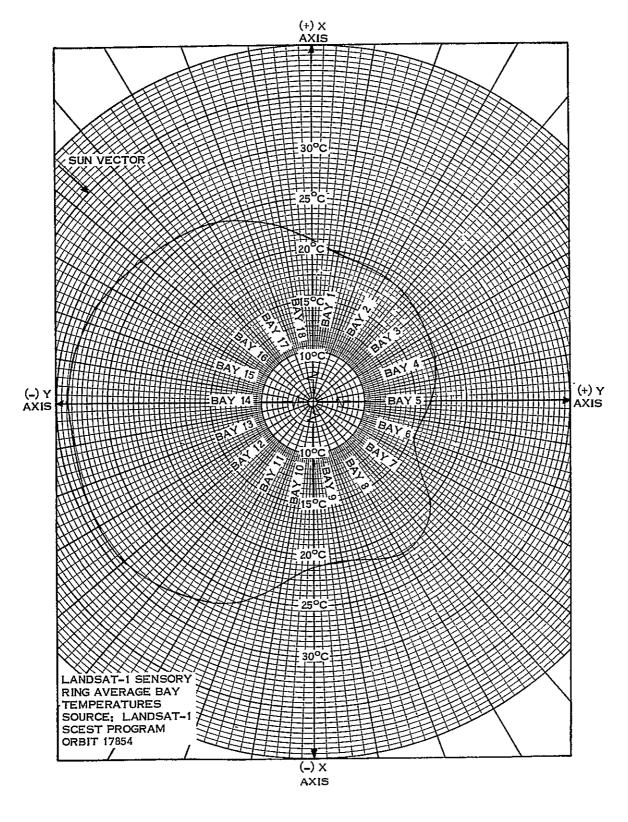


Figure 11-1. Landsat-1 Sensory Ring Thermal Profile

11-6 LS-1

NARROWBAND TAPE RECORDERS

NARROW BAND TAPE RECORDERS (NBR)

Narrowband Recorder NBR-B, which was turned off in Orbit 15256, has remained inactive during the entire reporting period.

Narrowband Recorder NBR-A operated satisfactorily during this period, and has provided coverage for MSS real-time operations as well as approximately 3-1/2 hours daily of normal orbital telemetry recording and playback functions.

Table 12-1 gives cumulative operating hours for both recorders by modes, and Table 12-2 gives typical telemetry values.

Table 12-1. NBR Operating Hours by Modes, Landsat-1

NBR	OM	OFF	Playback	Record
A	14122	16570	566	13556
В	11909	12666	476	11433

Table 12-2. Narrowband Tape Recorder Telemetry Values, Landsat-1

	Function		Typical	Telemetr	y Values -	Orbits	
No.	Name	6	3750- 3751	10862	15256	15888	17684
10001	A - Motor Cur. (ma) Record P/B	190,10 180,00	189.20 178.69	186.31 180.00	192.63 N.A.	192,63 *	195.8 *
10101	B - Motor Cur. (ma) Record P/B	193.26 188.18	193.04 185.44	198.95 187.89	198.95 202.1	*	*
10002	A - Pwr Sup. Cur. (ma) Record P/B	320,56 535,78	338.20 568.38	339.81 567.75	343.24 N.A.	339.81 *	339.81 *
10102	B - Pwr Sup. Cur. (ma) Record P/B	31 7. 62 570.78	336.05 553.63	350.00 567.50	346.75 580.51	*	*
10003	A - Rec. Temp. (DGC)	25.47	34.40	23.60	22.00	23.00	21.20
10103	B - Rec. Temp. (DGC)	24,58	23,41	23.41	23.18	18.18	19.54
10004	A - Supply (VDC)	-24.47	-24.44	-24.62	-24.62	-24.62	-24.62
10104	B - Supply (VDC)	-24.44	-24.51	-24.29	-24.57	-24.71	-24.71

N.A. - Data not available

^{* -} No data. NBR-B out of service

SECTION 13 WIDEBAND TELEMETRY SUBSYSTEM LANDSAT-1

WIDEBAND TELEMETRY SUBSYSTEM (WBTS)

The Wideband Telemetry Subsystem has operated nominally in this report period.

Table 13-1 shows typical telemetry values. All are nominal.

Figure 13-1 is the AGC history at Goldstone. The scatter of data points reflect variations in the ground station calibration and readout.

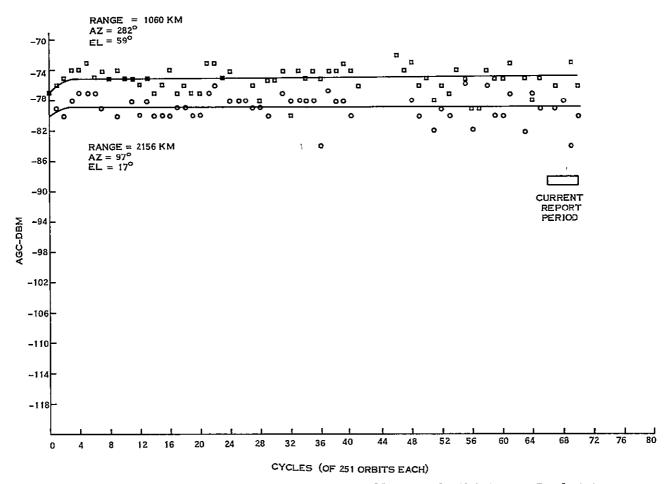


Figure 13-1. WPA-2 (Link 3) AGC Readings at Goldstone with 30' Antenna - Landsat-1

LS-1 13-1

Table 13-1. Wideband Modulator Telemetry Values, Landsat-1

WBPA-1

····	Function]		Oı	bits	
Number	Name		26	1894	1944	2095
12001 12002 12003 12004 12005 12227 12229 12232 12234 12235 12238 12240 12242	Tmpt TWT Coll. Helix Current TWT Cath. Curr. Forward Pwr Reflected Pwr Loop Str. AFC Con Volt (1) Mod Temp VCO +15 VDC Pwr Sup A (2) -15 VDC Pwr Sup A +5 VDC Pwr Sup A -5 VDC Pwr Sup A -15 VDC Pwr Sup A -17 VDC Pwr Sup A -18 VDC Unreg Volt A -19 VDC Unreg Volt A -19 VDC Unreg Volt A	(DgC) (Ma) (Ma) (DBM) (DBM) (MHz) (DgC) (TMV) (TMV) (TMV) (TMV) (TMV) (TMV) (DgC)	35.7 6.08 45.89 43.18 34.95 -0.39 21.93 2.69 5.98 3.94 5.28 5.56 20.60	39.20 6.49 43.54 42.88 34.99 -1.29 20.31 2.69 5.96 3.94 5.26 5.51 23.43	39.90 6.58 43.48 42.61 34.80 -0.86 20.88 2.65 5.73 3.94 5.18 5.42 24.71	39.90 6 78 45.01 43.15 35.21 -0.67 20.39 2 62 5.78 3.95 5.12 5.49 24.04

WBPA-2

	Function					Orbits			
Number	Name		33	4096	10602	15233	16987	17405	17824
12101 12102 12103 12104 12105 12228 12229 12232 12234 12236 12239 12240	Temp TWT Coll. (Max) Helix Current TWT Cath. Cur. Forward Pwr Reflected Pwr Loop Str. AFC Con Volt (1) Mod Temp VDC +15 VDC Pwr Sup A (2) -15 VDC Pwr Sup A +5 VDC Pwr Sup A -5 VDC Pwr Sup A -15 VDC Pwr Sup A -16 VDC Pwr Sup A -17 VDC Pwr Sup A -18 VDC Pwr Sup A -19 VDC Pwr Sup A -19 VDC Pwr Sup A	(DgC) (Ma) (Ma) (DBM) (DBM) (MHz) (DgC) (TMV) (TMV) (TMV) (TMV) (TMV) (CMV) (CMV)	35 38 7.32 44.30 43.57 31.59 1 11 21.70 2.68 5.90 3.97 5.24 5.43 23.03	34 24 7.70 43.85 43.57 32.79 -0.78 20.88 2.69 5.98 4.01 telemetr 5.52 22.96	35.96 7.67 42.72 43 47 32 62 -1.12 21.50 2.69 5.92 4.01 y point defe 5.46 23.86	29 77 7.90 43.70 43.52 33.07 -1.05 21.78 2.65 5.81 3.97 ective 5 44 23.66	23. 49 7. 56 41. 30 43. 34 32. 42 -1 63 22. 64 2. 68 5. 97 3. 90 5. 56 21. 26	26.26 7.78 42.61 43 52 32 71 -1 47 18.95 2.69 5.97 4.02 5.56 19.16	23 88 7.94 42 65 43 49 33 11 -1.17 20.45 2.67 5.80 3 97 5.47 23 44

⁽¹⁾ Satisfactory if not zero or -7.5 (2) B Power Supply not yet used in orbit

ATTITUDE MEASUREMENT SENSOR

ATTITUDE MEASUREMENT SENSOR (AMS)

Telemetry output of the AMS continues to be normal and in good agreement with the ACS subsystem.

Table 14-1 gives typical AMS telemetry values.

Table 14-1. Landsat-1 AMS Temperature Telemetry

			Orbits						
Function	Description	Units	35	5099	10182	15254	16530	17408	17826
3004	Case-Temp 1	DGC	18.92	19.42	19.71	18.54	18,37	18,93	19.40
3005	Assembly-Temp 2	DGC	19.15	19.76	19.96	18.73	18.70	19.19	19.74

WIDEBAND VIDEO TAPE RECORDERS

WIDEBAND VIDEO TAPE RECORDERS (WBVTR)

WBVTR-2 has not been operated since its failure in Orbit 148.

WBVTR-1 was removed from operational service after Orbit 9881 because of high minor frame sync error counts. The recorder has remained inactive since suspension of engineering tests after Orbit 10861.

Pressure and temperature telemetry values for WBVTR-1 transport and electronics units are shown in Table 15-1.

Table 15-1. WBVTR-1 Telemetry Values

W.B	VTR-1 Functions	Telemetry Values in Orbits					
Number	Name	ie 15260		16530	17810		
13022	Press. Trans. (PSI)	15.73	15.59	15.66	15.73		
13023	Temp. Trans. (DgC)	18.55	16.36	17.36	19.50		
13024	Temp. Elec. (DgC)	15.00	13.84	14.75	15,38		

RETURN BEAM VIDICON

RETURN BEAM VIDICON (RBV)

The RBV has not been reactivated since Orbit 196, but it is capable of operation through individual component power switching. An assessment of the RBV performance was given in ERTS-1 Flight Evaluation Report 23 July to 23 October, 1972.

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SECTION 17 MULTISPECTRAL SCANNER SUBSYSTEM LANDSAT-1

MULTISPECTRAL SCANNER SUBSYSTEM (MSS)

The Multispectral Scanner Subsystem operated nominally in this period without incident. Figure 17-1 shows the number of scenes imaged at each geographical location in this quarter. Figure 17-2 shows the number of scenes imaged in the first 3 years of operation. Figure 17-3 shows the number of scenes imaged after the 3 year period and before the start of this quarter. The sum of these three maps shows the number of scenes imaged since launch. In these maps, only those scenes received by U.S. ground stations are shown. Scenes transmitted to Canada, Brazil and Italy (34% of total) are not shown.

Table 17-1 shows typical telemetry values since launch. The higher temperatures shown in Orbit 17824, reflect general spacecraft temperature increases due to the earth-sun distance approaching its lowest value, but a new operating procedure adds greatly to the reported value, even though there is no real change in equipment temperature. The temperatures reported are computer-derived average temperatures for the NBR on-time. Until recently, the NBR was ON throughout the orbit, so that with MSS ON only 8% of this time, "averages" were relatively low. Recently, to prolong its life, the NBR is ON only to span MSS operations. Now with MSS ON about 70% of the NBR ON-time, "averages" are much higher. With this adjustment, all telemetry values are nominal.

Table 17-2 shows the history of sensor response to a constant input radiance level. Each sensor is sampled at 5 radiance levels, and all show essentially the same trends. Only one of these levels (the second highest) is listed in Table 17-2. Sensor 4 has declined most (22 %) since launch. This is twice the average sensor decline. Sensor 13 remains apparently stable at its elevated level - 13 % - since launch.

Line length history is also shown in Table 17-2, and remains satisfactory.

Sun Calibrations, performed every two weeks, continue to show nominal performance.

LS-1 17-1/2

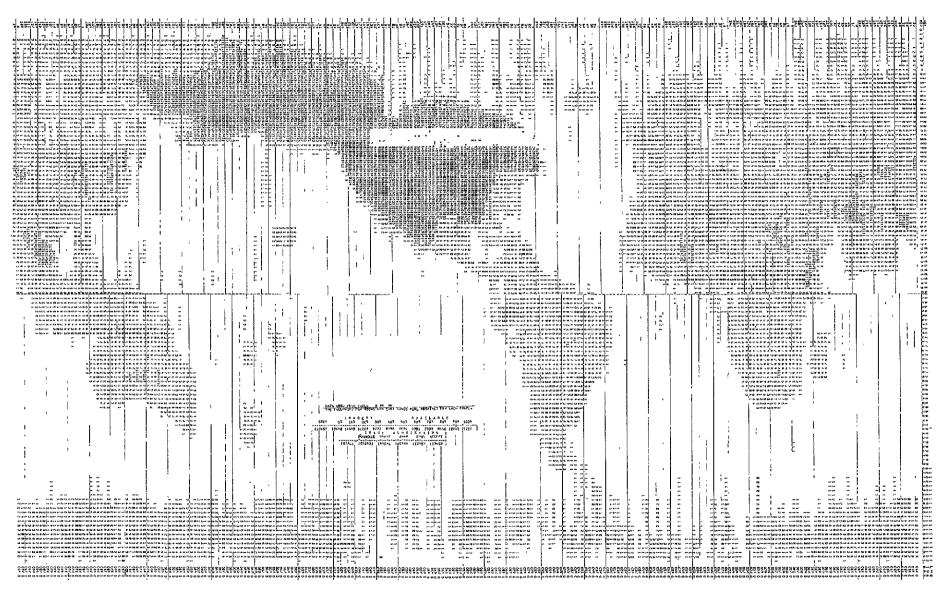


Figure 17-2. Computer Map of MSS Scenes for First 3 Years Operation - Landsat-1

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FOLDOUT FRAME

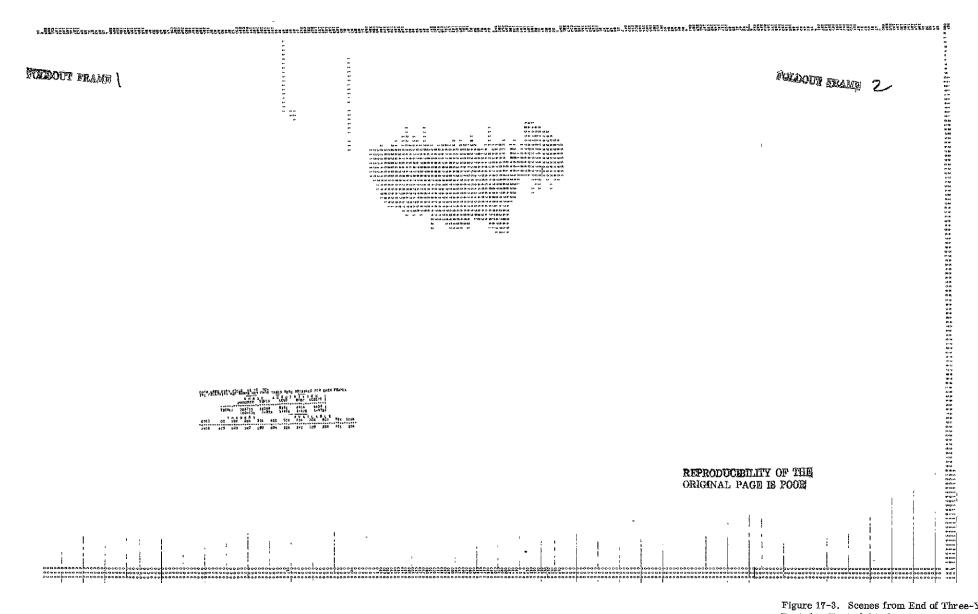


Figure 17-3. Scenes from End of Three-Year Period to Start of this Quarter - Landsat-1

Table 17-1. MSS Telemetry Values

Function			Telemetry Values in Orbits						
No.	Name		20	5060	10587	15233	16987	17405	17824
15044	FOPT 2 T	(DGC)	17.46	19.84	19.75	18.15	18.62	18.40	20.14
15046	ELEC CVR T	(DGC)	19.37	21.83	21.96	20.20	19.76	18.66	21.49
15048	SCAN MIR REG T	(DGC)	16.35	19.77	20.48	20.94	20,99	20.29	23.63
15050	SCAN MIR DR. COIL T	(DGC)	15.94	19.30	19.78	19,21	19.85	19.59	22.64
15052	ROT SHUT HSG T	(DGC)	16.91	20.07	20.23	18.74	18,89	18.84	20.52
15043	FOPT 1 T	(DGC)	17.67	20.01	19.93	18.35	18.84	18.62	20.33
15045	MUX PWR CASE T	(DGC)	21.19	22.03	23,87	26.92	24.23	22,50	30.84
15047	PWR SUP T	(DGC)	17.41	20,00	20,21	19.83	20.00	19,34	21.88
15049	SCAN MIR DR. ELC T	(DGC)	16.12	19.41	20.23	21.16	21.10	20.40	23.83
15051	SCAN MIR HSG T	(DGC)	15,60	19.05	19.49	18,40	19,32	18.78	22.00
15040	MUX -6 VDC	(TMV)	4.03	4.03	3.98	4.02	4.03	4.03	4.07
15042	AVE DENS DATA	(TMV)	1.67	2.13	2.05	2,28	2.10	1.78	2.08
15054	CAL LAMP CUR A	(TMV)	1.12	1,12	1.12	1.12	1.12	1.12	1,12
15056	BAND 2 <u>+</u> 15 VDC	(TMV)	5.10	5,10	5.04	5, 10	5.10	5.10	5.10
15058	BAND 4 <u>+</u> 15 VDC	(TMV)	5.10	5.10	5.04	5.10	5.10	5,10	5.10
15060	+ 12 -6 VDC REG	(TMV)	4.82	5.02	4.97	5,02 -	5,02	5.02	5.02
15062	+ 19 VDC REC OUT	(TMV)	4.80	4.90	4.97	5,03	5.03	5,03	5.03
15064	BAND 1 HV A	(TMV)	5.10	5.16	5.12	5,12	5.12	5.12	5.13
15066	BAND 2 HV A	(TMV)	4.50	4.52	4.52	4.50	4.50	4.57	4.52
15068	BAND 3 HV A	(TMV)	4.60	4.62	4.62	4.62	4.63	4.62	4.62
15070	SHUT MOT CON OUT	(TMV)	2.43	2,44	2.47	2,51	2.50	2.50	2.50
15041	S/D CONV REF V	(TMV)	5.93	5.93	5.87	5,93	5,93	5,93	5,93
15053	SCAN MIR REG V	(TMV)	4.42	4.51	4.51	4.61	4.61	4.60	4.60
15055	BAND 1 <u>+</u> 15 V	(TMV)	4.97	4.97	4.92	4.97	4.97	4.97	4.97
15057	BAND 3 <u>+</u> 15 V	(TMV)	5.00	5.00	4.94	5.00	5.00	5,00	5.00
15059	-15 VDC TEL.	(TMV)	5.02	5,02	5.02	5.02	5.02	5.02	5.02
15061	± 5 VDC LOGIC REG	(TMV)	4.82	4.81	4.77	4.76	4.82	4.81	4.77
15063	-19 VDC REG OUT	(TMV)	3.43	3,39	3,50	3.58	3.58	3.57	3,57
15071	SCAN MIR DR. CLK	(TMV)	1,93	1.97	1,98	2.00	2.00	1.96	1.97

Table 17-2. MSS Response History Landsat-1 Quantum Level for Selected Work (0=Black: 63=White)

1	Quantum Level							
	¥	1st	Year-	←2nd Yr:→	← 3rd Yr. →	← 4th Yr. →		% Change
Band	Sensor	Launch	2-4 Quar.	5–8 Quar.	9-12 Quar.	13 Quatr.	This Quar.	Since Launch
	1	43	39	39	38	37	37	-14
	2	44	39	40	40	39	39	-12
	3	43	38	40	40	39	40	-6
1	4	43	38	39	39	38	38	-12
	5	41	36	35	34	32	32	-22
	6	43	39	41	41	40	40	-7
	7	47	43	43	42	41	41	-13
	8	46	41.5	41	4 1	40	40	-13
2	9	47	44	42.5	42	41	40	-15
	10	4 6	42	41.5	41	41	41	-11
	11	47	42.5	42	42	41	41	-13
	12	45	42	42.5	42	42	42	~6
	13	46	46	49	5 1	52	52	+13
	14	44	42	42	42	42	42	-5
3	15	45	42.5	42	41	41	41	-9
	16	40	37.5	37.5	37	37	37	-8
	17	42	39	40	40	40	40	-5
	18	44	40	40.5	41	41	41	-7
4	19	28	28	27	25	23	23	-18
	20	25	26	25	23	21	21	-16
	21	26	27	26.5	25	23	23	12
	22	23	23	22	21	19	19	-18
	23	22	22,5	23	21	21	21	- 5
	24	24	23.5	24	23	22	22	-8
	Line Length	3221	3219	3217	3216	3216	1314	-0.2

17-10 LS-1

SECTION 18 DATA COLLECTION SUBSYSTEM LANDSAT-1

DATA COLLECTION SUBSYSTEM (DCS)

The Data Collection Subsystem was turned OFF after Orbit 12690 on 19 January 1975, and has not been used since.

The DCS operated without anomaly throughout its operational period. Only Receiver #1 was used.

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APPENDIX A LANDSAT-1 ANOMALY LIST

APPENDIX B

LANDSAT-1 SPACECRAFT ORBIT REFERENCE TABLES

LANDSAT-1

SPACECRAFT ORBIT REFERENCE TABLES

FROM JULY 1975 THRU DECEMBER 1976

ORBIT 14953 THRU 22621

FIIGHT DAY 1073 THRU 1622

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	4	185	1076	1	14995=15008	ļ	71 = 84	1	6	l	60
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	6	[187	€078	1	15023-15035	1	99#111	1	S	l	60
	7	ן 188 ן	€679	I	15036+15049	ŀ	112-125	ł	9	I	60
	ક	189	1080	ı	15050-15067	ı	126-139	1	10	ŀ	60
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	10	191	1082	ı	1507๙−15∩91	1	154=167	1	12	ŀ	60
	"11	1 192 1	1083	1~	115092-15105	1	~ 168=181	1	13	ŀ	60
	12	193	1084	- 1	15106=15119	1	182=195	1	14	1	60
	13	1 194 1	1085	1	15120-15133	1	196-209	1	15	I	60
	14	195	1086	ł	15134-15147	Ì	210-223	1	16	ı	60
	15	196	1087	-	15148-15161	ı	224-237	- 1	17	ļ	60
	16	1 197	1088	-	15162-15175	ı	238=251	-1	18	1	60
	- 17 -	198	1089	ı	15176-15189	Ì	- 1- 14	1	1	ŀ	61
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	19	1 200 1	1091	i	15204-15217	1	29- 42	- 1	3	l	61
	20	201	1092	I	15218=15231	1	43 = 56	1	4	ı	61
	21	1 202	1093	1	15232-15245	1	57 = 70	1	5	i	61
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	23		1095	-1-	T15260×15273	ŧ	። ጸናቀ 9ዳ	1	7	ı	61
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	25	1 206 1		ł	15287=15300	1	112=125	1	ð	ı	61
	26	I 207 !	1098	1	15301-15314	1	126=139	1	10	ı	61
	- 27	1 208 I	1099 -	- 1	1531ถื∞15จ≥ห	ı	140+153	1	11 5	1	61
	24	209	1100	ı	15329+15342	I	154=167	ŀ	12	ı	61
	6d	17710 T	^~~f101 ~	-1	15343-15356	1"	168-181	1	13	1	61
	30	211	1102	ŀ	15357=15370	i	182=195	1	14	ı	61
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1 11	284	1 1175	Ĺ	16375-16388	196-209	15	۸5
1 12	285	1 1176	Ţ	16389-16402	210-223	16	45
1 13	286 	1 1177	_l_	16403=16416	224+237	<u> 17</u> j	<u> </u>
1 14	1 287	1 1178	l	16417-16430	238-251	18	45
1 15	1 588	1 1179	1	16431=16444	1 = 14	1 1	46
1 16	1 Sp3	1180	Т	16445-16458	15- 28	2 1	46
<u>i 17</u>	1 290	1 1181		16459=16472	29- 42	3 1	_46 _1
J 18	291	1 1182	1	16473-16486	43- 56	4	46
1 19	1 535	1 1183		16487-16500 J	57- 70	5 1	46
1 50	593	1 1164	ł	16501=16514	71 = 84	6 1	46
<u>ı</u> 21	1 294	1185	1	16515-16528	85= 98	7 j	46
1 55	1 295	1186	Ţ	16529-16541	99-111	8 1	46 -
1 23	296	1187	1	16542-16555	112-125	9 (46
1 24	1 297	1188	1	16556-16569	126-139	10	66
_ I 25	1 598	11¤9		16570-16583 J	140-153	11	46
1 56	1 299	1 1190	1	16584-16597	154=167	12	46
<u> </u>	1 300	<u> 1191 </u>	1	16598-16611	168-181	13	66
1 58	1 301	1192	1	16612-16625	182-195 T	14	46.
1 29	1 302	<u>ı 1193</u>		16626-16639	196-209	_ 15 լ	66 I
1 30	1 303	1194	1	16640=16653	210-223	16 [46
1 31	1 304	1195	L	16654=16667 I	224-237	17	46

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- 1		FI IGHT	I SPACECRAFT	, ,		CYCLE I
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	* * = = * > =					
	305		<u> 16668-16681 </u>	<u> 238=251</u>	18	. 4 <u>6</u>
ا ج ا	306 1		1 16682-16695	! 1= 14 i		<u>67</u>
_13_1	307	1198	L 16696-16709	L15• 28L	2	67_1
1 4 1	308	1199	16710-16723	1 29= 42 1	3	6 <u>7</u>
51	309	1200	<u> 16724-16737</u>	<u> 43• 56 </u>	<u>4</u> l	L 671
6	310	1201	16 <u>738=16751</u>	i 57 - 70 i	5 (1 47 H
7 1	<u> 311 </u>	1202	<u> 16752-16765</u>	<u>i 71</u> - 84	6	1 47 1
1 8 1	312 1		, 10.00	I ઠે5 • 9 ઠા	7	67
9	313	1204	<u> 16780-16792</u>	99-111	8	L £7 L
10	314	1205	16793-16806	112-125	9	67
11 1	315	1206	<u> 1</u> 6807-16520	<u> 126-139</u>	10	إ 72 إ
12	316	1207	16821=16×34	140-153	11	4Z
11_31	1.317.1	<u>1</u> 208	<u>⊥ 1</u> 6835 <u>-1</u> 6×48	<u>154•167</u>	.12	. 47
14	31៦	1209	16849-16862	168 ~181	13	67
<u> </u>	<u> 319 </u>	1210	<u>l. 16863-16876</u>	182 ~ 195	14	L 7 1
16	320	1211	16877-16390	196-209 (15	ı 47 l
17	321	1212	<u> 16891=16904</u>	<u> 210=</u> 223	_ 16_ !	67
18	322	1213	1 16905-16918	224-237	17	ر ۲
19 1	353	1214	1 16919-16932	238 - 251j	18_	671
20	324	1215	16933-16946	1 - 14	1	84
21	325	1216	1 16947-16960	15- 28	2	<u>8</u>
22	326	1217	16961-16974	29- 42	3	48
23	327	1218	16975-16988	43= 56 j	4	
1 24	358	1219	16989-17002	57 = 70	5	8.
25	329	1220	17003 <u>-17</u> 016	71 = 84	. 6	48_ <u>i</u>
76	330	1221	17017-17030	85-98	7	.8 i
27	331	1222	17031-17043	99-111	8	48
28	335	1223	17044-17057	112-125	9	84
29	333	1224	17058-17071	126-139	10	84
30	33#	1225	17072-17085	140-153	11	

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1 1	335	1226	17036-17099	154-167	12	ا 8ء	<u></u>
1 2	336	1227	1 17100-17113	168+181	13	48	l
, 3	337	1228	17114-17127	182-195	14	48	<u> </u>
4	338	1229	17128-17141	196-209	ī 15 ī	ا 8،	I
5	339	1230	17142-17155	210=223	16 j	ر 8 ا	<u> </u>
1 6	1 340	1231	17156-17169	224-237	17	48	1
ì ĩ	341	1232	17170-17183	238-251	18	8	L
1 5	342	1233	1 17184-17197	1 - 14	1 1	د9 ا	1
i 9	343	1234	17198-17211	15- 28	2 1	<u> </u>	1
1 10	1 34#	1235	17212=17225	29= 42	3 ;	49	1
1 11	345	1236	i 17226-17239 j	43= 56	4 <u> </u> [49	
12	346	1237	17240-17253	57- 70	5 1	<u> </u>	Ē
13	347	1238	1 17254-17267	71= 84	6 1	49	1
1 14	1 348	1239	17268-17281	a5= 98	7	49	
i 15	349	1240	17282-17294	99-111	8	۷9	<u> </u>
1 16	350	1241	17295-17308	112-125	9	9۵	I
1 17	351	1242	17309-17322	126-139	10	49	1
i is	352	1243	1 17323-17336	140-153	11	49	l
19	353	1244	17337-17350	154-167	12	49	<u></u>
1 20	354	1245	17351-17364	168-181	13	49	1
21	i 355	1246	17365=17378	182-195	14 1	49	<u> </u>
1 55	356	1247	17379-17392	196-209	15	49	-
i 23	357	1 1248	17393-17406	210-223	16 (49	<u></u>
1 24	358	1249	17407-17420	224-237	17	٤9	1
25	359	1250	17421=17434	238-251	18 [49	1
1 26	360	1251	1743b=17448	1 = 14	1 1	70	i
27	361	1 1252	17449=17462	15- 28	<u> </u>	70	1
1 58	1 362	1 1253	17463-17476	29= 42	<u> </u>	70	ļ
į 29	363	1 1254	1 17477-17490	43- 56	4	70	1_
1 30	364	1 1255	1 17491-17504	57 = 70) 5 ₁	70	1
j 31	365	1 1256	17505-17518	71 - 84	1 6 1	70	<u>L_</u>
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	CMT I	Fillunt I	SPACECRAFT	KEFERENCE	1 055 1	<u>-</u>
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1 1	1_1	12571	17519=17532	85= 98	1 7_1	7 0
2	2	1258	17533-17545	99-111	8 1	70
31	3 1	1259i_	. 17546=17559		19 1	70
4	4 [1260	17560-17573	126-139	ı 10 ı	70
5 1	5 (1261	<u> 1</u> 7574-1758 <u>7</u>	<u> </u>	111_1	7.0
6	6	1262	17588-17601	154-167	12	70
<u> </u>	<u>7_</u> _l	<u> 12</u> 63 _ J	_17632-17615			70
8	δ į	1264	17616-17629	142-195	1 14 1	70
<u>9</u> i	9 1	1265	<u> 17630-17643</u>	196-209	<u></u>	
10	10	1266	17644-17657	210=223	1 16 1	70
<u> </u>	11 _1	1567	_1765 5=17 671	224=237	J 17 L	70_
12	12	1268	17672-17685	238-251	18	70
13	13_!	12691	17686-17699	1 - 14	1 <u>1</u> 1	71
14	14	1270	17700-17713	15~ 28	1 5 1	71
<u>1</u> 5	15	1271	_17714-17727 _	29= 42	1, 3 1	71
16	16	1272	17728=17741	43* 56		71
17	<u> </u>	1273	_17742=17755_ 17756=17769	1 57 70 1 71 84	1 5 1	$-\frac{71}{71}$
	18 19	1274 1275	17736=17783	/1= 04 85= 98	6 7	71
19			17784-17796	<u> </u>		7 1
20 21	20 21	1276	17797-17810	,	1 6 1 1 9 1	71
	55	<u>1277 (</u> 1278 (17811-17824	112-125 126-139	1 10 1	71
53 55	53	1279	17825=17838	140-153	10 1	71 71
24	23 24	1260	17839+17852	1 154-167	1 12 1	71
25	25	1281	17853-17866	168-181	13	71
56	26	1282		182=195	⊥±≥ 1. 14	71 71
27	27	1283	17881=17894	1 196-209	15	71
28	58 -	1284	17895-17908	210-223	16 1	71
59	53	1285	17909-17922	1 224-237	1 17	71
30	30	1286	17923-17936	238-251	1 18 1	
31	31	1287	17937-17950	1 1= 14	1 1	. 72


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	<del></del>	GMT	FIIGHT	I SPACECRAFT !	REFERENCE I	REF I	CYCLE I
' '	PATE	DAY	DAY	BRBITS I	ORBITS	DAY	Na I
	/AIF	<u> </u>					
,	4	32 1	1288	1 17951-17964 1	15- 28	2 1	721
	2	33	1289	1 17965-17978	29* 42	3 1	72
!	3	34	1290	1 17979-17992	43= 56	L4 L_	72 _!
	4	35	1291	17993-18006	57- 70	5 I	72
- ;	5	36	1292	18007-18020	71 - 84	6 1	72
	6	37	1293	18021-18034	85- 98	7	72
1	7	38	1294	18035-18047	99=111	[8]	72
1	<del>-</del>	39	1295	18048-18061	112-125	9 1	72
l Ł	9	40	1296	18062-18075	126-139	<u> 10 L</u>	72
	10	41	1297	18076-18089	140*153	j 11 j	72
- ;	11	42	1298	18090-18103	154-167	12 1	72
	12	43	1299	18104-18117	168-181	13	72
- 1	13	44	1300	18118-18131	182-195	<u>  14                                   </u>	<u>72 _  _</u>
	14	45	1301	18132-18145	196=209	i 15 i	72
i	15	46	1302	18146-18159	210-223	<u> 16 1</u>	<u> </u>
<del></del>	16	1 47	1 1303	18160-18173	224-237	17 L	72
•	17	48	1 1304	18174-18187	238-251	<u>  18  </u>	72
<del>- ;</del>	18	1 49	1 1305	1 18188-18201	1= 14	1 1	73 4
1	19.	50	1306	18202-18215	15- 28	1 5 1	_ <u>73</u>
<del></del>	20	51	1307	18216-18229	29- 42	3 1	73
i	21	52	1308	18230-18243	43= 56	1 4 1	73 I
<del></del>	22-	<u>i 53</u>	1309	1 18244-18257	57 <b>-</b> 70	1 5 1	73
ı t	53	, 54	1310	18258-18271	71-84	1 6 1	<u> 73 L</u>
	24	55	1311	18272-18285	85- 98	1 7 1	73
i	25	56	1312	18286=18298	99-111_	1 8 1	<u>73  </u>
<del></del>	56	<del>i</del> 57	1313	18239-18312	112-125	1 9 1	73
į	27	; 58	1 1314	18313-18326	126=139	10	73
<del></del>	28	59	1315	18327-18340	140-153	11	73
i	29	i 60	1316	18341=18354	154-167	1 .15 1	73
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11	<u> </u>	1.317	]_18355 <b>-</b> 18368_ <u>_</u> _	1 <u>68=1</u> 21.	I. 13 I	73
1 2	62	1318	18369+18382	182-195	14 (	73
1 3	63	<u> 1319</u>	1_18383-18396_[	196-209	15 (	_ 73 _
1 4	6#	1320	18397-18410	210-223	15 1	73
<u> 5</u>	<u> 65 </u>	1321	<u>  18411-18424  </u>	<u> 224=237</u>	<u> </u>	7 <u>3</u>
1 6	1 66 1	1322	18425-18436	238-251	18	73
7	<u> 67_</u>	1323	: 18439-1845 <u>2 :</u>	1=14	L 1 L	74
l g	68	1324	18453=18466	15= 28	1 2 1	74
, 9	69	1325	<u>  18467=18480  </u>	29- 42	<u> 3</u> 1	2 ⁴
1 10	Į 70 i	1326	18481-18494	43= 56	l 4 t	74
1 11	<u> 71 </u>	<u> 1</u> 327	18495 <b>-</b> 18508	<u>57=</u> 70	I 5 I	.74
1 12	72	1328	18509-18522	71 = 84	[ 6 j	74
1 13	<u> 73</u>	<u> 1329 _ </u>	<u>  1</u> 8523 <u>-18536  </u>	85 <b>-</b> 98	<u> </u>	7生
1 14	74	1330	18537 <b>-</b> 18549	99•111	1 8 1	74
1 15	<u>75</u>	1_331	<u> _18550-18563  </u>	112-125	j 9 j	74
1 16	76	1332	18564-18577	126=139	10	74
i 17	77	1333	<u>  18578-18591  </u>	<u>140-153</u>	<u> </u>	74
1 18	78	1334	18592-18605	154-167	12	74
19	79	<u>1 1335</u>	<u>  18606-18619  </u>	<u> 168-181</u>	L13 _L	74
1 50	ا 80	1 1336	18620-18633	182=195	14	74
21	81	1337	1 18634-18647 I	<u> 196-209</u>	115 1_	
52	82	1 1338	18648-18661	210-223	16	74
i 83	i 83	1339	18662-18675	224=237	1 17 1	74
1 24	84	1 1340	18676-18689	238-251	18 (	74
25	։ լ გ5_	1341	<u> </u>	1-14	.l 1 .l.	75
26	86	1342	18704-18717	15= 28	1 5 1	75
i 27	i 87	1 1343	18718 • 18731 i	29- 42	L _3 _1	75
28	88	1344	18732-18745	43 - 56	1 4 1	75
29	89	1 1345	18746-18759	57 <del>-</del> 70	1 5 1	75
30	ı 90	1 1346	i 1876∪-18773 i	71 = 84	6 1	75
31	91	1347	18774-18787	85 - 98	7 1	75

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1 1	92	1348	18788-18800	99-111	8	<u> 75_ 1</u>
1 2	93	1349	18801-18814	112-125	ı 9 ı	75 ]
1 3	<u>94_</u> [	1350	18815=18328	126-139	10 1	75 _
1 4	95	1351	18829-18842	140-153	11	75
<u>ı 5</u>	96 j	1352	18843-18856	154-167	12 1	75 j
6	97	1353	18857-18870	168-131	13 !	75
	[ <u>    98                                </u>	1354	18871=18884	182-195	14	. 75 j
<u> </u>	99	1355	18885 <b>-</b> 1889d	196-209	15 1	75 j
9	100	1356	18899-18912	210-223	16 i	75
1 10	101	1357	18913-18926	224-237	17	75
[ 11 ]	102	1358	18927-18940	238-251	18	75
12	103	1359	18941-18954	1 - 14	1 1	76
13	104	1360	18955-18968	15* 28	3 1	76
14	105	1361	18969-18982	29= 42	3 1	76
1 15	106	1362	18983-18996	43= 56	4	76 j
16	107	1363	18997-19010	57= 70	5	76 I
17	108	1364	19011-19024	71 - 84	6	76
- 18	109	1365	19025-19038	85- 98	7	76
<u>ı</u> 19 j	110	1366	19039-19051	99-111	8	76
1 50 1	111	1367	19052-19065	112-125	9 i	76
1 21 1	112	1368	19066-19079	126=139	10	76
1 55 1	113	1369	19080-19093	140-153	11	76
1 53 1	114	1370	19094-19107	154-167	12	76
1 24 1	115	1371	19108-19121	168-181	13 (	76
I 25 I	116	1372	19122-19135	182-195	14	76 j
1 50 1	117	1373	19136-19149	196-209	15	76
<b>1 27</b> 1	118	1374	19150-19163	210-223	16	76 j
1 58 1	119	1375	19164-19177	224-237	17	76 1
1 29 1	120	1376	19178-19191	238=251	18	76 j
1 30 1	121	1377 -	19192-19205	1-14	1 1	77

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	1 122	1378	<u>  19206=19219</u>	15= 28	1 " - 5 1	77
, S	1 123	1379	: 19220+19233 I	29= 42	. 3 I	77
3	1 124	1380	19234-19247	43 - 56	4 1	_77
4	1 125	1381	19248-19261	57 <b>=</b> 70	5 1	77
5	126	1382	19262-19275	71 = 84	. 6 i	77
1 6	1 127	1383	19276-19289	85= 98	7 1	77
, , , , , , , , , , , , , , , , , , ,	128	1384	19290-19302	99-111	8 1	77
1 8	1 129	1385	19303-19316	112-125	9 1	77
i 9	i 130	1386	19317-19330	126-139	10.1	77
1 10	1 131	1387	19331-19344	140-153	1 11 )	77
11	132	1388	19345-19358	154=167	i12 i	<u></u> 77 _
1.5	1 133	1389	19359-19372	168=181	13	77
1 13	1 134	1 390	<u> </u>	182-195	114.1	77
1 14	1 135	1391	19387-19400	196-209	ı 15 ı	77
15	1 136	11392	1_19401=19414	L210=223	16 1	ップ
1 16	1 137	1393	19415-19428	224-237	i 17 i	77
1 17	1 138	1 1394	19429-19442	<u> 238-251</u>	18 1	<u>77_</u>
1 18	1 139	1395	19443-19456		1 1 1	78
1 19	140_	1396	19457-19470	<u> 15- 28</u>	1_2_1	78
1 20	1 141	1 397	19471-19484	29- 42	3 1	78
1 21	142	1 1398	19485-19498	43- 56	<u> 4 1</u>	78
1 55	1 143	1 1399	19499-19512	57- 70	1 5 1	78
1 23	1 144	1 400	<u> 19513-19526</u>	71 - 84	<u> </u>	78_
1 24	1 145	1 401	19527-19540	85- 98	7 1	78
25	146	1402	<u>  19541-19553</u>	99-111	I8 -I	78
26	1 147	1 1403	19554-19567	112-125	9 (	78 -8
1 27	1 148	1404	19568-19581	<u> 126-139</u>	<u> </u>	78
1 59	1 149	1 1405	19582-19595	140=153	111	78   78
1 59	<u> 150</u>	1 1406	19596-19609   19646-19603	154-167	<u>i 12 j</u>	-
1 30	151	1407	19610-19623	168 <b>-1</b> 81   182 <b>-1</b> 95	13   14	78 78
<u> 31</u>	1 152	1 1408	19624-19637	1 195-122	J	70

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		153	1409	1	19638-19651	_	196-209	1	15 j	78	<u> L</u>
1	۶	154	1 1410		19652-19665	1	210-223	ł	16 1	78	1
	3	155	1 1411	1_	19666-19679		224-237	1_	17 !	78	Ĺ
1	4	156	1 1412	1	19680-19693	1	238=251	1	18	78	1
	5	157	1 1413		19694-19707	1	1= 14	ì	1	79	1
i	6	158	1 1414		19738-19721	ī	15= 28	T	5 1	79	1
ــــٰـــ	7	159	1415	i	19722-19735	i.	29= 42	.i.	3 1	<del>√</del> 9	i
ī	ь	1 160	1 1416			Ī	43* 56	1	4 1	79	1
	9	161	1 1417	i	19750-19763	Ì	57- 70	i	. 5 i	79	i
1	10	1 162	1 1418	1	19764-19777	ī	71 = 84	1	6 i	79	1
Ì	11	1 163	1419		19778-19791	ì	85= 98	i	7 i	79	i
Ī	12	164	1 1420		19792-19804	Ī	99-111	1	8 1	79	i
لــــــــــــــــــــــــــــــــــــــ	13	165	1 1421	i	19805-19818	ĺ	112-125	i	9 i	79	i
1	14	166	1 1422	1	19819-19832	_i_	126-139	ī	10 i	79	ī
_ i	15	167	1 1423	i	19833-19846	i	140-153	Ĺ	11 i	79	i
1	16	168	1424	1	19847-19860	T	154-167	1	12	79	1
ı	17	169	1 1425	i	19861-19374	Ì	168-181	ì	13 i	79	i
1	16	170	1 1426	ī	19875-19888	1	182-195	ī	14 1	79	1
i	19	171	1427	1	19889-19902	į	196-209	ì	15 i	79	ì
	20	172	1428	ī	19903-19916	1	210-223	ì	1 ₀ I	79	Ť
1	21	173	1 1429	1	19917-19930	Ī	224-237	i	17 T	<u>ور</u>	í
1	55	174	1430	1	19931-19944	j	238-251	÷	18 1	79	<del>i-</del>
1	23	1 175	1 4431	Ĺ	19945-19958	ì	1 - 14	į	1 1	RQ.	i
T	24	176	1 1432	Ť	19959-19972	T	15= 28	Ť	· 2 i	₽Q.	ŤΤ
_ 1	25	177	1 1433	- 1	19973-19986	1	29- 42	1	3 1	¥0	i
Ī	26	178	1434	Ţ	19987-20000	ī	43= 56	i	4 1	20	<del>i</del>
1	27	179	1435	ĺ	20001-20014	i	57- 70	i	5	×0	i
Ī	28	180	1436	Ī	20015-20028	Ť	71 - 34	Ī	6 1	P 0	Ť
- 1	29	181	1437	1	20029-20042	i	85= 98	i	7 1	80	i
$\overline{}$	30	182	1438	<del>-</del> -	20043-20055	Ť	99-111	÷	8 1	RQ	<del>'</del>
<u>.</u>						. <del>-</del> .		<u>-</u> -			-
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<u> </u>	1 183	1439 1	<u>_</u> 20056 <b>-</b> 20069	112-125	ـاـ 9	<u>"</u> яО ] _
	184	1440	20070=20083		ι 10 ι	ន0 1
13	185	<u> </u>	_2003 <b>4+</b> 20097_	140-153		k0 _1
4	186	1442	2009a=20111		12 1	۱ 0a
<u> 1 5 </u>	<u> 187                                   </u>	1443	20112=20125	<u> 168=181                                   </u>	113	
1 6	188			, _	1 14 1	яQ I
1 7	<u> 189  </u>	1445	20140-20153	<u>19</u> 6-209	L_15 L.	— ₽Õ —T
ા ક	1 190 1	1446	20154-20167		16 1	۸ <u>0</u> ا
<u> </u>	<u> </u>	1447	<u>20164-20181</u>	224-237	<u> </u>	<u>80</u>
1 10	192	1448		238*251	18	я <b>0</b>
11	<u>193</u>	<u> </u>	L_20196-20209 _	L1 = . 14	11_1.	P1   1
1 12	194	1450	20210-20223	15- 28	1 2 1	81 I
1 13	1 195	1451	20224-20237	59- 45		81
1 14	1 196	1452	,		1 4 1	<b>≈1</b>
15	197			j 57 <b>-</b> 70		g1
1 10	1 198	1454	20266-20279	71=84   85=98	6     7	81   81
1 17	1 199	1 4 5 5	1 20280-20293 1 20294-20306	99=111	! <u> </u>	<u> </u>
1 18	1 200	1 456 1 457	1 20307-20320	112-125	1 0 1 1 9 1	×1   21
1 20	1 505	1458	2030 <u>7</u> -203 <u>2</u> 0_ ı 20321 <b>-</b> 20334	126 <b>-1</b> 39	1 10 1	<u>*</u>
1 51	1 503	1 459	1 20335-20348	140-153	111	81 I
1 55	1 204	1460	20349-20362	154=167	12	81 I-
1 23	1 207	1461	20363-20376	168 <b>-</b> 181	13	ži i
1 24	1 509	1462	20377-20390	182-195	1 14 1	<u> </u>
25	1 207	1463	20391-20404	1 196=209	15	91 <u> </u>
1 26	1 208	1464	20405=20418	210-223	16	<u> </u>
i 27	209	1465	20419-20432	1 2 *4 *237	17	<u> </u>
1 <u>58</u>	1 210	1466	20433-20446	238-251	18	£1
29	211	1467	20447-20460	1= 14		22
1 30	1 212	1468		15- 28	5 1	1 Sa
31	213	1469	20475=20488	1 29- 42	3 1	<b>52</b>
	1 447	<u>'</u>	<del></del>		4	

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1	GMT	FI IUHT	SPACECRAFT	REFERENCE	I REF I	CYCLE
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*****	*	****				
1 1	1 214	1 1470	20489-20502	43= 56	1 4 1	×2 1
1 5	215	1 471	20503-20516	57* 70	5 1	£2
1 3	216	1472	20517-20530	71 - 84	6	42 j
1 4	217	1473	20531-20544	85- 98	7 1	1 84
1 5	218	1 474	20545-20557	99=111	8 1	F2
1 6	219	1 475	20558=20571	112-125	1 ⁹ I	£2
1 7	220	1 4476	20572-20585	126-139	10_1	82
8	221	1477	20586=20599 [	140-153	11 1	k5
9	555	1 1478	20600-20613	154-167	12 1	45
1 10	1 553	1479	20614=20627	168=181	13 !	k2 )
<u> </u>	224	1480	20628-20641	182=195	14 1	85 l
1 12	225	1481	20642-20655	196-209	15 I	≥2
1 13	226	1 1482 1	20656-20669	210-223	16 1	×2 j
1 14	227	1 1483	20670-20683	224-237	17 1	#2 ]
1 15	528	1 1484	20684-20697	238-251	18 :	×2
1 16	1 553	1 1485	20698-20711	1- 14	1 1	E E
<u> </u>	1 530	1486	20712-20725	15= 28	. 2 [	R3
1 18	231	1487	20726-20739	29= 42	3 (	£3
19	535	1488	20740-20753	43= 56	4 1	<u>83</u>
1 20	533	1489	20754-20767	57 <b>-</b> 70 (	5 1	g3 j
21	234	1 490	20768 <b>-</b> 20781	71 - 84	6 1	k3
1 55	235	1491	20782-20795	85= 98	7 1	- j ER
<u> </u>	236	1492	20796+20808	99-111	8 (	£3
1 24	237	1493	50809+50855	112-125	9	g3 j
1 25	238	1494	20823-20336	126-139	10 i	£3
1 26	538	1495	20837-20850	140-153	11	g3
1 27	240	1496	20851-20864	154=167	12 (	į, <b>E</b> s
1 58	1 241	1 1497	20865-20878	168-181	13 i	¥3
<u> 1 53</u>	242	1498	20879-20892 1	182-195	14	я <b>З</b> (
1 30	243	1499	20893-20906	196-209	15	<u>£3</u>
1 31	244	1500	20907-20920 1	210-223 _I	16 !	<b>£3</b>
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DATE	GMT     DAY	FIIGHT	SPACECRAFT   ORBITS	REFERENCE   ORBITS		
DAIF	<u> </u>		UND115 1		- ny : -3	
1	1 245 1	1501	20921-20934	224-237	17	,u3
5	246	1502	20935-20948	238*251 I	18 (	
3	247	1503	20949 <b>-</b> 20962 <u>i</u>	1= 14	1 . i	<u></u>
4	[ 248 ]	1504	20963-20976	15= 28	5 1	<b>24</b>
5	1 249 1	1505	20977-20990	29- 42 1	3_1	84
6	520	1506	20991-21004	43= 56	<u>4</u> 1	R 4
7	T 551 T	1507	21005•21018_ <u>[</u>	57 <u>=</u> 701	5 ι	_ R4
ŏ	252	1508	21019=21032	71 = 84	6 1	ρ4.
9	<u> </u>	1509	<u> 21033-21046  </u>	<u>85 = 98  </u>	7_1	94
10	254	1510	21047-21059	99-111	8 1	24
11 12	<u>  258  </u>   256	1511	<u>21060-21073  </u>	112=125	9	54 _   24
12	1 257 1	1512   1513	21074=21087   21085=21101	126-139   140-153	10 I 11	24 24
14	1 258	1514	21102-21115	154-167	12	
15	259     259	1515	21116-21129	168=181 _	13	, x+ , x4 _
16	1 590 1	1516	21130-21143	182=195 I	14	। .×⊤ . 
17	261	1517	21144-21157	196-209	15	24
18	1 262	1518	21150-21171	210-223	16	
19	263	1519	21172-21185	224=237	17 i	R4
20	26#	1520	21186-21199	238-251	18	24
21	265	1521	21200-21213	1 = 14	1	£5
55	566	1522	21214-21227	15- 28	2	g 5
53	267	1523	21228-21241	29- 42	3	g <b>5</b>
24	268	1524	21242-21255	43- 56	4 1	g 5
25	269	1525	21256-21269	<u>57≈ 70 l</u>	<u>5_</u> _ı	<u> </u>
26	1 270 1	1526	21270-21283	71 - 84	6 1	. £5
27	271	1527	21284-21297	85= 98		<u>.k.5</u> .
58	1 272 1	1528	21298-21310	99-111	ક ા	ı 25
29	1 273 L	1529	21311-21324	112=125 I	9_ı	<u>£</u> 5



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	GMT	FIIGHT	1	SPACECRAFT	REFERENCE I	REF	CYCLE
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1	275	1531	1	21339-21352	140-153 I	11	<b>.</b> 5
5	276	1532	ī	21353-21366	154-167 I	12	<u></u>
3	277	1533	ì	21367-21380	168-131	13	<b>⊬</b> 5
4	278	1534	1	21381-21394	182-195	14 [	~~~`×5
5	279	1535	i	21395-21408	196-209	15	£5
á	780	1536	ì	21409-21422	210-223	16	я5
7	281	1537	į	21423=21436	224 <b>+2</b> 37 (	17	<b>£</b> 5
ĸ	282	1538	Ì	21437-21450	238-251	18	£5
9_	283	1539	1	21451-21464	1= 14	11	R6
10	284	1540	ī	21465-21478	15 <del>-</del> 28	2 1	٤6
11	285	1541	i	21479-21492	29= 42 i	. 3 .	<b>26</b>
12	586	1542	ı)	21493-21506	43= 56	4	۶6
13	287	1543	Ĺ	21507-21520	57 <b>-</b> 70 ∣	5	× 6
14	788	1544	ī	21521-21534	71- 84	6	26
15	289	1545	i	21535-21548	85= 98	7	<b>£6</b>
16	290	1546	Ī	21549-21561	99-111	8	26
17	291	1547	i	21562=21575	112-125	9	26
18	292	1548	1	21576-21589	126-139	10	26
19	293	1549	i	21590-21603	140-153	11	я <b>6</b>
20	294	1550	Ť.	21604-21617	154-167	12	я6
21	295	1551	i	21618-21631	168-181	13 I	<b>я</b> б
55	296	1552	Ī	21632-21645	182-195	14 [	26
53	297	1553	1	21646=21659	196-209	<b>1</b> 5 j	<b>£</b> 6
24	298	1554	ī	21660=21673	210-223	16	86
25	299	1555	i	21674-21687	224-237	17	<b>26</b>
26	300	1556	1	21688-21701	238-251	โช	26
27	301	1557	1	21702-21715	1- 14	1	۶7
28	305	1558	T	21716-21729	15= 28	2 1	£7
29	303 j	1559	1	21730-21743	29= 42	3 1	٤7
30	304	1569	ī	21744-21757	43= 56	4	g7
31	305	1561	i	21758+21771	57 <del>-</del> 70 i	5 (	۶7

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1	GMT	FI IGHT	SPACECRAFT	KEFFRENCE	REF	CYTLE
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	<u>  306  </u>	<u> 1562 </u>	<u> </u>	71 <b>-</b> _ 84	l	271
) 5	1 307	1563	21786-21799	85 <b>=</b> 98	7	27 I
1 3	1 308 1	<u>1</u> 564 1505	21800+21812 <u> </u>   21813 <b>-</b> 21826	99 <b>-</b> 111 _ 112 <b>-</b> 125	L - 8 - 1	<u>8</u> 7 L
5	310	1566	21827=21840	126-139	1 10	87 I
6	311		21841=21854	140=153	111	87 i
i 7	312	1568	21855=21868	154-167	12	Ŕ7
1 8	313	1569	21869=21482 1	168=181	13	87 i
9	314	1570	21883-21896	182-195	1 14 1	و 7
1 10	315	1571	21897-21910	196-209	15	
i 11	316	1572	21911-21924	210=223	. 16 i	g7 j
1 12	317	1573	21925-21938	224-237	i 17 i	27 . 1
13	<u>j 318 j</u>	1574	21939-21952	238-251	<u>1_8_i</u>	<u>87i</u>
1 14	319	1575	21953-21966	1 - 14	1 1	28 J
<u>15</u>	1 350 T	1576	<u>  21</u> 967 <b>-</b> 21980	15 <b>-</b> 28	1 2 1	_ 8a
1 16 ~	321	1577	21981=21994	29= 42	1 3 1	28 J
117	1 355 l	1578	<u>  21935-22008  </u>	43= 56	4 1	<u> </u>
į 18	1 353 1	1579	55008-55055	57- 70	j 5 j	8 <u>8</u>
19	32#	1580	58053 <b>-</b> 55039	71= 84	<u> </u>	<u> </u>
1 50	1 325	1581	22037-22050	85 + 98	7 1	28 I
1 21	1 326 1	1582	55021-55063	99-111	1 8 1	<u> 88  </u>
1 55	327	1583	22064-22077	112=125	1 9 1	≅8  -
1 23	1 328 1	1584	22078-22091	126-139	<u>i 10 i</u>	<u>88  </u>
1 24	1 329	1585	22092-22105	140-153	11	88   
25	1 330 j 1 331 j	<u>1586</u> 1587	<u>  22106+22119  </u>   22120 <b>-</b> 22133	154=167 168=181	12_1	<u>88</u>
1 27	1 335 1	1507 1548	22134=22147	182=195	j 13 (   14	¥0 ↓ ≅8 ↓
1 28	1 333 1	1589	22148=22161	196-209	<del>                                  </del>	<u> </u>
1 29	1 335 1	1590	22162=22175	210-223	16	28 I
1 30	335	1591	22176-22189	224-237	17 1	
j 30	255		051/0.00107			

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_1	DATE	I DAY	I DAY	L	0RBIIs	1	aRBITS	1	DAY	Ne _t •	<u> j</u>
-				-							-
1	1	336	1592	1	<u> 22190-52203</u>	L	<u> 238-251</u>	1	18	8	上
- 1	2	337	1593	1	22204-22217	1	1 - <u>1</u> 4	ŀ	1	! £9	1
. 1	3	<u> </u>	1594	1	<u>_22218=22231</u>	L.	15•_28	. L_	<u> 2</u>	<u> 29</u>	_ ل
- 1	4	339	1595	1	22232-22245	ļ	29- 42	1	3	, ş9	1
	5	340	1596		22246-22259	L	<u>43= 56</u>		4	<u> </u>	1
ŧ	6	341	1597	ī	22260-22273	Ī	57- 70	T	5 1	£9	1
_!	7	1 342	<u>  1</u> 598	_[_	_22274=22287_	1	71 + 84	_]_	6	_k9	1
į	8	343	1599	1	22238#22301	Ī	85= 98	Ī	7 1	- E.9	1
	9	344	1600	L	22302-22314	1	99-111	1	8 1	<u> ×9</u>	1
į	10	345	1601	ī	22315-22328	Γ	112-125	1	9 !	9ء	T
- }	11	346	1602	1	22329-22342	1	126-139	1	10 I	£9	ł
ı	12	347	1603	ī	22343-22356	Ï	140-153	ī	11	₽9	ı
	13	348	1604	1	22357-22370	١	154-167	1	12 1	<u>89</u>	1
ī	14	349	1 1605	ī	22371-22384	Ī	168-181	ī	$-\frac{13}{13}$	9	Ī
1.	_ 15	350	1606	1	22385-22398	ı	182-195	1	14 1	22	Ĺ
$\overline{}$	16	351	1 1607	ī	~22399 <b>-</b> 22412~	ī	196-209	1	_15_1	49	1
ł	17	352	1608	İ	22413-22426	ı	210-223	i	16 1	я9	í
1	18	353	1609	ī	22427-22440	i	224-237	ī	17 i	٤9	i
1	19	354	1610	1	22441-22454	1	238-251	i	18 _I	۶9	i
ī	50	355	1611	Ī	22455-22468	1	5 - 14	1	1 1	90	Ť
1	21	356	1612	ı	22469-22482	ſ	15= 28	i	2 i	90	í
ī	55	357	1613	ī	22483-22496	ì	29= 42	i	3 i	9.0	1-
Ĺ	23	358	1614	i	22497-22510	ĺ	43- 56	i	4 i	яÖ	í
ī	24	359	1615	Ť	22511-22524	ī	57- 70	<del>-</del> i	5 j	90	<del>Í</del>
i	25	360	1616	i	22525-22538	ĺ	71 = 84	í	6 i	90	í
ī	56	361	1617	Ì	22539-22552	Ĺ	85- 98	÷	<del>-</del>	90	<del></del>
ì	27	362	1618	i	22553-22565	ĺ	99-111	í	8 i	90	i
1	28	363	1619	ì	22566-22579	i	112-125	i	9 i	90	<del>i</del>
1	<b>2</b> 9	364	1620	i	22580-22593	i	126-139	i	10 i	90	i
ì	30	365	1621	ī	22594-22607	İ	140-153	- <u>'</u>	11 1		<del>:</del>
1	31	366	1622	i	22608-22621	i	154-167	i	12	40	ì
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## APPENDIX C

LANDSAT-1 DOCUMENTS ISSUED THIS REPORT PERIOD

### APPENDIX C

## LANDSAT-1 DOCUMENTS ISSUED THIS REPORT PERIOD

None issued.

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### INTRODUCTION

This is the fifth report in a continuing series of documents issued at launch, and thereafter quarterly, to present flight performance analysis of the Landsat-2 spacecraft. Previously issued documents are:

Document No.	Title	Date
75SDS4214	Landsat-2 Launch and Flight Activation Evaluation Report, 22 to 26 January 1975, Launch through Orbit 50 and Orbit Adjust Operation.	21 March 1975
75SDS4228	Landsat-1 and Landsat-2 Flight Evaluation Report, 23 January 1975 to 23 April 1975.	15 August 1975
75SDS4255	Landsat-1 and Landsat-2 Flight Evaluation Report, 23 April 1975 to 23 July 1975.	10 October 1975
75SDS4266	Landsat-1 and Landsat-2 Flight Evaluation Report, 23 July 1975 to 23 October 1975.	1 December 1975

This report contains analysis of performance for Orbits 3815 to 5100 for Landsat-2.

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SECTION 1
SUMMARY
LANDSAT-2 OPERATIONS

#### SUMMARY LANDSAT-2 OPERATIONS

The Landsat-2 spacecraft was launched from the Western Test Range on January 22, 1975, at 022:17:55: 51.604. The launch and orbital injection phase of the space flight were nominal and deployment of the spacecraft followed predictions. All systems continue normal except Forward Scanner Pressure, Forward Scanner Pressure Telemetry, and Wideband Video Tape Recorder No. 1 (WBVTR-1). The Forward Scanner Pressure had begun leaking before launch but will not affect scanner performance. The Forward Scanner Pressure (Function 1003) telemetry became erratic in Orbit 2244.

WBVTR-1 failed to rewind in Orbit 1021 and had intermittent operation to Orbit 1659 when normal operation was resumed. WBVTR-1 had a new anomaly in Orbit 2863 on August 3, 1975 when ground stations were unable to obtain video sync lockup because of failure of one head to produce video, and WBVTR-1 operations were then discontinued. Tests were made thru Orbit 4893 on 8 January 1976, after which all use of the recorder stopped. Spacecraft performance has not been degraded by these anomalies. Table 1-1 shows cumulative in-orbit payload system performance.

IS-2 1-1

Table 1-1. In-Orbit Payload Systems Performance Launch Thru Orbit 5070 (1/21/76) Landsat-2

	<del></del>	
RBV	Total Scenes Imaged	729
	Avg. Scenes/Day	66
	Total Area Imaged (millions of sq. mi.)	6,4
	ON TIME (hr)	7.8
<b>!</b>	ON/OFF Cycles	55
İ	% Real Time Images	98
}	% Recorded Images	2
1400	m . 10	
MSS	Total Scenes Imaged	63,706
	Avg. Scenes/Day	179
	Total Area Imaged (millions of sq. n. mi.)	55 <b>5.</b> 5
•	ON TIME (hr)	702.6
	ON/OFF Cycles	5351
	% Real Time Images	60
1	% Recorded Images	40
DCS	Messages at OCC	398,082
1	Non-Perfect MSGS	29,073
	Max. DCP's ACTIVE/DAY	110
1	Users	46
ĺ	Avg. MSG/ACTIVE Orbit	158
	ON TIME (hr)	8,632
		•
WPA-1	% Real Time Mode	1
	% Playback Mode	99
J	ON TIME (hr)	86.2
	ON/OFF Cycles	554
WPA-2	% Real Time Mode	60
	% P/B Mode	40
	ON TIME (hr)	552.1
	ON/OFF Cycles	3,441
i		0, 222
WBVTR-1	% Record Mode	38
Ì	% Playback Mode	41
}	% Rewind Mode	20
	% Standby Mode	1
ļ	Mirror Frame Sync Error Count in P/B	< 10
	Time Head-Tape Contact (hr)	105.6
ļ	Cycles Head-Tape Contact	1,693
	ON TIME (hr)	133.6
WBVTR-2	% Record Mode	38
	% Playback Mode	41
	% Rewind Mode	20
	% Standby Mode	1
	MFSE Count in P/B	< 10
	Time Head-Tape Contact (hr)	346.7
	Cycles Head-Tape Contact	4,641
	ON TIME (hr)	439.0
<u> </u>		

## ORBITAL PARAMETERS

LANDSAT-2

#### ORBITAL PARAMETERS

Landsat-2, together with Landsat-1, has continued to provide the ground track repeat pattern required for the nine-day image coverage of the earth. During this report period, the ground track of Landsat-2 has been maintained, as required, within 10 NM longitude error at the equator. This has been done by controlling the ACS pitch gates through the use of pitch position bias mode. (See Section 4 also.) Therefore, no orbit maintenance burn of the OAS was required during the current report period.

The error in longitude since launch as a function of time and orbit maintenance burns is shown in Figure 2-1. Figure 2-2 shows the change in sun time at the descending equatorial crossings.

As of 23 January 1976, Landsat-2 has descending equatorial crossings at approximately 9:28 AM local time as opposed to 9:07 AM for Landsat-1. A projection of the variation of local mean time at the descending nodes for both spacecrafts is given in Figure 2-3.

The Brouwer Mean Orbital Parameters for Landsat-2 are given in Table 2-1. Appendix B gives ground trace repeat cycle predictions.

Table 2-1. Landsat-2 Brouwer Mean Orbital Parameters

Element Date	Apogee (KM)	Perigee (KM)	Inclination (Deg )	Semi-Major Axıs (KM)	Eccentricity	Two Body Period (Min)	Nodal Period (Min)	Argument of Perigee (Deg)	Right Ascension (Deg)	Mean Aromaly (Deg)
25 Jan 1975 ¹	915 03	901 56	99 095	7286 462	0 000925	103 165	-	272 852	86 637	139 578
6 Feb 1975 ²	916 84	898 47	99 096	7285 820	0 001260	103 151	-	256 040	99 347	134 523
24 Apr 1975	917 85	897 40	99 079	7285 788	0 001403	103 151	103 266	62 55	174 339	117 183
25 July 1975	917 45	897 68	99 071	7285 733	0 001356	103 150	103 265	166 118	264 891	13 726
23 Oct 1975	916 70	898 49	99 059	7285 762	0 001250	103 150	103 266	282 749	353 366	257 271
24 Jan 1976	917 36	897 81	99 046	7285 754	0 001342	103 150	103 266	31 621	84 584	148 179

¹ Post launch

² After the sequence of phasing maneuvers completed in Orbit 212

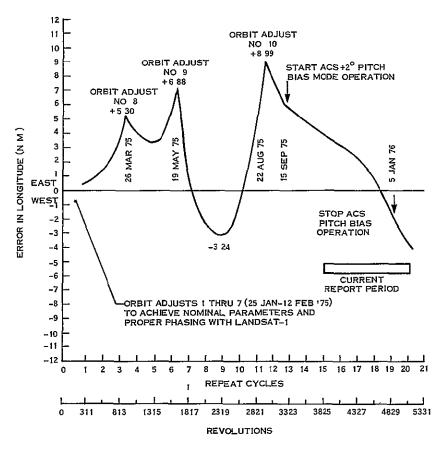


Figure 2-1. Effect of Orbit Adjusts on Landsat-2 Ground Track

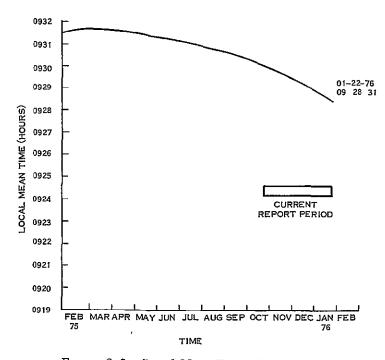


Figure 2-2. Local Mean Time of Descending Node

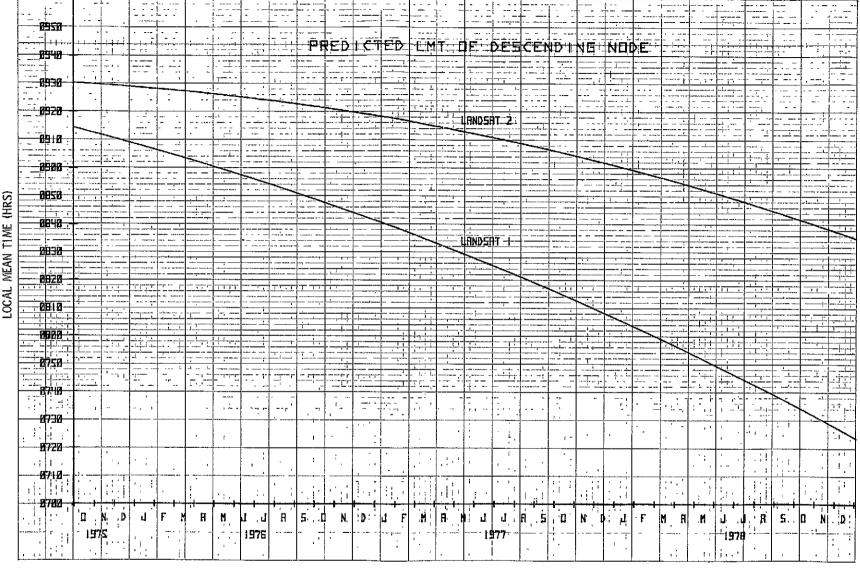


Figure 2-3. Predicted Limit of Descending Node

POWER SUBSYSTEM (PWR)

LANDSAT-2

#### POWER SUBSYSTEM (PWR)

The Power Subsystem on Landsat-2 has performed well throughout this report period. The solar arrays have continued to provide excess energy above spacecraft and payload requirements and are expected to fully support the Landsat-2 mission beyond 1976. The batteries and the subsystem electronics have also shown very good performance during this report period.

The percentage degradation of the arrays is plotted as a function of days in orbit in Figure 3-1, along with the pre-launch predicted array degradation. The array degradation during this report period has been slightly higher than predicted. The projected values of midday array current are plotted in Figure 3-2. Here the array current is adjusted for sun intensity and array degradation, as well as sun angle. Along with the same curve is plotted the actual telemetry values observed until the end of the current report period.

During Orbit 3971 (3 November 1975) Landsat-2 passed through the partial solar eclipse over the Southern Hemisphere. Real time adjustments to the auxiliary loads were made to compensate for the loss in array energy.

The battery packs averaged a typical 9.0-10.0% depth of discharge (DOD) during this report period but has peaked as high as about 16% during nights, with long WBR playbacks. Compensation loads have been reduced to minimize the peaks in DOD, leaving only loads 3, 4 and 8 on at the end of the current report period. (See Table 11-2 for a history of compensation load switchings since launch.) Battery temperature spread ranged from 5.0 to 8.5°C and is expected to be in the lower range during the on-coming period of lower sun intensity. Charge and load sharing of individual batteries have been satisfactory. Battery voltages have been maintained within suitable limits with Landsat-2 power management procedures, excess array energy being dissipated through auxiliary loads.

The power subsystem electronics have performed extremely well during this report period with all regulated voltages stable. Table 3-1 shows major subsystem parameters and Table 3-2 shows power subsystem telemetry for selected orbits. Some parameters in Table 3-1 may be slightly different from those in Table 3-2 because Table 3-1 uses a power management time span (night followed by day), whereas the time span used in Table 3-2 is the playback period from the NBR.

The shunt limiter on Landsat-2 has operated several times since launch and has held the solar array bus voltage at specified levels.

Figure 3-3 shows the actual variation in sun angle to orbit plane and solar panels for Landsat-2. Figure 3-4 is a prediction of the variations of the sun angle through 1977 for Landsat-1 and 2.

LS-2

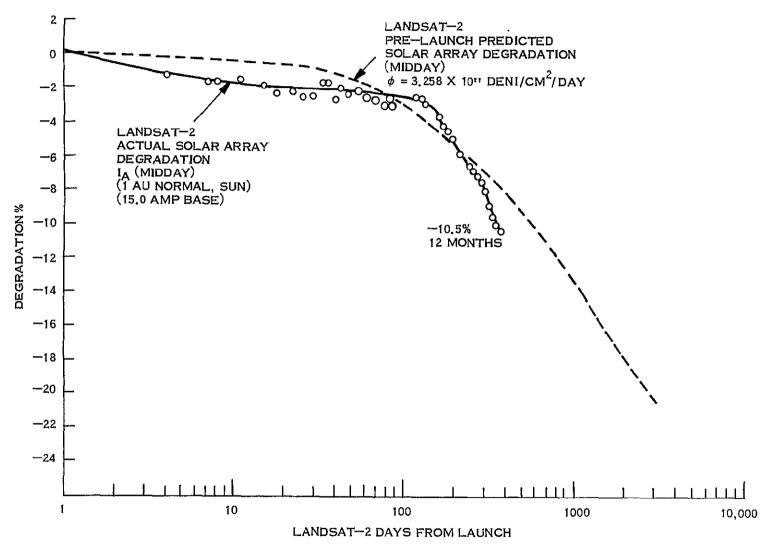


Figure 3-1. Landsat-2  $I_A$  (Midday) Degradation vs. Days

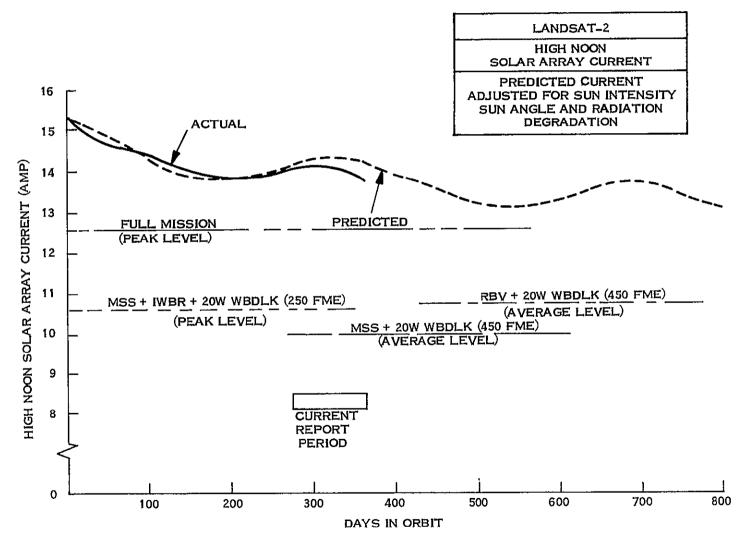


Figure 3-2. Landsat-2 Midday Solar Array Current

Table 3-1. Landsat-2 Major Power Subsystem Parameters

Pwr. Mgmt. Orbit No.	50	1251	2540	3820	4250	4669	5100
Batt 1 Max	33,43	33.08	33,25	33,60	32.91	32.91	32.66
2 Chge	33.40	33,05	33,14	33,48	32.89	32.89	32.63
3 Volt	33.35	33.00	33.09	33,43	32,83	32,92	32.57
4	33,45	33.02	33,20	33, 54	32,85	32,94	32,68
5	33,42	33.08	33,25	33,59	32.91	32,91	32,65
6	33,41	33.07	33.24	33,50	32.90	32.90	32.64
7	33.45	33.11	33.28	33,54	32,93	32.93	32.68
8	33 45	33.10	33.27	33.53	32.93	32.93	32.68
Average	33 42	33.07	33.21	33, 53	32.89	32.92	32.65
Batt 1 End-of-Night	29.32	28,98	29.06	28,89	29.06	28,80	29.06
2	29.38	28.95	29, 12	28.87	29.04	28.78	
3	29.32	28.98	29.07	28,89	29.07		29.04
4	29,34	29,00	29.09	28,91		28.81	29.07
5	29.40	28.97	,	,	29,09	28,83	29.09
6			29.06	28.89	29.06	28.89	29,06
	29.31	28,96	28.96	28.79	28.96	28.79	28.96
7 8	29.34	29.00	29.08	28,91	29.08	28.82	29.08
	29.34	29.00	29.00	28.82	29.00	28,82	29.00
Average	29.34	28.98	29.05	28.87	29.04	28.82	29.04
Batt 1 Chge	12.76	12.36	12.13	12.57	12.76	13,21	12.43
2 Share	11.68	12.24	12,45	12.12	11.77	11.67	11.42
3 (%)	12.24	13,21	13.67	13.62	12,96	13.08	12,48
4	11,99	12.62	12.50	12,34	11.91	12 10	11.76
5	12.84	12.01	11.52	11.83	12.50	12.49	13,24
6	13.35	12.71	13.20	13.02	14.02	13.12	14.32
7	12.90	12.86	12.81	12.83	12.90	13,01	12.97
8	12.24	11,99	11.72	11.65	11.18	11.32	11.38
Batt 1 Load	12.60	11.97	11,35	11.40	11.20	11.50	11.80
2 Share	12,70	14.12	13,99	13.51	13.75	13.44	13.34
3 (%)	12,67	13.14	14.38	13,81	14,43	13.64	13.74
4	12.44	12.57	12.99	12.87	12.84	12.67	12,48
5	12.34	11.59	11,58	11.87	11.92	12.34	
6	12.70	12,10	11.30	11.91	11,33	11.84	12.36
7	12.47	12,42	12.35	12.56			11.56
8	12.04	12.08	12.06	12.08	12.53	12.63	12.70
Batt l Temp	21.46	20.20			12.00	11.94	12.02
2 in			21.34	22.02	21.78	21.82	21.94
3 (°C)	20.25	19.98	21.44	21.02	20.13	19.67	19.94
- ·	18.60	18,22	19.18	18.72	17.79	17.62	17.86
4	20.83	20.73	20.91	20.98	20.15	20.18	20,36
5	24.98	22.11	22,31	23.14	23.66	24.16	27.27
6	24.26	21.78	23.01	23.70	24.28	24,20	27.28
7	24.71	22.59	23,62	24,34	24.66	24.62	26.32
. 8	23.63	22.04	22.71	23.29	23.30	23,40	24.41
Average	22.34	20,95	21.81	22,15	21.97	21.96	23,17
S/C Reg Bus Pwr. (W)	*	161.38	185.0	190.2	147.6	154.7	149.3
Comp Load Pwr. (W)	*	34.06	41.2	41.2	19.4	24.8	24.8
P/L Reg Bus Pwr. (W)	*	9.59	9.6	9.6	9,8	12.6	9.8
C/D Ratio	1,15	1.08	1.10	1,28	1,20	1.24	1.11
Total Charge (A-M)	271.9	250.98	267,55	298.55	248,35	257.99	223,46
Total Discharge (A-M)	237.2	229.67	2 <b>44.</b> 33	233.14	206.73	207.49	201.45
Solar Array (A–M)	1106	1032	981	999	1006	1009	1003
S.A. Peak I (Amp)	16.05	15,37	14,67	14.82	14.74	14.82	14.43
Midday Array I (Amp)	*	14.51	13.88	14.04	14.12	13.96	13.72
Sun Angle (Deg)	*	0.08	~1.22	1.55	2.10	4.84	8.35
Max R Pad Temp (OC)	*	60.80	59.60	64.40	64.40	65.60	63,20
Min R Pad Temp (°C)	*	-38.67	-38.00	-37,40	-36.80	~36.20	-35.00
Max L Pad Temp (°C)	*	57.69	56.92	60.0	62.15	64,31	62.15
Min L Pad Temp (°C)	*	-45.71	-45.00	-44,29	-43.57	-43.57	-42.14
=======================================			70.00	TT, 40	TO 101	- 40.01	五4. 14

^{*} Data not processed and unavailable

Table 3-2. Landsat-2 Power Subsystem Analog Telemetry (Average Value for Data Received in NBTR Playback)

			<u> </u>			Orbits	,	,., <u>.</u>	
Function	Description	Unit	50	1253	2532	3810	4251	4670	5102
6001	Batt 1 Disc I	Amp	1,01	0,89	0.85	0.68	0.87	0.75	0.74
6002	2		1.01	0.97	0,97	0.82	1 04	0.90	0.84
6003	3		1.00	0.97	0,99	0.85	1 06	0.92	0.87
6004	4		1.00	0.93	0.93	0.79	0,97	0,85	0.73
6005	5		0.99	0.86	0.85	0.73	0,91	0,84	0.10
6006	6		1 02	0.90	0,86		0.87	0.80	0 73
6007	7		1.00	0.91		0,72	0.94	0.87	0,80
6008	8		0 97	0.91	0.91	0,77	0.91	0,82	
	-	A	1		0.87	0.74	-		0,75
6011	Batt 1 Chg I	Amp	0.47	0.43	0.57	0.51	0 51	0.45	0,42
6012	2		0.43	0.46	0.57	0.49	0.48	0.40	0,38
6013	3		0,45	0.45	0,61	0.54	0.52	0.44	0.42
6014	4		0 44	0.43	0.57	0 50	0.48	0.41	0.39
6015	5		0.47	0.41	0.54	0.48	0.50	0.42	0.44
6016	6		0.49	0.44	0,60	0.53	0.55	0.45	0.47
6017	7		0.47	0.44	0.60	0,52	0,52	0.44	0,43
6018	8		0,45	0.41	0.55	0,48	0.46	0.38	0.38
6021	Batt 1 Volt	VDC	31.50	31, 18	30.92	31.17	31,06	31,02	31.11
6022	2		31.48	31, 15	30,90	31,16	31,04	31,00	31.09
6023	3		31.49	31,16	30,91	31,16	31,05	31.01	31,10
6024	4		31,49	31,16	30,91	31,17	31,05	31.01	31.10
6025	5		31.50	31,18	30.92	31,18	31.05	31.02	31,11
6026	6	Į	31 49	31, 16	30,90	31,15	31.03	31,01	31.08
6027	7	1	31.52	31,20	30.94	31,20	31.08	31 05	31 14
6028	8		31.49	31, 17	30.92	31, 17	31.06	31.03	31,11
6031	Batt 1 Temp	DGC	21.59	20.23	20,93	22,02	21,74	21.88	21,91
6032	2		20.53	20.05	20.75	20.93	20.14	19,74	19 90
6033	3		18.80	18.30	18.66	18.84	17.80	17,65	17,77
6034	4		20.90	20.75	20.88	21.05	20.17	20,20	20.33
6035	5		25.16	22.15	22 22	23.26	23.59	24.22	27,18
6036	6		24.37	21 79	22 55	23 86	24.24	24.26	27, 19
6037	7		24.83	22,62	23.26	24.36	24.67	24.67	26.19
6038	8						23, 31	23.47	
6040	Rt. Pad Temp	DGC	23.75	22,05	22,52	23,37	1		24.36
			28.96	26.72	26.16	29.31	29.43	30.50	30,90
6041	Rt. Pad VM	VDC	33.72	33.74	33.56	33.51	33.48	33.23	32,86
6042	Rt. Pad VN	VDC	33,46	33.00	33.18	33.25	32.98	32,62	32,44
6044	Lt. Pad Temp	DGC	25,56	21.86	21.16	24.71	24.88	26.38	28,22
6045	Lt. Pad VF	VDC	34 40	33, 99	33.80	33.95	33,94	33.87	33,82
6046	Lt. Pad VG	VDC	34,48	34.09	33.91	34.04	34.03	33,94	33.91
6050	S/C UR Bus V	VDC	31,73	31.41	31,14	31,35	31.30	31.26	31,33
6051	S/C RG Bus V	ADC	24,57	24.58	24,57	24.57	24.57	24,58	24,58
6052	Aux Reg AV	ADC	23,36	23,39	23,40	23.42	23.44	23.44	23 44
6053	Aux Reg BV	ADC	23.37	23,40	23,39	23.39	23.41	23,44	23 44
6054	Solar I	Amp	14.81	14.24	13,76	13,85	13.86	13.74	13.40
6056	S/C RG Bus J	Amp	7,23	6,62	7,17	7.37	6.25	6.24	6,28
6068	PC Mod T1	DGC	21.67	21.42	21.98	22.16	20.28	20.18	20,77
6059	PC Mod T2	DGC	20.44	20.06	20.53	20.68	19,51	19.43	19 56
6070	P/L RG Bus V	VDC	24.61	24.60	24.60	24.60	24,60	24.60	24.60
6071	P/L UR Bus V	VDC	31,85	31,49	31.21	31,44	31.37	31.32	31,40
6073	P Aux AV	VDC	23,47	23.50	23,51	23,49	23.51	23,51	23 51
6074	P Aux BV	VDC	23.46	23,50	23.51	23.50	23.51	23,51	23,51
6075	PR Mod T1	DGC	20.84	20.69	21.39	21.44	20,57	20,14	20,32
6076	PR Mod T2	DGC	22.13	22.01	22.38	22.54	21.91	21.64	21,79
6079	Fuse Blow V	VDC	24.48	24 47	24.48	24,50	24.49	24.47	24,49
6080	Shunt 1 I	Amp	0 0	0.0	0.0	0.0	0.00	0.00	0.00
6081	2		0.0	0.0	0.0	0.0	0.00	0.00	0.00
6082	3	]	0.0	0.0	0.0	0.0	0.00	0.00	0.00
6083	4		0.0	0.0	0.0	0.0	0.00	0.00	0.00
			1				N .		1
6084 6085	5		0.0	0.0	0.0	0.0	0.00	0.00	0.00
6085	6		0.0	0.0	0.0	0.0	0.00	0.00	0.00
6086	7		0.0	0.0	0.0	0.0	0.00	0.00	0,00
6087	8		0.0	0.0	0.0	0.0	0.00	0.00	0,00
6100	P/L RG Bus I	Amp	0.38	0.42	0,80	0.0	0.66	0.48	0.54
Total No.	Major Frames	$\mathbf{Frm}$	396	785	387	384	784	785	785

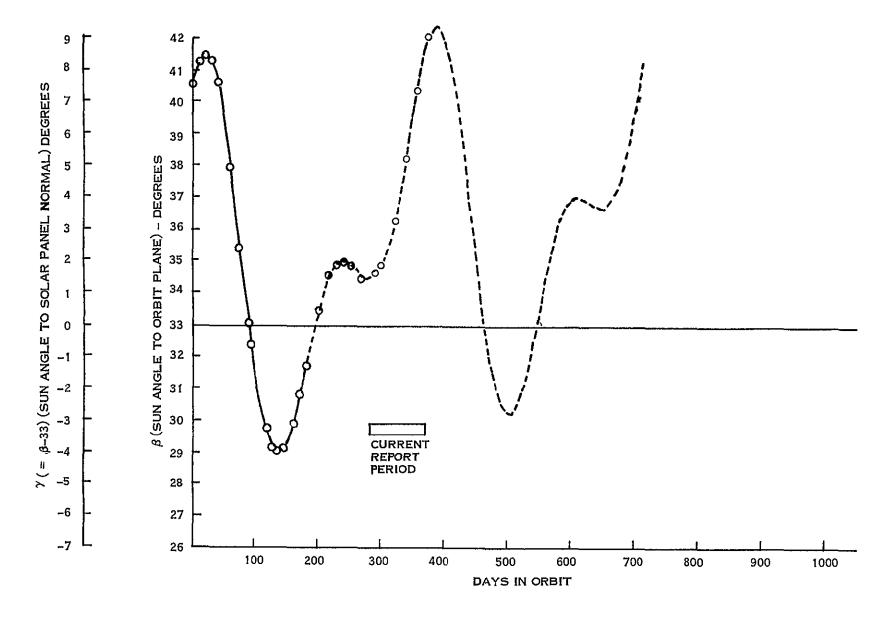


Figure 3-3. Landsat-2 Actual  $\beta$  and  $\gamma$  (Paddle) Sun Angles

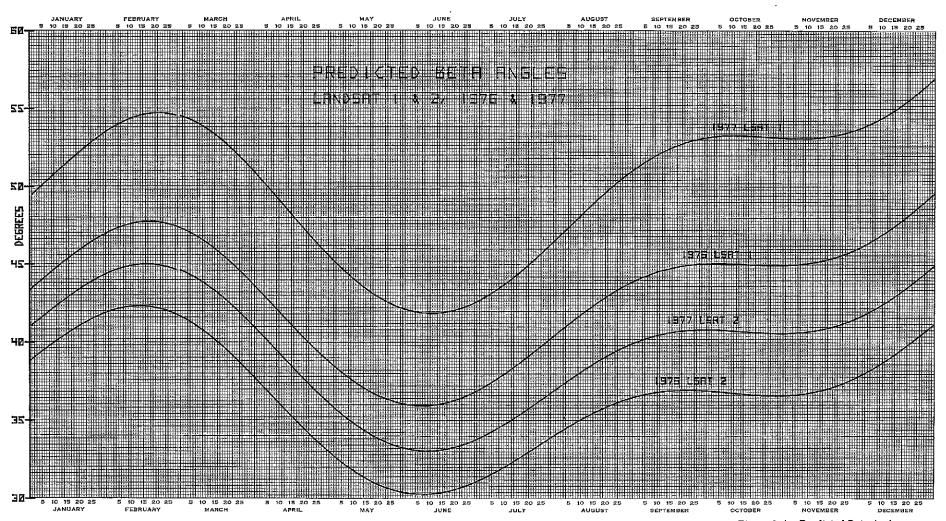


Figure 3-4. Predicted Beta Angles for Landsat-1 and Landsat-2 - 1976 and 1977

### SECTION 4 $\label{eq:approx} \text{ATTITUDE CONTROL SUBSYSTEM (ACS)}$

### ATTITUDE CONTROL SYSTEM (ACS)

Landsat-2's Attitude Control System has been operating properly since launch and has consistently maintained correct spacecraft attitude.

The pressure leak in the Forward Scanner has had no effect on the ACS System's performance.

In mid September (Orbit 3288, 15 September 1975) a program was implemented to control spacecraft ground track drift by limiting the number of pitch gates occurring in each orbit and by assigning them polarity. The ACS system is commanded into the  $\pm 2^{\circ}$  Pitch Position Bias mode during satellite night for specific durations centered about satellite midnight. In addition, the program is implemented in either alternate or successive orbits, depending upon the number of properly polarized pitch gates required to affect the spacecraft's ground track drift and/or drift rate.

Table 4-1 summarizes the sequences maintained to date and Figure 2-1 in Section 2 shows the effects of these sequences on the spacecraft's orbit.

Time Span	Implementation	Duration Centered About Satellite Midnight (Minutes)	Resulting Average Number of Pitch Gates Per Day
15 Sept to 18 Sept	Alternate Orbits	25	5 + pitch`
18 Sept to 12 Oct	Consecutive Orbits	50	2 - pitch
12 Oct to 18 Oct	Alternate Orbits	25	2 to 4 + pitch
18 Oct to 14 Nov	Consecutive Orbits	50	2 to 5 - pitch
14 Nov to 18 Nov	Alternate Orbits	25	2 to 3 + pitch
18 Nov to 18 Dec	Consecutive Orbits	50	2 to 3 - pitch
18 Dec to 5 Jan	Alternate Orbits	25	1 to 2 + pitch
5 Jan to 11 Feb	Discontinued	<b>4-</b>	10 to 11 + pitch

Table 4-1, Landsat-2, +20 Pitch Position Bias Summary

Secondary benefits have also been derived from this effort. The requirements for routine orbit adjusts have been eliminated and freon is being conserved due to the metering effects of controlled pneumatic gating.

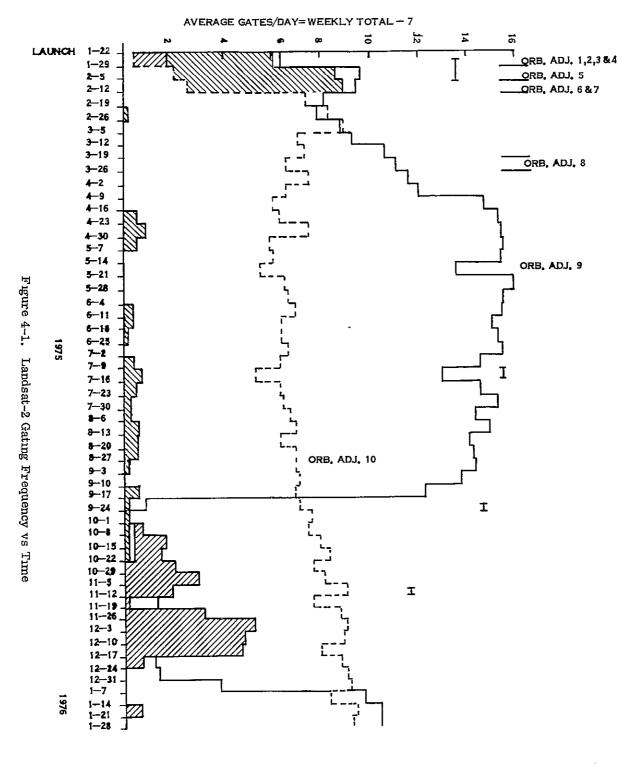
Freon Useable Impulse declined predictably during this report period as shown in Figures 4-1 and 4-2.

RMP 2, commanded into operation shortly after ACS acquisition as the primary control of the yaw subsystem has functioned normally.

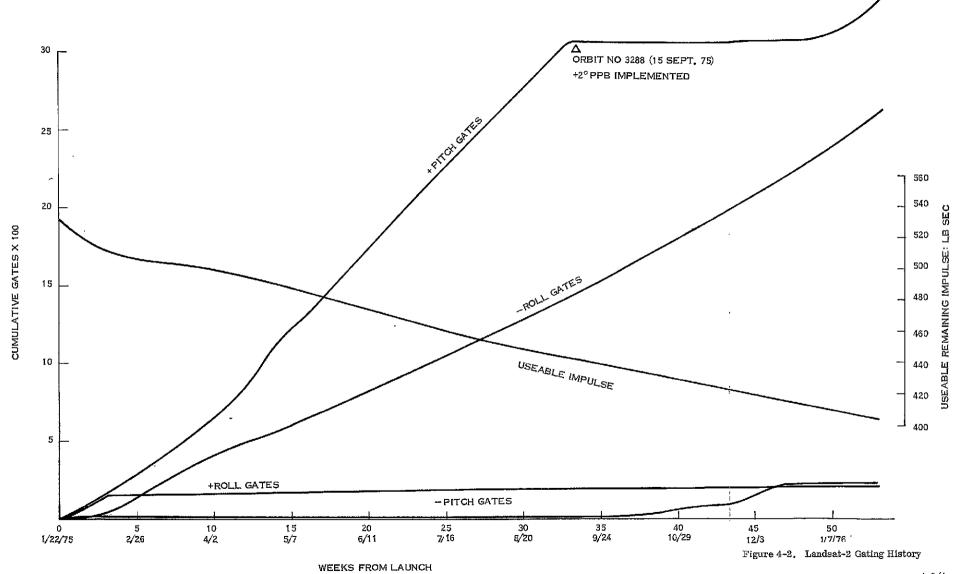
Both Solar Array Drives (SAD) performed normally and maintained proper solar panel alignment with the sun line during satellite day. Motor voltages and temperatures are within specifications.

Typically, flywheel duty cycles have averaged seven percent or less. Pitch and Yaw flywheel speeds have averaged less than -150 RPM while the Roll flywheels have averaged +760 RPM. Sun transient response due to dual scanner mode operation has been similar to Landsat-1 and is normal.

Tables 4-2, 4-3, and 4-4 show typical telemetry for temperatures and pressures; voltages and currents; and attitude errors and driver duty cycles as obtained from SCEST program averages.



(+) PITCH
(+) PITCH
(+) ROLL
(+) ROLL
(+) ROLL
RBV ON



IDLDOUT FRAME Z

Table 4-2. Landsat-2 Subsystem Temperature and Pressure Averages

				•	Orbits			
Function	Units	29	1253	2532	3810	4241	4670	5102
1084 RMP 1 Gyro Temperature	DGC	19 33(1)	21, 15	21 02	22.70	24, 26	23, 83	22,69
1094 RMP 2 Gyro Temperature	DGC	74.00	74,00	74.00	74 02	74.31	74.34	74, 26
1222 SAD RT MTR HSNG Temp.	DGC	19.50	22 24	22.23	23.81	25 16	24.66	22.98
1242 SAD LT MTR HSNG Temp.	DGC	26.87	27 94	27.54	29,36	30,61	30 60	29.79
1223 SAD RT MTR WNDNG Temp.	DGC	21,76	24,31	24,23	25, 75	26.83	26 23	24.36
1243 SAD LT MTR WNDNG Temp.	DGC	30.23	30, 85	30,32	32 28	33, 72	33.74	32, 83
1228 SAD RT HSG Pressure	PSI	7.26	7, 25	7.25	7.25	7, 20	7.22	7,18
1248 SAD LT HSG Pressure	PSI	7.28	7.28	7.27	7, 27	7, 24	7.24	7.21
1007 FWD Scanner MTR Temp.	DGC	22,07	22.72	22,25	23, 82	25, 58	25 33	23.80
1016 Rear Scanner MTR Temp.	DGC	24.19	24.18	23.62	24, 96	26, 31	26.26	25.04
1003 FWD Scanner Pressure	PSI	9.59(2)	2,59	מ	D	D	D	D
1012 Rear Scanner Pressure	PSI	6,21	6.19	6.00	5, 91	5, 82	5, 83	5,62
1212 Gas Tank Pressure	PSI	1948.0	1800, 29	1672.12	1599.60	1590, 78	1559 49	1517.04
1210 Gas Tank Temperature	DGC	20.66	22,66	22.33	24, 13	25, 38	25 33	24, 25
1213 Manifold Pressure	PSI	53.98	54,55	54,83	54.70	56, 76	54 68	54.56
1211 Manifold Temperature	DGC	19.18	20 78	20,50	22, 45	23, 88	23, 73	22.59
1059 CLG Power Supply Card Temp	DGC	39,00	40 00	39.52	41. 11	42, 46	42 41	41,47
1260 TH01 EBP	DGC	24,29	25 31	25.01	26.78	28, 01	28.06	27.21
1261 TH02 EBP	DGC	20.29	21 63	21.36	23.04	24, 44	24, 35	23, 25
1262 TH03 EBP	DGC	18.29	20 31	20.05	21, 57	23, 12	22 84	21.46
1263 TH01 STS	DGC	6.54	-3, 03	-6.22	-2,61	1.60	1 76	0.52
1264 TH02 STS	DGC	D	D	D	D	D	D	D
1265 TH03 STS	DGC	8.46	0.79	- 48	4.96	7, 47	8, 31	8,67
1266 TH04 STS	DGC	-2.78	-9. 13	-9 65	-4. 95	-2.14	-2.04	-3,26
1267 TH05 STS	DGC	9 62	1 28	-2.64	2, 19	6.41	6 59	5, 57
1224 SAD R FSST	DGC	35 00	34 56	36 57	38.78	39, 98	39.00	35, 81
1244 SAD L FSST	DGC	50.00	46.17	46.29	48, 55	48, 99	49, 18	49.13

⁽¹⁾ RMP-1 Left off after initial test in Orbit 1
(2) Prelaunch leak - refer to text
D = Defective telemetry point

Table 4-3. Landsat-2 ACS Voltages and Currents

					Orbit			
Function	Units	29	1253	2532	3810	4241	4670	5102
1081 RMP 1 MTR Volts	VDC	OFF						
1082 RMP 1 MTR Current	Amps	OFF	OFF	OFF	OFF	OFF	OFF	OFF
1080 RMP 1 Supply Volts	VDC	OFF						
1091 RMP 2 MTR Volts	VDC	29.99	29 97	29 94	29 94	29 94	29 93	29 92
1092 RMP 2 MTR Current	Amps	0 10	0 10	0 10	0.10	0.10	0 10	0 10
1090 RMP 2 Supply Volts	VDC	~23 63	-23 62	-23.61	-23 59	-23.58	~23 58	-23 59
1220 SAD RT MTR WNDNG Vol	ts VDC	-5 47	-4.71	-4.51	-4 85	-4 48	-4 49	-4 47
1240 SAD LT MTR WNDNG Vol	ts VDC	-5 08	-4.91	-4.70	-4.70	-4 75	-4, 72	-4 72
1227 SAD RT -15 VDC Conv	VDC	15 14	15.14	15 15	15 14	15 12	15, 12	<b>1</b> 5 16
1247 SAD LT -15 VDC Conv	VDC	15,23	15 21	15 22	15 23	15 21	15 20	15, 21
1056 CLB ± 6 VDC	TMV	2.35	2, 35	2.35	2 38	2 37	2 37	2 38
1055 CLB ± 10 VDC	TMV	2 88	2, 90	2 90	2,92	2, 92	2 92	2 92
1057 CLB Power Supply Volts	TMV	2,97	2,94	2,94	2 96	2 97	2,97	2 96

Table 4-4. Landsat-2 ACS Attitude Errors and Driver Duty Cycles

					Orbits			
Function	Units	26	1202	2532	3810	4241	4670	5102
1041 Pitch Fine Error	DEG	-0 15	-0 14	-0 14	-1 23	-1 24	- 77	- 13
1043 Pitch Flywheel Speed	RPM	-156 12	-221, 22	-198 41	66 38	125 87	-101 31	-162 97
1038 Pitch Mtr Drvr CCW	PCT	6 64	8 61	7 35	4 33	4 76	6 58	6 05
1039 Pitch Mtr Drvr CW	PCT	2 03	3 64	2 60	6 82	7 39	4 24	1 80
1030 Roll Fine Error	DEG	-0 13	-0 11	-0 09	- 13	- 15	-, 13	- 14
1027 Roll Rear Flywheel SPD	RPM	729 30	731 98	739 75	754 14	781 91	763 10	748 56
1026 Roll Fwd Flywheel SPD	RPM	703 02	710 22	725 23	735 32	732 53	747 87	735 81
1022 Roll Rear Mtr Drvr CCW	PCT	0 67	0 86	39	31	55	99	63
1025 Roll Rear Mtr Drvr CW	PCT	7 54	7 11	5 47	6 21	6 97	7 19	6 34
1023 Roll Fwd Mtr Drvr CCW	PCT	0,70	0 79	37	53	63	1 32	. 87
1024 Roll Fwd Mtr Drvr CW	PCT	5, 46	4 47	4 74	4 06	5 07	5 14	4 01
1035 Yaw Tach	RPM	-95 73	-77 38	-41 57	-98 81	-62 65	-75 84	-38 16
1033 Yaw Mtr Drvr CW	PCT	1 98	2 10	1 77	1 59	1 94	2 35	2 01
1034 Yaw Mtr Drvr CCW	PCT	2 10	2.15	1 72	1 80	2 00	2.74	1 90
1221 SAD Right Tach	D/M	0.00	3 39	3 38	3 37	3 39	3 38	3 38
1241 SAD Left Tach	D/M	3,68	3 64	3 63	3 60	3 57	3 56	3 56

# SECTION 5 COMMAND/CLOCK SUBSYSTEM LANDSAT-2

### COMMAND/CLOCK SUBSYSTEM (CMD)

The CMD Subsystem operated nominally in this report period. On January 1, 1976, during Orbit 4787, the spacecraft clock was moved back by approximately 3 seconds.

Figure 5-1 shows the history of the S/C clock drift since launch. Figure 5-2 shows the cumulative drift since launch (3.1 seconds in 12 months). As can be seen, the clock of Landsat-2 drifts in opposite direction from the clock of Landsat-1. Figure 5-2 also shows the clock drift rate, which is nearly constant at +0.6 milliseconds per orbit.

Table 5-1 shows typical telemetry values since launch. All are nominal.

Table 5-1. Command/Clock Telemetry Summary, Landsat-2

Function							Orbit			
No	Name	Mode	Units	35	1253	2462	2964	4241	4670	5091
8005	Pri Power Supply Temp		DGC	38 82	39 86	40 43	39 91	39 45	39 50	39 43
8006	Red. Power Supply Temp		DGC	36 93	38 03	38 70	38 20	38 02	39 29	38 00
8007	Pri Osc Temp	-	DGC	28 70	28 70	29 35	28 70	28 34	28 63	28 70
8008	Red Osc Temp	-	DGC	27 82	27 93	28 68	27 85	27 10	27 82	27 26
8009	Pri Osc Output	-	TMV	1 06	1 05	1 06	1 06	1 05	1 05	1 05
8010	Red Osc Output	-	TMIV	1 17	1, 19	1 20	1 19	1 18	1 20	1 18
8011	100 KHz	Pri - Red	TMV	3 17	3 16	3 16	3 16	3 15	3 15	3 15
8012	10 KHz	Pri - Red	TMV	3 08	3 05	3 05	3 05	3 05	3 05	3 05
8013	2 5 KHz	Pri - Red	TMV	3 01	2 95	2 95	2 95	2 95	2 95	2 95
8014	400 Hz	Pri - Red	TMV	4 17	4 45	4 45	4 45	4 45	4 45	4 45
8015	Pri, +4V Power Supply	Pri Clk ON	VDC	NA	2 05	2 05	2 05	2 05	2 05	2 05
8016	Red. +4V Power Supply	Red Clk ON	VDC	NA	2 01	2 01	2 01	2 00	2 03	2 00
8017	Pri +6V Power Supply	Pri Cik ON	VDC	NA	2 30	2 30	2 31	2 30	2 30	2 30
8018	Red. +6V Power Supply	Red Clk ON	VDC	NA	2 31	2 31	2 31	2 30	2 33	2 30
8019	Pri - 6V Power Supply	Pri Clk ON	VDC	ŅΑ	5 22	5 23	5 23	5 23	5 22	5 <b>2</b> 3
8020	Red 6V Power Supply	Red Clk ON	VDC	NA	5 23	5 23	5 23	5 23	5 25	5 23
8021	Pri - 23V Power Supply	Pri Clk ON	VDC	NA	5 70	5 70	5 70	5 70	5 70	5 70
8022	Red - 23V Power Supply	Red Clk ON	VDC	NA	5 65	5 65	5 65	5 65	5 65	5 <b>6</b> 5
8023	Pri - 29V Power Supply	Pri Clk ON	VDC	NA	5 29	5 30	5 29	5 29	5 29	5 29
8024	Red - 29V Power Supply	Red Clk ON	VDC	NA	5 29	5 29	5 28	5 29	5 30	5 29
8101	CIU A - 12V	CIU A ON	VDC	3 79	3 97	3 97	3 97	3 97	3 97	3 97
8102	CIU B - 12V	CIU B ON	VDC	3 78	3 95	3 95	3 95	3 95	3 97	3 95
8103	CIU A - 5V	CIU A ON	VDC	3 93	4 15	4 15	4 14	4 15	4 14	4 15
8104	CIUB - 5V	CIU B ON	VDC	3 90	4 10	4 10	4 10	4 10	4 12	4 10
8105	CIU A Temp	CIU A ON	DGC	26 01	22 09	22 50	21 94	21 34	21 60	21 67
8106	CIU B Temp	CIU B ON	DGC	23 35	19 96	20 38	19 90	19 45	20 33	19 70
8201	Receiver RF-A Temp	-	DGC	NA NA	29 58	30 02	29 50	28 89	29 03	29 14
8202	Receiver RF-B Temp	-	DGC	29 09	F	F	F	F	F	F
8203	D MOD A Temp	-	DGC	28 95	38 80	39 20	38 72	38 37	38 44	38 56
8204	D MOD B Temp	-	DGC	37 73	27 10	27 56	27,03	26 49	26 84	26 72
8205	Receiver A AGC	Receiver A ON	DGC	F	-91 00	-92 18	-91 74	-91 32	-90 83	-91 43
8206	Receiver B AGC	Receiver B CN	DBM	-87 83	F	F	F	F	r	F
8207	Amp A Output	Receiver A ON	TMV	F	2 70	2 51	2 52	2 49	2 77	2 54
8208	Amp B Output	Receiver B ON	TMV	2 10	F	F	F	F	F	F
8209	Freq Shift Key A Out	Receiver A ON	TMV	F	1 09	1 08	1 08	1 08	1 09	1 08
8210	Freq Shift Key B Out	Receiver B ON	TMV	1 11	F	F	F	F	F	F
8211	Amp A Output	Receiver A ON	TMV	F	1 13	1 12	1 12	1 13	1 14	1 13
8212	Amp B Output	Receiver B ON	TMV	1 13	F	F	F	F	F	F
8215	D MOD A - 15V	Receiver A ON	TMV	F	4 87	4 87	4 87	4 87	4 87	4 87
8216	D MOD B - 15V	Receiver B ON	TMV	4 77	F	F	F	Г	F	F
8217	Regulator A - 10V	Receiver A ON	TMV	F	5 40	5 40	5 40	5 40	5 40	5 46
8218	Regulator B - 10V	Receiver B ON	TMV	5 32	F	F	F	F	F	F
8311	ECAM Mem Tmp	ECAM ON	DGC	NA	17 95	18 03	17 89	18 66	18 66	18 44
8312	ECAM Pwr Spply Temp	ECAM ON	DGC	NA	22 43	23 13	22 34	23 32	23 31	23 13

NA - Not available due to processing problem - MT 710

F - OFF

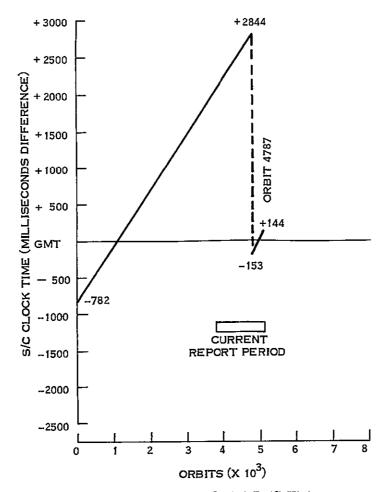


Figure 5-1. Landsat-2 Drift History

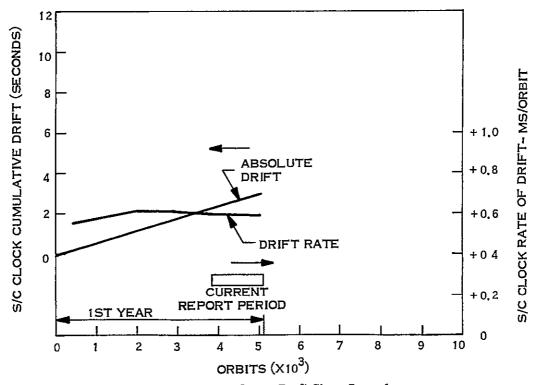


Figure 5-2. Cumulative Drift Since Launch

### SECTION 6 TELEMETRY SUBSYSTEM LANDSAT-2

### TELEMETRY SUBSYSTEM (TLM)

The TLM has operated nominally in this report period.

Table 6-1 shows typical telemetry values since launch. All are nominal except for functions 1264 (Thermal Shield 5 Temperature), 4002 (MMCA Board 2 Temperature), and 13200 (APU 24 Volt Input), which were defective before launch. Verification of these functions is acceptable by adjacent temperature and downstream voltage measurements respectively.

The Memory section of the telemetry matrix remains in the 0.0 mode.

Table 6-1. Landsat-2 TMP Telemetry Values

Func.			Orbit							
No.	Function Name	Unit	35	1253	2467	3810	4261	4670	5091	
9001	Memory Sequencer A Converter	VDC	4.45	4.45	4.45	4.45	4,45	4.45	4.45	
9002	Memory Sequencer B Converter	VDC	**	**	**	**	**	**	**	
9003	Memory Sequencer Temp	°C	20,00	19,19	20,77	20,65	20,96	21, 13	21, 37	
9004	Formatter A Converter	VDC	4,52	4.51	4,51	4.52	4. 52	4.52	4. 52	
9005	Formater B Converter	VDC	**	**	**	**	**	**	**	
9006	Dig. Mux A Converter	VDC	4.22	4.22	4.22	4.22	4, 22	4, 22	4.22	
9007	Dig. Mux B Converter	VDC	**	**	**	**	**	**	**	
9008	Formatter/Dig Mux Temp	°C	25,00	23,23	23,98	24.75	24.93	26.80	27.80	
9009	Analog Mux A Converter	VDC	4.02	4.05	4,05	4.05	4,05	4.05	4,05	
9010	Analog Mux B Converter	VDC	**	**	**	**	**	**	**	
9011	A/D Converter A Voltage	VDC	4.02	4.02	4.02	4.03	4.03	4.05	4.03	
9012	A/D Converter B Voltage	VDC	**	**	**	**	**	**	**	
9013	Analog Mux, A/D Conv. Temp	°C	25.00	25.00	24.91	25.41	26.10	27.42	27.33	
9014	Preregulator A Voltage	VDC	4.00	4,00	4.00	4.00	4.00	4,00	4,00	
9015	Preregulator B Voltage	VDC	**	**	**	**	**	**	**	
9016	Reprogrammer Temp	°C	22.50	22,24	22,27	22,34	22.49	22.50	24.74	
9017	Memory A Converter	VDC	4,45	4,45	4.45	4.45	4.45	4.45	4.45	
9018	Memory A Temp	°C	17,50	16.46	17.33	17,26	17.10	16.86	17.17	
9019	Memory B Converter	VDC	**	**	**	**	**	**	**	
9020	Memory B Temp	°C	17.50	16.78	17.28	17.27	17.41	17,50	17,41	
9100	Reflected Power (Xmtr A)	dBm	18.29	13.84	13.68	13.85	13,91	13, 99	14, 18	
9101	Xmtr A-20 VDC	VDC	3,80	3.97	3,98	3.97	3.97	3, 97	3.97	
9103	Xmtr A Temp	°C	27.73	21,02	20.97	21,79	21.92	23.21	26.40	
9104	Xmtr B Temp	°C	*	23,27	22.07	22,87	23.02	24.43	27.74	
9105	Xmtr A Power Output	dBm	27.73	26.14	26.19	26.19	26.19	26.19	26.29	
9106	Xmtr B Power Output	dBm	**	**	**	**	**	**	**	

^{*} Not available due software

^{**} Not turned on since Prelaunch

ORBIT ADJUST SUBSYSTEM

### ORBIT ADJUST SUBSYSTEM (OAS)

The Orbit Adjust Subsystem on Landsat-2 has been fired ten times since launch, 6 times using the -X thruster and 4 times using the +X thruster. One firing of the -X and +X thruster each was for alignment tests. Three +X firings and two -X firings were made to phase the satellite with Landsat-1 to obtain a combined nine day ground track repeat pattern. Three -X firings were for orbit maintenance.

No firing of the OAS was made during this report period (See Section 2 also).

The Subsystem activity since launch is summarized in Table 7-1. A total of 6.87 lbs. of hydrazine has been expended so far from the pre-launch load of 67 lbs.

The OAS telemetry has consistently shown normal pressure temperature parameters. A sampling of the same is given in Table 7-2. The variations in the thrust chamber temperatures in Table 7-2 are consistent with the variations in sun intensity and sun angle.

Table 7-1. Landsat-2 Orbit Adjust Summary

Orbit	Orbit Adjust No.	Ignition Epoch	Burn Duration (Seconds)	+∆a (Meters)	Engine Performance Efficiency %	Fuel ¹ Used (Lbs)	Tank Pressure (PSIA)	Tank Temperature (° F)	Thruster Axis
32	1	25 Jan 75 00 34 00.8	4.8	39	104.3	0.02	539.96	72.0	-x
71	2	27 Jan 75 19 57 00.8	4.8	-36	90.1	0.02	547.46	73.5	+X
79	3	28 Jan 75 09 49 00.8	420.0	3455	107.0	1.62	547.46	73.5	-X
86	4	28 Jan 75 21 13 00.8	420.0	3233	107.0	1.51	502.46	73.5	-x
163	5	3 Feb 75 10 36 00.8	420.0	-2974	97.0	1.42	468.75	75.0	+X
191	6	5 Feb 75 10 51 00.8	360.0	-2421	97.5	1.15	438.71	75.0	+X
212	7	6 Feb 75 22 31 00.8	308.8	-2009	98.6	0.95	416.21	75.0	+:X
880	8	26 Mar 75 21 44 00.8	12.8	82	107.6	0.04	397.47	70.5	-x
1632	9	19 May 75 18 54 00.8	24.0	+154	107.6	0.07	401.21	73.5	-x
2958	10	22 Aug 75 22 11 58.8	22.0	146	110.3	0.07	404.96	73.5	-x

¹ Initial Fuel Capacity - 67 lbs.

Table 7-2. Landsat-2 OAS Telemetry Values

Function						Orbit			
No.	Name	Units	50	1253	2532	3810	4241	4670	5102
2001	Prop. Tank Temp.	°C	23.03	21.97	23.05	23.47	23.05	23,47	23.89
2003	Thrust Chamber No. 1 (-X) Temp.*	°C	24.84	30.28	30.14	29.24	29.13	28,12	25,12
2004	Thrust Chamber No. 2 (+X) Temp.*	°C	37.34	37.63	38.41	39.83	40.20	39.69	38,55
2005	Thrust Chamber No. 3 (-Y) Temp.*	°C	47.22	36.23	34.20	37.92	38,83	42.36	46,35
2006	Line Pressure	psia	545.60	399.69	404.97	410.26	411.10	412.44	413,25

^{*}Widespread of temperature is due to nozzle locations and satellite day/night transitions relative to data averaged.

Typical orbital range is from 19 to 59 DGC.

# SECTION 8 MAGNETIC MOMENT COMPENSATING ASSEMBLY LANDSAT-2

### MAGNETIC MOMENT COMPENSATING ASSEMBLY (MMCA)

The spacecraft was corrected for unbalanced magnetic moments in Orbits 293 and 321 as reported earlier. These adjustments were made on the pitch magnetic rod of the MMCA.

No adjustment to the MMCA dipoles was made during this report period.

Orbital averages of MMCA telemetry functions for selected orbits are given in Table 8-1.

Table 8-1. Landsat-2 MMCA Telemetry Values

!						Orbit			<u> </u>
Function	Name	Units	50	1253	2532	3810	4241	4670	5102
4001	A1 Board Temp	°C	20.56	19.84	19.82	19,97	19.44	19.44	19 47
4002	A2 Board Temp	°c	*	*	*	*	*	*	*
4003	Hall Current	TMV	3.40	3.40	3.40	3.40	3.40	3.40	3 40
4004	Yaw Flux Density	TMV	3.05	3.06	3.07	3,07	3.07	3, 06	3,07
4005	Pitch Flux Density	TMV	3.15**	2.92**	2.90	2,90	2.90	2.90	2.90
4006	Roll Flux Density	TMV	2.99	2.98	2.98	2.98	2,97	2, 97	2.97

^{*}Defective Telemetry Function (Pre-launch)

^{**}Post launch telemetry drift.

UNIFIED S-BAND/PREMODULATION PROCESSOR

### UNIFIED S-BAND/PREMODULATION PROCESSOR (USB/PMP)

The USB Subsystem has operated nominally in this report period.

Table 9-1 shows telemetry values since launch. All are nominal. The transmitter has maintained a steady power output of about 1.4 watts since launch. Figure 9-1 shows AGC readings of Goldstone for a constant position in space. The scatter of data points reflect variations in the ground station calibration and readout.

Table 9-1. Landsat-2 USB/PMP Telemetry Values

								ORBITS				
No.	Function Name	Units	T/V (20°C)	15	50	1253	2462	2964	3810	4241	4670	5091
11001	USB Revr AGC	DBM	NA	-112 72	-120.24	-121 7	-128.8	-125 3	-131.5	-130 5	-131 5	-124 29
11002	USB Xmtr Pwr	WTS	1 40	1.36	1 36	1 38	1 43	1 40	1.42	1 39	1 37	1 38
11003	USB Revr Error	KHz	NA	-2 15	-4.87	-4 14	-4.64	-6 88	-4, 23	<b>-4</b> 15	-4 13	-2 97
11004	USB Xpond Temp	DGC	22 93	25 88	29 12	24 38	24 37	25 20	24.96	24 85	25 32	27 49
11005	USB Xpond Press	PSI	16.99	17.08	17.09	16 94	16 74	16 71	16 61	16 47	16 47	16 49
11007	USB Xmtr A -15V	VDC	2 35	2 36	F	F	F	F	F	F	F	F
11008	USB Xmtr B -15V	VDC	2 39	F	2 40	2 40	2 40	2 40	2 42	2 40	2 43	2 42
11009	USB Range -15V	VDC	2 07	2 07	2 05	2 05	2.07	2,06	2 06	2 05	2 05	2 06
11101	PMP Pwr A Volt	VDC	-15 22	-15 10	F	F	F	F	F	F	F	F
11102	PMP Pwr B Volt	VDC	-15 07	F	-14 96	-14.98	-15.02	-15.00	-15.01	-15 02	-15 04	-14 99
11103	PMP Temp A	DGC	NA.	37 30	32 37	28.64	29 12	29.46	29 74	30 11	30 84	34 67
11104	PMP Temp B	DGC	NA	28 34	35.16	30,03	30 57	31.31	31 26	31 53	31 99	36 08

F Unit OFF in this period

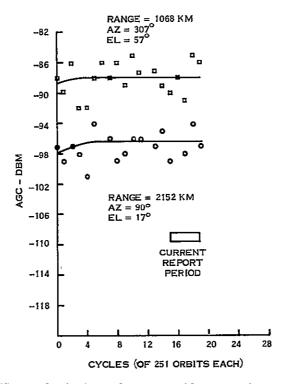


Figure 9-1. USB (Link) AGC Readings at Goldstone with 30' Antenna - Landsat-2

ELECTRICAL INTERFACE SUBSYSTEM

### ELECTRICAL INTERFACE SUBSYSTEM (EIS) LANDSAT-2

The Auxiliary Processing Unit (APU) consisting of Search Track Data, Time Code Data, and Back-up Timers operated satisfactorily throughout this report period. Telemetry for the APU is shown in Table 10-1.

Table 10-1. Landsat-2 APU Telemetry Functions

			Orbit								
Function	Description	Unit	21	1253	2532	3810	4241	4670	5102		
13200	APU, -24.5 VDC	TMV	*	*	*	*	*	*	*		
13201	APU, -12 Volts	TMV	2.42	2.44	2.45	2.45	2.45	2.45	2.45		
13202	APU Temp	DGC	27.44	26. 65	26, 60	27.01	26.51	27.03	27.70		

^{*}Defective Telemetry (Prelaunch)

The Power Switching Module (PSM) containing the switching relays for power to the OAS, MSS, WBVTR No. 1 and No. 2, RBV and PRM, functioned normally. During this report period, the MSS as well as WBVTR No. 2 power circuits, have been operated on a regular basis. RBV power circuits have been operated during the periodic tests on 10 November 1975 and later for image coverage on 11 and 12 November 1975.

The Interface Switching Module performed all switchings normally during this report period.

THERMAL SUBSYSTEM

### THERMAL SUBSYSTEM (THM)

The Thermal Control Subsystem on Landsat-2 has provided excellent temperature control of all spacecraft equipments since launch.

Table 11-1 gives average subsystem telemetry values for several representative orbits during the first twelve months of operation of Landsat-2. Average temperatures of the sensory ring bays are plotted in Figure 11-1.

During this report period the sun intensity increased from 1.012 of the mean value to a peak of 1.034 and then slightly declined to a value of 1.032. This caused a general increase in spacecraft temperatures, noticeably along bays 11 through 18. The temperatures are expected to decrease during the on-coming period of lower sun intensity.

During Orbit 4204, compensation loads 1, 2, 5 and 8 were turned off to assist in power management. However, in Orbit 4372, compensation load 8 was turned on again because of decreasing MSS temperatures. A history of all switchings of compensation loads is given in Table 11-2.

LS-2 11-1

Table 11-1. Landsat-2 Thermal Subsystem Analog Telemetry (Average Value for Frames of Data Received in NBTR Playback)

Function No	Function Description	- ·			-	Orbits			
No		ı							
		Unit	21	1253	2532	3810	4241	4670	5102
	THM THOL STI	DGC	19 40	18 71	19 59	19 90	19 33	19 54	19 97
7002	THM THO2 SBO	DGC	17 18	17 48	18 05	18 22	17 65	17 48	17 47
7003	THM THOS STI	DGC	18 73	18 38	19 49	19 54	18 38	18 19	18 50
7004	THM THIO TCB	DGC	19 38	19 08	19 01	19 34	18 67	18 96	19 34
7005	THM THO4 STI	DGC	17 19	17 06	17 92	18 03	16 76	16 45 16 63	16 76 16 68
7006	THM TH05 SBO	DGC	17 42	17 13	17 46 20 58	17 55 20 61	16 79 19 81	19 88	19 65
7007	OA-X Thruster	DGC	19 66 14 78	20 52 14 50	20 36 14 77	14 85	13 94	13 93	13 94
7008 7009	THM THO6-STO	DGC	19 18	18 82	19 18	19 52	18 34	18 29	18 41
7010	THM THOT STI	DGC	18 08	18 00	18 26	18 42	17 30	17 41	17 44
7011	THM THOS STO	DGC	19 34	20 07	20 22	20 27	19 34	19 49	19 23
7012	THM TH09 SBI	DGC	21 44	21 75	21 80	21 99	20 55	20 82	20 93 18 39
7013	THM THIO SBO	DGC	18 58	18 58	18 56	18 80	17 99 20 70	18 26 21 27	21 93
7014	THM THIL STI	DGC	21 65 23 93	21 11 22 28	21 13 22 13	21 58 22 87	22 47	23 47	24 68
7015 7016	THM THI2 SBO THM THI3 STI	DGC	22 21	20 49	20 51	21 20	20 93	21 82	23 62
7017	RBV Beam Ctr In	DGC	20 38	20 32	20 33	20 65	19 07	19 50	19 92
7018	THM TH14 STO	DGC	24 12	21 34	21 29	22 32	22 41	23 54	26 43
7019	NBR Rad Outbd B4	DGC	2 72	3 05	3 26	3 37	2 72	2 73	2 93
7020	THM THIS SBI	DGC	23 07	20 96	21 13	22 15	21 93	22 95	25 56
7021	THM THI6 STI	DGC	23 26	21 92	22 29	23 11	22 79	23 60 22 47	25 46 23 74
7022	THM TH17 SBI	DGC	21 77	20 72	21 22	22 11 22 42	21 86 22 25	22 67	23 36
7023 7030	THM THIS SBO THM THOS Bur	DGC DGC	21 67 15 50	21 06 15 48	21 49 16 28	16 29	15 48	15 10	15 14
7030	THM TH12 Bur	DGC	23 05	21 71	21 70	22 41	22 27	23 11	24 59
7035	THM THIS Bur	DGC	19 53	18 73	19 32	19 77	19 60	19 95	20 39
7040	THM THO1 TCB	DGC	19 42	19 08	19 78	20 11	19 43	19 46	19 72
7041	THM TH02 TCB	DGC	17 55	17 33	18 02	18 14	17 52	17 32	17 39 16 32
7012	THM THO3 TCB	DGC	16 85	16 83	18 23 20 05	18 29 20 20	16 62 19 53	15 93 19 24	16 32 19 33
7043	THM TH04 TCB	DGC DGC	19 90 16 42	19 69 16 08	16 21	20 20 16 45	15 81	15 61	15 75
7044 7045	THM THOS TOB	DGC	17 76	17 96	18 12	18 23	17 36	17 38	17 33
7046	THM THOS TOB	DGC	19 30	19 24	19 31	19 51	18 53	18 73	18 81
7048	THM THII TCB	DGC	23 27	22 50	22 45	22 98	22 39	23 02	23 74
7049	THM THI2 TCB	DGC	23 04	20 62	20 62	21 24	21 15	22 08	23 94
7050	тим тиз тсв	DGC	22 89	20 43	20 34	21 17	21 09	22 25	24 67
7051	THM TH14 TCB	DGC	25 07	22 09	22 11	23 19	23 28	24 26 22 86	27 69 24 29
7052	THM THIS TCB	DGC	22 22	20 83 22 32	21 59 22 79	22 56 23 71	22 23 23 48	23 91	24 86
7053	THM THI7 TCB THM THI8 TCB	DGC DGC	23 52 20 01	19 46	20 05	20 89	20 59	20 80	20 99
7054 7060	THM Shutter By 1	DEG	22 54	18 26	24 43	27 61	21 62	22 12	26 65
7061	THM Shutter By 2	DEG	19 34	19 00	24 75	26 64	20 45	21 26	21 13
7062	THM Shutter By 3	DEG	22 75	19 48	31 67	31 71	14 51	7 78	11 99
7063	THM Shutter By 4	DEG	33 89	35 12	36 32	36 34	32 37	32 88	33 00
7064	THM Shutter By 5	DEG	7 50	6 35	8 67	6 40	3 40	2 90	2 90 14 11
7065	THM Shutter By 7	DEG	17 06	19 77 35 25	22 52 38 22	21 87 37 09	13 66 34 48	14 32 34 13	34 12
7067	THM Shutter By 9 THM Shutter By 10	DEG DEG	33 75 37 46	35 65	34 96	36 62	32 85	35 15	37 09
7068 7069	THM Shutter By 11	DEG	52 25	17 10	10 16	27 12	16 42	16 77	17 39
7070	THM Shutter By 12	DEG	61 38	46 16	46 20	50 <b>0</b> 5	49 56	55 76	67 46
7071	THM Shutter By 13	DEG	63 60	47 54	45 76	53 45	52 95	61 02	74 14
7072	THM Shutter By 14	DEG	59 44	40 54	40 40	47 92	48.71	54 93	72 14
7073	THM Shutter By 15	DEG	67 79	52 64	53 78	62 33	63 03 48 38	69 04 51 04	82 12 61 13
7074	THM Shutter By 16	DEG	45 20 57 90	37 85 49 22	43 68 52 10	51 34 58 35	57 24	60 80	67 62
7075 7076	THM Shutter By 17 THM Shutter By 18	DEG DEG	57 88 40 49	36 36	39 32	44 47	42 97	44 57	45 84
7076	THM Q1 T Zener V	VDC	4 85	4 85	4 85	4 86	4 85	4 85	4 85
7081	THM Q2 T Zener V	VDC	4 90	4 90	4 90	4 90	4 90	4 90	4 90
7082	THM Q3 T Zener V	VDC	5 05	5 03	5 04	5 05	5 03	5 04	5 05
7083	THM Q1 S Zener V	VDC	4 97	4 96	4 96	4 97	4 95	4 95 4 98	4 96 4 99
7084	THM Q2 S Zener V THM Q3 S Zener V	VDC VDC	4 98 5 15	4 98 5 15	4 98 5 15	4 99 5 15	4 98 5 15	5 15	5 15
7085 7090	THM Q3 S Zener V	DGC	21 02	20 76	21 05	21 36	20 16	20 80	21 71
7091	THM Ind Attitude	DGC	17 79	17 73	17 86	18 21	16 91	17 16	17 24
7092	THM RBV Radiator	DGC	18 01	18 07	18 06	18 54	14 80	15 65	16 24
7093	THM RBVC Ctr Bm	DGC	20 74	20 82	20 82	21 82	18 12	18 76	19 31
7094	THM WBVTR Root	DGC	13 77	14 24	14 71	15 00	13 99	14 96	15 72 = ##
7095	THM WBVTR Rad Ct	DGC	3 64 15 90	4 52 16 24	4 99 16 95	5 19 17 12	4 30 16 20	5 27 16 94	5 55 17 63
7096 7097	THM WBVTR Strap THM WB Mt Bay 1	DGC DGC	15 90 22 91	16 24	22 60	21 19	21 01	21 87	22 49
7097	THM WE Mat Bay 1	DGC	22 07	16 61	19 25	18 34	18 15	19 23	20 14
7099	THM WBVTR Sep 3	DGC	18 03	17 81	18 76	18 82	17 82	17 73	18 12
7100	THM WBVTR Sep 17	DGC	21 83	20 87	21, 55	22 14	21 78	22 35	23 51
7101	THM WBVTR 1 Cent	DGC	22 45	22 20	23 13	23 23	22 59	23 03	23 78
7102	THM WBVTR 2 Bay	DGC	17 34	17 27	17 69	17 89	16 92	17 04	17 29 23 87
71,03	THM WBVTR 2 By 15	DGC	21 77	20 72 20 65	20 99 21 08	21 57 21 17	21 13 20 25	22 04 21 16	22 34
7104	THM WBVTR 2 Ctr	DGC	20 74 17 82	20 65 17 73	17 96	18 36	20 25 17 17	17 67	17 86
7105	THM NBTR B Sep 6 THM NBTR B Sep 1	DGC DGC	22 11	20 64	20 70	21 33	20 82	21 82	23 85
7106 7107	THM NBTR B Sep 1	DGC	20 32	20 30	20 44	20 74	19 49	20 18	21 21
7107	THM MSS Mount 14	DGC	20 59	19 33	19 40	20 28	19 57	20 75	22 86
7109	THM OA - Y Thruster		25 64	22 25	21 99	23 39	23 44	24 79	27 51
		DGC	16 75	17 15	17 54	17 84	16 52	17 51	18 21 20 43
7110	THM MSS WBVTR Bm								
7110 7111	THM OA +X Thruster	DGC	20 33	17 55	19 72	19 39	19 22	19 86	
7110			20 33 34 18 2 90	17 55 31 52 0 84	19 72 6 21 2 22	9 49 23 50	34 58 4 44	30 07 6 46	29 67 6 97

LS-2

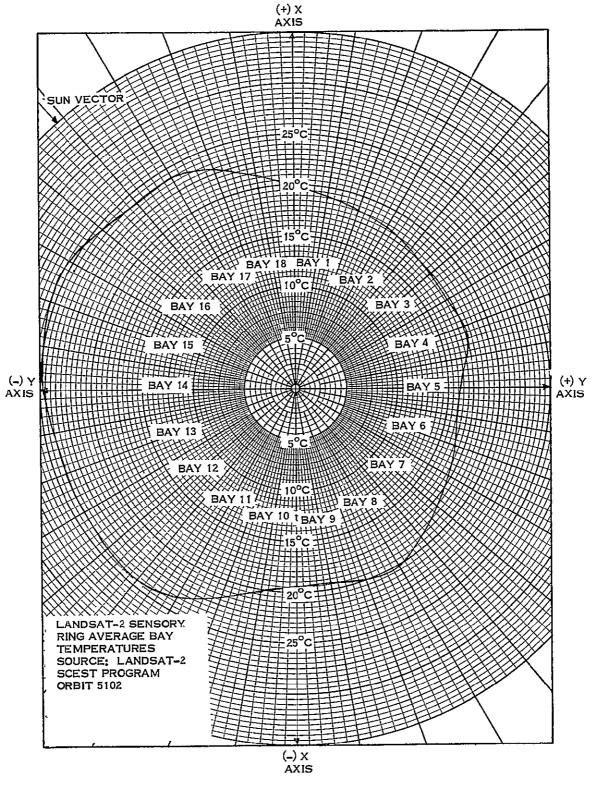


Figure 11-1. Landsat-2 Sensory Ring Thermal Profile

Table 11-2. Landsat-2 Compensation Load History

Compensation Load Status*										
Orbits	1	2	3	4	5	6	7	8		
Launch	0	0	0	0	0	0	0	0		
2	X	х	х	Х	х	0	х	х		
237	X	х	x	х	х	0	0	0		
272	X	Х	x	X	x	0	х	х		
306	Х	x	0	X	x	0	0	0		
572	X	х	0	X	x	0	0	x		
1367	х	x	x	x	x	0	0	x		
1645	х	х	0	X	x	0	0	x		
1657	х	x	х	x	х	0	0	x		
4202	0	0	X	X	0	0	0	0		
4372	0	0	X	Х	0	0	0	х		

*Note

X = ON

0 = OFF

NARROWBAND TAPE RECORDERS LANDSAT-2

### NARROWBAND TAPE RECORDERS (NBR)

The Narrowband Recorder Subsystem operated satisfactorily throughout the entire period, both Recorders alternating in Record and Playback modes with a nominal one minute overlap.

Since launch, each Recorder has operated for a period of 4591 hours.

Table 12-1 identifies cumulative operating hours for both Recorders by mode, and Table 12-2 gives typical telemetry values.

Table 12-1. NBR Operating Hours by Modes

NBR	On Off		Playback	Record
A	4591	4169	183	<del>44</del> 08
В	4591	4169	183	4408

Table 12-2. Narrowband Tape Recorder Telemetry Values, Landsat-2

	Function	Ty	pical Telemet	ry Values - O	rbits	
No.	Name	36/37	437/719	2111/2112	3801/3802	4980/4981
10001	A - Motor Cur. (ma) Record P/B	132.0 108.0	140.5 107.8	133.3 95.2	130.2 95.2	130.2 93.7
10101	B - Motor Cur. (ma) Record P/B	148.5 143.6	146.33 141.71	141.7 138.7	140.2 135.7	135,7 135,7
10002	A - Pwr Sup. Cur. (ma) Record P/B	170.5 410.0	172.4 409.2	167.5 399.3	165.8 405.9	162.5 399.3
10102	B - Pwr Sup. Cur. (ma) Record P/B	260.0 481.0	259.8 479.7	261.3 479.7	261.4 479.7	264.5 489.2
10003	A - Rec. Temp (DGC)	26.1	25.0	26.1	24.8	24.2
10103	B - Rec. Temp. (DGC)	27.0	25.4	27.0	26.6	26.2
10004	A - Supply (VDC)	-24.87	-25,10	-25.1	-25.1	-25,1
10104	B - Supply (VDC)	-24.55	-24.68	-24,6	-24.6	-24.6

## SECTION 13 WIDEBAND TELEMETRY SUBSYSTEM ... LANDSAT-2

### WIDEBAND TELEMETRY SUBSYSTEM (WBTS) LANDSAT-2

The WBTS has operated nominally in this report period.

Table 13-1 shows typical telemetry values. All are nominal.

Figure 13-1 is the AGC history recorded at Goldstone with the spacecraft successively at the same points m space. The scatter of data points reflect variations in the ground station calibration and readout. WBPA-2 has been used more consistently and is presented in this Figure. Values from WBPA-1 are nearly identical when this power amplifier is used.

Table 13-1. Wideband Telemetry Subsystem

		T/V	(2)	Orbits						
(π)	Name	10W	20W	424	1479	2462	3810	4241	4672	5091
12001	Temp, TWT Coll (DGC)	30 1	33 6	OFF	35 63	35 00	20 74	19 30	19 31	19 45
12101		27 9	31 2	31 43	35 71	37 14	30 00	16 92	18 14	18 17
12002	Cur, Helix (MA)	3 30	3 85	OFF	4 30	4 51	OFF	F	F	F
12102		4 03	4 56	4.53	4 43	4 48	4 52	4 61	4 57	4 59
12003	Cur, TWT Cath (MA)	33 20	46 10	OFF	43 60	45 12	OFF	F	F	F
12103		34 09	46 78	45 37	45 26	45 24	44 39	46 00	46 00	46 00
12004	Fwd Power (DBM) (3)	40 61	42 68	OFF	42 60	42 77	OFF	F	F	F
12104		40 93	43 71	43 65	43 66	43 69	43 56	43 60	43 63	43 61
12005	Refl Power (DBM) (3)	22 34	27 0	OFF	25 61	26 10	OFF	F	F	F
12105	, , , ,	34 55	36 45	36 36	37 15	37 14	36 91	37 27	37 12	37 08
12227	Con Volt, Loop Stress (MHz) (4)	1.	54	OFF	1 42	1 12	1 32	1 86	1 64	-14 00
12228	• •	2	53	0 32	0 24	-0 01	-0 30	0 05	-0 39	-0 22
12229	Temp Mod (DGC)	19	5	17 16	19 93	20 88	19 22	16 21	16 94	17 97
12232	+15 VDC Pwr	2	65	2 65	2 65	2 65	2 65	2 65	2 65	2 65
12234	+15 VDC Pwr Sup (TMV) (5)	4	07	4 08	4 01	3 94	4 10	4 19	4 10	4 04
12236	+5 VDC Pwr Sup (TMV) (5)	3	55	3 50	3 53	3 54	3 47	3 55	3 52	3 51
12238	-5 VDC Pwr Sup (TMV) (5)	4	08	4 07	4 03	4 01	4 09	4 11	4 08	4 07
12240	-24 VDC Unreg Pwr (TMV) (5)	5	86	5 90	5 80	5 66	5 91	6 05	5 92	5 90
12242	Temp, Inv (DGC)	23	7	21 68	23 21	23 79	22 93	22 01	22 21	22 53

### NOTES

- (1) Function numbers for WPA-1=120XX; for WPA-2=121XX
- (2) Thermo-Vacuum Test data for comparison
- (3) Pwr outputs of 10 or 20 watts can be selected
- (4) Any reading other than zero or -7 5 Is acceptable
- (5) Only power supply A operated during these orbits

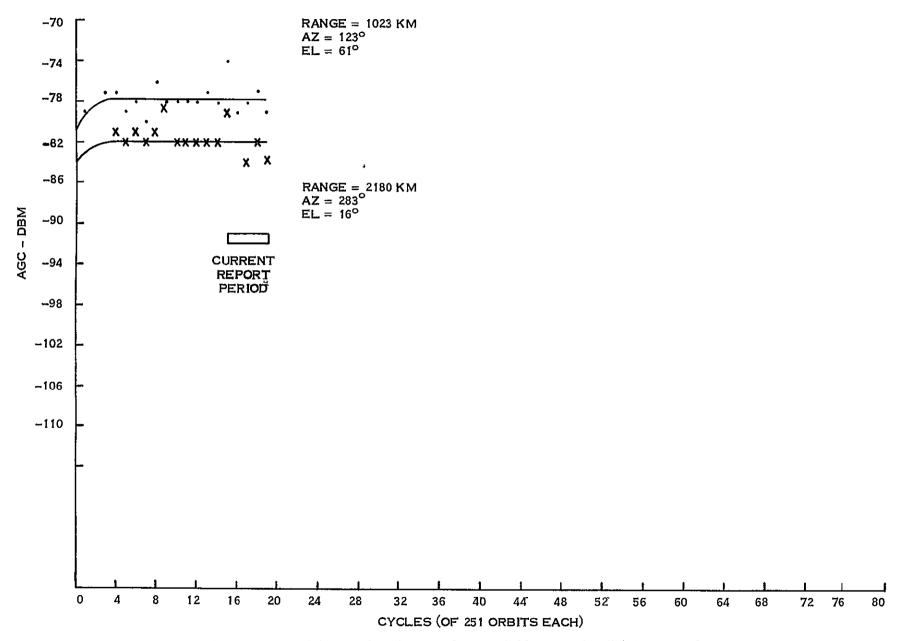


Figure 13-1. WPA-2 (Link 3) AGC Readings at Goldstone with 30" Antenna Landsat 2

### SECTION 14 ATTITUDE MEASUREMENT SENSOR (AMS) LANDSAT-2

#### ATTITUDE MEASUREMENT SENSOR (AMS)

The AMS is a passive radiometric balance sensor which operates in the 14-16 micron IR band. AMS Telemetry Values are shown in Table 14-1.

The AMS was launched in the OFF mode (CMD 774), turned ON during Orbit 6, and has been performing normally since then.

Table 14-1. Landsat-2 AMS Temperature Telemetry

Function		Units	50	1253	2532	3810	4241	4670	5102
3004	Case – Temp 1	DGC	19.00	19.05	19.02	19,39	18.18	18.67	18, 68
3005	Assembly - Temp - 2	DGC	18.70	18.69	18.71	18.93	17.87	18.30	18.30

# SECTION 15 WIDEBAND VIDEO TAPE RECORDERS LANDSAT-2

#### WIDEBAND VIDEO TAPE RECORDERS (WBVTR)

On January 6, 7, and 8, 1976 tests were performed on WBVTR-1 in an attempt to restore it to normal service. These tests, performed in Orbits 4865, 4878, 4879, 4892, and 4893, failed to effect any change to the Recorder. Thus, WBVTR-1 still remains mactive.

WBVTR-2 has functioned normally throughout this period except for a dropout from Rewind mode in Orbit 3854 (26 October), similar to a prior anomalous dropout in Orbit 1919 (9 June).

Table 15-1 gives typical telemetry values for WBVTR-1 and WBVTR-2. Tables 15-2 and 15-3 show the telemetry values for Record, Playback, Rewind, and Standby operational modes.

Figure 15-1 shows tape usage for WBVTR-2.

Table 15-1. WBVTR Telemetry Values

WBVTR-	1 Functions	]	Te	elemetry Valu	es In Orbits			
Number	Name	45/46	996	2642	3812	4261	4680	4879(ET)
13022	Pressure Trans	16 52	16. 51	16 51	16 39	16.39	16 39	16 39
13023	Temp Trans	20.74	20 05	20 62	19 00	18 77	19 00	20 12
13024	Temp Elec	25 00	18 59	24 57	19 67	20.07	20 00	21 68
13032	Limiter Volt	1 48	1 49	1, 51	*	*	*	1 41
13034	+5 6 VDC Conv	5 70	5, 48	5.54	*	*	*	5 67
13201	+2 VDC APU	2 44	2.45	2.45	2.45	2 45	2 45	2 45
13202	Temp APU	29 06	26. 76	26.76	27 03	26 58	27 0 <del>4</del>	27 29

WVVTR-	-2 Functions	İ	Telemetry Values In Orbits									
Number	Name	45/46	966	2642	3812	4261	4680	5071				
13122	Pressure Trans	16.12	16 12	15 81	15 49	15 46	15 34	15 33				
<b>1</b> 3123	Temp Trans	21 50	18 48	20 00	20.99	21 21	22 32	23 08				
13124	Temp Elec	23 50	14.49	18, 31	19 48	21 85	22 10	22 72				
13132	Limiter Volt	1 30	NA	1 32	1 33	1.34	1 30	1 28				
13134	+5.6 VDC Conv	5 71	6 32	5, 69	5 74	5 67	5 71	5 85				
13201	-12 VDC APU	2 44	2 45	2 45	2.45	2 45	2 45	2, 45				
13202	Temp APU	29 06	26.76	26.76	27. 03	26.58	27 04	27 63				

(ET) - Engineering Test of WBVTR-1

NA - Data not available

* - No data WBVTR-1 out of service

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Table 15-2. Function Values by Mode Landsat-2 WBVTR-1 Telemetry

WBVTR-1			Orbit		
Function/Description	T/V	718	1734	2642	4878(ET)
13029 ~ Input P/B Voltage					
Record	0.0	0.0	0 0	0 0	0 0
Playback	0 33	0 30	0.32	0, 32	0 30
Rewind	0 0	0.0	0 0	0.0	0 0
Standby	0.0	0 0	0 0	0.0	0.0
13028 - Capstan Motor Current					
Record	0.32	0.27	0 36	0.33	0.31
Playback	0.29	0.30	0.30	0 31	0 30
Rewind	0 23	0 21	0 27	0 23	0.28
Standby	0.0	0.0	0 0	0.0	0 0
13030 - Headwheel Motor Current	1				
Record	0.50	0.51	0.50	0 50	0 53
Playback	0 495	0.49	0 49	0 49	0.53
Rewind	0.41	0.44	0 44	0 44	0. <del>4</del> 7
Standbý	0.41	0.44	0 43	0.45	0.46
13031 - Recorder Input Current				j	
Record	3.58	3 61	3 62	3 69	3 62
Playback	3 92	3 86	3 93	3,86	3 86
Rewind	2 18	2 16	2 30	2 19	2 23
Standby	1 79	1 90	1 80	1 95	1 95
13033 - Servo Voltage					
Record	0.0	0.0	0 0	0.0	0 0
Playback	49 99	50.04	50.37	50 08	50.37
Rewind	0.0	0.0	00	0 0	0 0
Standby	0 0	0.0	0 0	0 0	0 0
13026 - Capstan Motor Speed					
Record	89 77	88 03	88 03	88. 03	85, 13
Playback	89 37	87.45	86 29	86 87	85.13
Rewind	100 12	99 06	97 32	98 48	96.73
Standby	0 0	0 0	0.0	0.0	0 0
13027 - Headwheel Motor Speed					
Record	97.5	96 18	95 07	95. 07	93 96
Playback	96, 86	95.07	94.52	94.52	92.86
Rewind	98 96	97 28	95.62	96 73	96 73
Standby	99. 12	97 28	93 96	95 62	95 07

(ET) - Engineering Test of WBVTR-1

Table 15-3. Function Values by Mode Landsat-2 WBVTR-2 Telemetry

WBVTR-2			Orbit		
Function/Description	T/V	437	1734	2642	4878
13129 - Input P/B Voltage					
Record ,	0.0	0.0	0.0	0.0	0 0
Playback	0 37	0 36	0.34	0, 33	0.34
Rewind	00	0 0	0 0	0.0	0 0
Standby	0 0	0.0	0 0	0.0	0 0
13128 – Capstan Motor Current		i			
Record	0.33	0.33	0.32	0 37	0.38
Playback	0 34	0.35	0 35	0.34	0.35
Rewind	0 16	0.20	0 19	0.18	0, 15
Standby	0.0	0.0	0.0	0.0	0 0
13130 - Headwheel Motor Current	1				
Record	0 47	0.47	0 47	0.47	0.48
Playback	0 46	0.46	0 47	0.47	0 48
Rewind	0.43	0 42	0 43	0 42	0 41
Standby	0,45	0.42	0.43	0 43	0.41
13131 - Recorder Input Current			1		
Record	2 88	2 90	2 90	2 90	2.90
Playback	3 11	3.02	3 08	3.08	3.11
Rewind	1 79	1 79	1 80	1.80	1 80
Standby	1 18	1.58	1 60	1 48	1 62
13133 - Servo Voltage	1				
Record	0 0	0 0	0,0	0.0	0 0
Playback	48.92	49 04	49 33	49 52	49 43
Rewind	0 0	0.0	0.0	0 0	0 0
Standby	0.0	0.0	0 0	0.0	0 0
13126 - Capstan Motor Speed	ļ				
Record	108.66	106.70	106 02	105 33	105 33
Playback	108 38	106 70	106.02	105.33	103.96
Rewind	130.09	117.68	117 0	116 31	117 68
Standby	0.0	0.0	0 0	0.0	0.0
13127 - Headwheel Motor Speed					
Record	98.41	96 52	96.00	96 52	95 48
Playback	98.11	96.00	95 48	94.44	94 44
Rewind	99 95	97 04	96 00	95.48	96 52
Standby	101 72	97 04	96 52	94.96	96,00

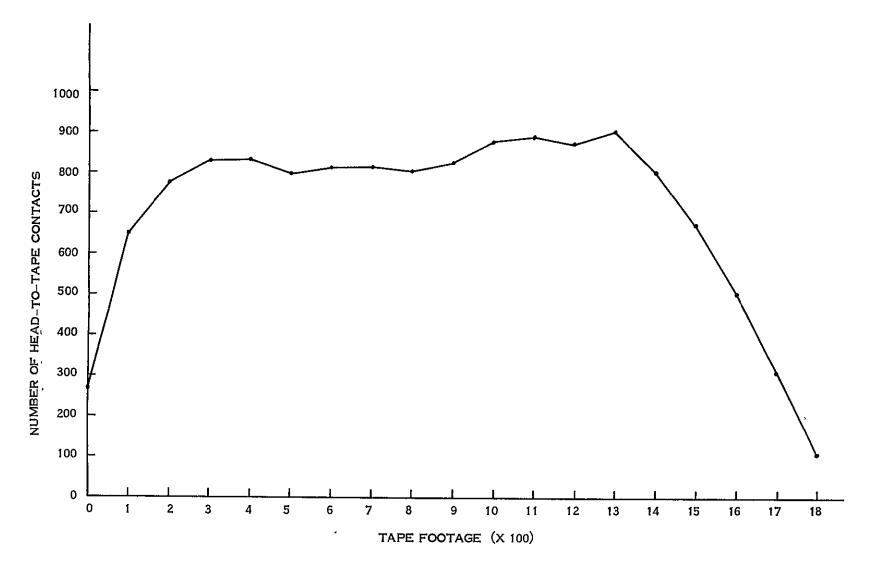


Figure 15-1. Tape Usage Thru Orbit 5096 WBVTR-2

#### RETURN BEAM VIDICON

LANDSAT-2

#### RETURN BEAM VIDICON (RBV)

The second periodic test of the RBV Subsystem was performed on 10 November 1975. In Orbit 4068 the downlink filters were configured, and all RBV modes were set up. RBV operational tests were started in Orbit 4070 and continued through Orbit 4072. MSS imagery was transmitted simultaneously for comparison and evaluation. All operations were normal with no discernible effect on other spacecraft subsystems.

During Orbits 4082 and 4083 (11 November), and Orbits 4096 and 4097 (12 November) the RBV was operated over Brazil for use by that station. Again, all operations were normal.

Table 16-1 gives typical telemetry values for the RBV Subsystem during the test operations. Tables 16-2, 16-3, and 16-4 give telemetry values for Prepare, Hold, and Read modes of the three RBV cameras.

LS-2 16-1

Table 16-1. RBV Telemetry Values

	Function				C	rbits			
No.	Name	T/V Value	41	54	151	209	2371	3052	4072
14001	CCC Board Temp. (DgC)	N/A	19.939	19.65	19.72	20 58	20 27	19.41	20, 12
14002	CCC Pwr. Sup Temp (DgC)	N/A	21.047	20.52	20.65	21.90	21 46	20 61	21.12
14003	15 VDC Sup. (TMV)	N/A	3.950	3.92	3.75	3.89	3 92	3 92	3, 95
14004	+6V, -5.25 VDC Sup (TMV)	N/A	3.075	2.92	2.92	3.00	3 07	3.05	3, 05
14100}		0.98	NA	NA	NA	NA	0.70	0.70	0.70
14200 } *	VID Output V (TMV)	0.93	NA	1.05	1 16	1.30	1 23	F	1.11
14300)		1.06	NA	1.03	1.10	1 24	1 27	F	1, 25
14102)		3.75-4.02	3.950	3.85	3.85	3.86	3 81	3.83	3,74
14202 }*	Comb Align Cur. (TMV)	3.87-4 10	3.875	3.91	3.91	3 92	3 92	F	3.78
14302)		3.80-4.05	3.850	3.90	3.72	3.85	3.80	F	3.72
14103)		N/A	24.363	24.24	24.10	26.08	24 49	22 87	24.02
14203 }*	Elec Temp. (DgC)	N/A	20.387	19.84	19.97	22.16	22 40	20 01	20, 91
14303)		N/A	25.363	25.05	25.35	28.20	24 15	22, 22	23, 55
14104 )		N/A	23.363	23.44	23,55	25 68	24 13	22 16	23, 69
14204 >*	LV Pwr Sup T. (DgC)	N/A	18.834	18 14	18.29	20 61	20 87	18 20	19.34
14304 )	- ' -	N/A	26,023	25.36	25.66	28 28	24 12	22 30	23, 62
14105 )		3.92-4.07	3.950	4.00	3,82	3.95	3 94	3.98	3, 69
14205 }*	Defl. Pwr. Sup. +10 VDC (TMV)	3.95-4.10	3 950	3.97	3.80	3.93	3 92	Г	3.85
14305 )		3.95-4.07	4.000	4.00	4.00	4.00	3 95	F	4.00
14106		3.65-3.80	3.700	3.67	3,52	3.64	3 59	3.67	3,40
14206 }*	L V P.S. +6V, -6.3 VDC (TMV)	3.67-3.80	3.650	3.65	3.49	3.61	3 61	F	3,42
14306	, ,	3.65-3.77	3.725	3.70	3.70	3.71	3 66	r	3.70
14107 )		2.53	2.650	2.61	2.49	2.54	2 54	2 59	2.39
14207 *	Ther. Elec. Cur. (TMV)	2.43	2.500	2.49	2.37	2 42	2 44	F	2.31
14307		2.52	2.575	2 57	2,46	2.49	2 52	F	2.54
14108		1.80-3.50	2.550	2.43	2,44	2 49	2 48	2 55	2.36
14208 >*	Vid. Fil. Cur. (TMV)	2.55-2.75	2.400	2.40	2.30	2 37	2 34	F	2.25
14308	(4)	2.50-2.80	2.575	2.58	2.46	2.54	2 54	F	2.46
14110		2.95-3.20	3,025	2.98	2.98	2.98	2 95	2 95	2.90
14210 }*	Vid. Tgt. Volt (TMV)	3 15-3 45	3.050	2.86	2,86	2 93	2 93	F F	2.81
14310	,, - <b>0</b> ,, ,, ,	2.55-2.80	3, 225	2.63	2.51	2,60	2 56	F	2.51
14113		2,86	4.050	2,92	2.87	2 84	2 79	2 98	2, 31
14213 >*	Vert Def V (TMV)	3.09	4.275	3,15	3, 12	3.08	2 99		
14313		3.91	4.275	3.59	3 45	3.51	3 48	F F	3 18
14114		21 99	21.997	19.87	20 18	21 18	20 67	_	3,56
14214 *	Vid FPT (DgC)	21.00	21 059	20.55	20.64	21 56	21 14	19 92	20, 53
14314		22.66	22.398	20.55	20.85	21 89	21 14	20 60	21.03
14115	<u> </u>	24.17	20.940	21.04	21.47	23 23	22 41	20 37	20.96
14215 >*	Foc Coil T (DgC)	23 82	20.340	20.67	21.47	23 23	22 41	20 98	21.95
14315	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	24.47	21.940	22.25	22,66	24.53		20 63	21.55
~ #UAU /			21.540	44,40	42.00	44.03	23 08	21.72	22.67

^{* 141}XX refers to Camera 1

¹⁴²XX refers to Camera 2

¹⁴³XX refers to Camera 3

NA - Data not Available

F - Cameras 2 and 3 off Camera 1 only was operated

Table 16-2. Camera #1 (Blue) Telemetry (Values in TMV)

					Orbit				
Function No.	Function Name	Mode	T/V Value	054	151	209	2371	3052	4072
14101	Focus I	Hold Prep Read	0.66 1 71 2.83	0.65 1.68 2.80	0.65 1.68 2.85	0.67 1.74 2.85	0.70 1.75 2.90	0.63 1.67 *	0.68 1.73 2.85
14109	Grid V	Prep Read Hold	0.79 2.43 4.00	0.80 2.42 3.95	0.75 2.43 3.95	0.75 2.42 3.95	0.80 2.44 4.00	0.77 2.42 3.96	0.79 2.41 3.99
14111	Cath I	Hold Read Prep	0.38 0.84 3.03	0.38 0.83 3.05	0.38 0.83 3.00	0.38 0.83 3.04	0.40 0.85 3.10	0.35 0.82 3.01	0.37 0.83 3.02
14112 ,	Hor Def	Hold Prep Read	0.01 1 79 3 23	0.00 1.75 3.25	0.00 1.75 3.25	0.00 1.75 3 25	0.00 1.80 3.30	0.00 1.76 3.20	0.00 1.77 3.25
14120	+500 V	Prep Read	0.92 4.05	0.85 4.05	0.85 4.05	0 88 4.05	0.90 4.10	0.90 4.03	0,90 4,05

^{*}No Data due to slow TLM sample rate

Table 16-3. Camera #2 (Yellow) Telemetry (Values in TMV)

<u> </u>					Orbit			
Function No.	Function Name	Mode	T/V Value	054	151	209	2371	4072
14201	Focus I	Hold Prep Read	0.58 1.60 2.71	0.54 1.56 2.65	0.49 1.57 2.65	0.54 1.54 2.65	0.60 1.60 2.70	0.56 1.56 2.67
14209	Grid V	Prep Read Hold	0.83 2.25 4.13	0.75 2.25 4.05	0.82 2.25 4.05	0.81 2.25 4.09	0.85 2.30 4.10	0,79 2,20 4,12
14211	Cath I	Hold Read Prep	0.37 0.95 3.05	0.37 0.95 3.05	0.33 0.95 3.05	0.34 0.95 3.05	0.35 1.00 3.10	0.35 0.95 3.05
14212	Hor Def	Hold Prep Read	0.01 1.87 3.32	0.00 1.85 3.25	0.00 1.88 3.25	0.00 1.85 3.25	0.00 1.90 3.30	0.00 1.87 3.31
14220	÷500 V	Prep Read	1.14 4.29	1.15 4.25	1.15 4.25	1.15 4.25	1.20 4.30	1.14 4.27

Table 16-4. Camera #3 (Red) Telemetry (Values in TMV)

The skins	The street				Orbit		
Function No.	Function Name	Mode	054	151	209	2371	4072
14301	Focus I	Hold Prep Read	0.65 1.79 2.85	0. 65 1. 85 2. 85	0.71 1.84 2.92	0.70 1.83 2.90	0.70 1.83 2.91
14309	Grid V	Prep Read Hold	0.75 2.65 4.08	0.75 2.65 4.10	0.75 2.65 4.13	0.80 2.70 4.18	0.76 2.67 4.13
14311	Cath I	Hold Read Prep	0.39 0.54 3.25	0.39 0.54 3.25	0.39 0.54 3.25	0.40 0.55 3.30	0.40 0.55 3.22
14312	Hor Def	Hold Prep Read	0.00 2.05 3.35	0.00 2.05 3.35	0.00 2.05 3.41	0.00 2.10 3.45	0.00 2.06 3.41
14320	+500 V	Prep Read	1.15 4.25	1.15 4.25	1.15 4.25	1.20 4.30	1.15 4.27

# SECTION 17 MULTISPECTRAL SCANNER SUBSYSTEM LANDSAT-2

#### MULTISPECTRAL SCANNER SUBSYSTEM (MSS)

The MSS Subsystem has operated nominally in this period without incident. Figure 17-1 shows the number of scenes imaged at each geographic location this quarter, and Figure 17-2 shows images since launch.

In these maps, only those scenes received by U.S. ground stations are shown. Scenes transmitted to Canada, Brazil and Italy (32% of total) are not shown.

Table 17-1 shows typical telemetry values since launch. All are nominal. Table 17-2 shows the history of sensor response to a constant input radiance level. Each sensor is sampled at 5 radiance levels and all show essentially the same trends. Only one of these levels (the second highest) is listed in Table 17-2. Line length history is also shown in Table 17-2 and is nominal.

Recent processing of MSS film from earlier recordings show occasional unscheduled insertions of a single or double group of 4 black and 4 white words in all sensor data. Sometimes these anomalous inserts are mistaken for a Line Start Code and result in displacement of the video in an entire mirror sweep (6 lines on the processed image). A study of a sample of the known anomalies concludes that the data loss is random; is a very small percentage of the received data (e.g., 17 pixels out of every million); and is limited to the region of the South Atlantic magnetic anomaly. Similar effects are seen in retrospective examinations of early Landsat-1 MSS processed film. This effect is, therefore, not considered to be a problem at this time.

Sun calibrations, performed every two weeks, show nominal performance.

LS-2

Table 17-1. MSS Telemetry - Landsat-2

		*T.V.	1	<del></del>	<del></del>	Orbit		· <del></del> -	
Function	Name	Norm	27	1254	2500	3400	4241	4670	5091
15040	MUX -6 VDC (TMV)	3,92	4.05	4.07	4.04	4.07	4.05	4.07	4,07
15041	A/D SUPPLY (TMV)	5.74	5,95	5.95	5.95	5.95	5.95	5.95	5,95
42	AVERAGE DENSITY (TMV)	1.72	1.71	2,30	.2.39	2.17	1.86	2.04	1.95
43	FIBER OPTICS PLATE 1 TEMP (DGC)	22.30	18.13	18.4	20.41	21.23	18.60	20.67	21.75
44	FIBER OPTICS PLATE 2 TEMP (DGC)	22.30	17.87	18.1	18.86	19.75	16.73	19.11	20.20
45	MUX TEMP (DGC)	25.59	23.38	25.6	20.57	22.76	21.03	21.68	23.63
46	ELEC COVER TEMP (DGC)	23.09	20.25	21.3	21.40	22,44	18,19	21.71	22.96
47	PWR. SUP. TEMP. (DGC)	23.85	19.45	21.0	19.83	21.19	18.16	20.11	21.62
48	SCAN MIR REG. TEMP (DG )	23.44	18.30	18.0	18,29	20.18	17.33	19.26	21,13
49	SCAN MIR DRIVE ELEC. TEMP. (DGC)	24.34	18.96	19.6	18.49	20.53	17.43	19.36	21.42
15050	SCAN MIR DRIVE COVER TEMP. (DGC)	22.50	17.26	19.4	18,28	20.20	17.37	19.41	21.21
51	SCAN MIR TEMP (DGC)	21.87	17.26	17.9	18.09	19.71	17.26	19.08	20.89
52	ROT. SHUT HOUSING TEMP (DGC)	22.58	23, 26	18.4	18.91	19.80	16.72	19.14	20,28
53	SCAN MIR REG VOLT (TMV)	4.56	4.7	4.57	4.57	4.59	4.62	4.57	4,57
54	CAL LAMP CURRENT (TMV)	1.18	1.17	1.17	1,20	1.17	1.17	1, 17	1,20
55	BAND 1 15 VDC (TMV)	4.97	4.98	4,97	4.97	4.97	4.97	4.97	4.97
56	BAND 2 15 VDC (TMV)	5.00	5.00	5,00	5.00	5.00	5.00	5.00	5.00
57	BAND 3 15 VDC (TMV)	4.88	4.95	4.95	4.95	4.95	4.95	4.97	4.95
58	BAND 4 15 VDC (TMV)	4.83	5,00	5,00	5,00	5.00	5.00	5.00	5,00
59	TLM 15 VDC (TMV)	5.04	5.06	5.07	5.07	5.07	5.07	5.07	5.07
15060	+12 VDC +6 VDC (TMV)	4.92	5,03	5.02	5.02	5.02	5,02	5.02	5.02
61	LOGIC +5 VDC (TMV)	4.86	4.81	4.80	4.80	4.82	4.81	4.90	4.83
62	RECT. +19 VDC (TMV)	4.97	5.03	5.05	5,05	5.05	5,05	5.05	5.05
63	RECT19 VDC (TMV)	3.54	3.60	3.60	3,60	3.60	3.60	3.60	3.60
64	BAND 1 HVA (TMV)	4.95	4.95	4.95	4.95	4,95	4.95	4.95	4.95
65	BAND 1 HVB (TMV)	5.03	OFF	OFF	OFF	OFF	F	F	$\mathbf{F}$
66	BAND 2 HVA (TMV)	4.72	4.70	4.72	4.72	4.72	4.72	4.72	4.75
67	BAND 2 HVB (TMV)	4.70	OFF	OFF	OFF	OFF	F	F	F
68	BAND 3 HV A (TMV)	4.75	4.72	4.75	4.76	4.75	4.75	4.75	4.73
69	BAND 3 HVB (TMV)	4.65	OFF	OFF	OFF	OFF	F	F	F
15070	SHUT MOT. CONTR. INTEG (TMV)	2,49	2.60	2,57	2,60	2.60	2.60	2.60	2,60
15071	SCAN MIRROR DRIVE CLOCK (TMV)	1,93	2.0	2.00	2.00	2.00	2.01	2.00	2.00

^{*} Thermal Vacuum Test Data at 20°C

Table 17-2. MSS Response History - Landsat-2

### Quantum Level for Selected Word (0 = Black; 63 = White)

Band	Sensor	Launch	1, 2 & 3 Quarter	This Quarter	% Change Since Launch
	1	43	41	40	-8
]	2	41	40	39	-7
i .	3	46	43	43	-7
1	4 5	46	45	44	-4
	5	44	41	40	-9
	6	46	43	43	-7
	7	47	46	45	-4
	8	44	41	41	-7
2	9,	48	47	46	-4
"	10	50	48	48	-4
	11	48	48	47	-2
<u>L</u>	12	47	44	44	-6
*	13	42	41	40	<b>-</b> 5
	14	44	43	42	-5
3	15	47	46	47	0
1 °	16	47	45	46	-2
	17	48	46	46	-4
	18	46	44	45	-2
	19	25	25	25	0
	20	26	27	27	+4
4	21	32	32	32	0
=	22	29	30	30	+3
	23	32	33	33	+3
	24	28	28	28	0
	Line Length	3250	3249	3248	0.06

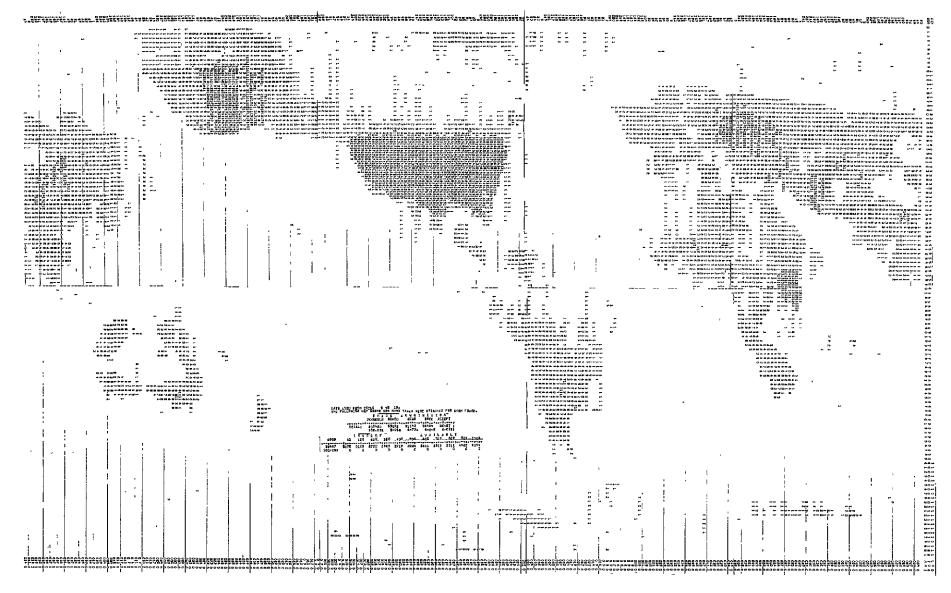


Figure 17-2. Computer Map of MSS Scenes Since Launch Landsat-2

#### DATA COLLECTION SUBSYSTEM

LANDSAT-2

#### DATA COLLECTION SYSTEM (DCS)

The DCS Subsystem performed nominally during this report period, continuing message collection at substantially the same rate.

The Alaska ground station commenced receiving DCS messages during this quarter, joining Greenbelt and Goldstone. During Orbit 4393 on 3 December 1975, the first messages were received at Alaska. No more messages were received until 8 December, when during Orbit 4457, regular reception was commenced. DCS messages are now being collected on 12 orbits of the 14-orbit day, rather than the previous 8-orbit cycle. This increased the number of messages received in the quarter by 26%, but severely reduced the statistic of messages per active orbit. Because of the geographical location of Alaska with respect to the present locations of DCP's, Alaska up to now receives only about 20% of the number of messages received by Greenbelt or Goldstone, while increasing the number of active orbits by 50%. Hence, the number for "Average messages per active Orbit" listed in Table 1-1 is reduced substantially. (Thus, in the prior three quarters, the average number of messages per orbit was 164; in this quarter, it was 139). The maximum number of platforms received in one day of this quarter was 110 on 14 January. The maximum number of messages received per orbit was 464 on Orbit 5005 on 16 January 1976.

There are 46 users in the data base, 246 DCP's have been shipped, with 231 in the data base.

Table 18-1 shows telemetry values since launch. All are nominal.

Table 18-1. DCS Telemetry Values

Func.		Orbits								
No.	Name	5	1253	2462	3410	4241	4670	5091		
16001	Receiver 1 Sig Strength (DBM)*	-123.34	-122.79	-124.81	-124,00	-122,66	-123.87	-122.02		
16002	Receiver 1 Temp (DGC)	22,54	24.13	24,20	24.39	23.55	23.98	24.37		
16003	Rec-1 Pwr Input Volt (VDC)	2.35	2.37	2,36	2,37	2,35	2.36	2,36		
16004	Receiver 2 Sig Volt (DBM)	F	F	${f F}$	${f F}$	F	${f F}$	F		
16005	Receiver 2 Temp (DGC)	$\mathbf{F}$	F	F	F	F	F	${f F}$		
16006	Receiver 2 Input Volt (VDC)	F	F	F	F	F	F	F		

^{*} This value is for a CW carrier only; it is not valid during DCS message reception F = Receiver 2 was OFF

Figure 18-1 shows the number of DCS messages per 18-day cycle at OCC, and the average number of DCP's active per cycle. Also shown is percentage of good messages for each cycle.

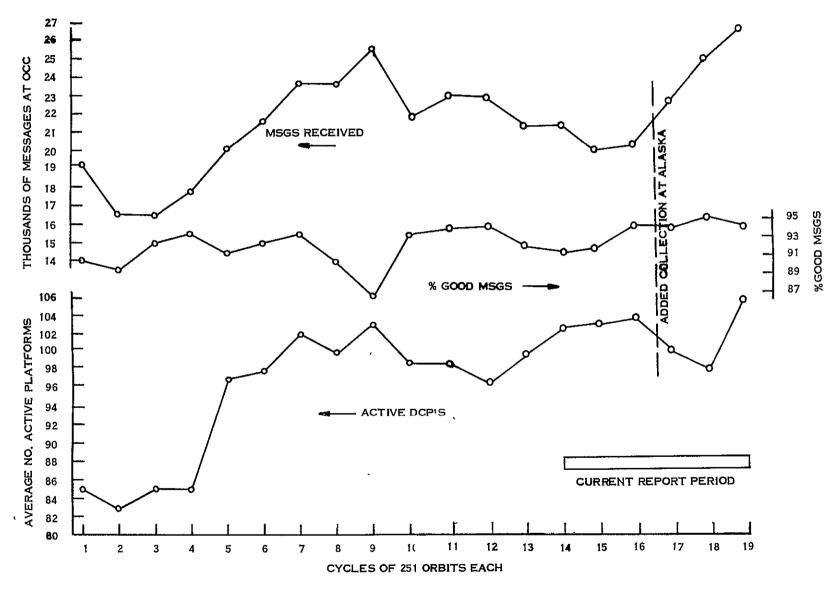


Figure 18-1. DCS Message History

#### APPENDIX A

LANDSAT-2 ANOMALY LIST

Landsat-2 Anomalies and Observations

		Anomanes and Obs	
Date	Anomaly/Observation	How Observed	Comments
Prelaunch	Forward Scanner Pressure Leak	Spacecraft Integration	Before launch pressure increased. After launch pressure decreased. No anticipated effect on Scanner or S/C mission.
Prelaunch	Defective TLM Functions 1264, 4002, 13200	Spacecraft Integration	Functions are temperatures which are non- critical. Sensors failed prior to launch. Mission unaffected.
3/8/75	Non-Landsat OCC authorized Un- encoded command 781, CIU Channel B Off, received by spacecraft from RF interference. Commands 782 or 786, switch comdecs, received at other times.	On-Line	Non-Landsat OCC Authorized Unencoded commands received in Orbit 619, 640, 743, 1575, 1700, 2605, 3164.
3/17/75	MMCA Pitch Flux Density TLM Drift	Off-Line	Telemetry decreased 5 counts and indicates increase flux density on charged magnet. Investigation underway. Probable sensor drift. No apparent effect on S/C performance.
4/5/75	WBVTR-1 Rewind Failure	On-Line	ECAM Rewind command to WBVTR-1 failed to execute in Orbit 1021. R/T commands failed to execute. Operation resumed Orbit 1476. Investigation continuing.
5/12/75	WBVTR-1 Failed to R/W	On-Line	See entry 4/5/75
5/15/75	WBVTR-1 Failed to R/W	On-Line	See entry 4/5/75
6/9/75	WBVTR-2 had short R/W	On-Line	WBVTR-2 started R/W but stopped pre- maturely. WBVTR (1 & 2) investigation still continuing while operation resumed.
7/2/75	WBVTR-1 had short R/W	On-Line	See entry 4/5/75 and 6/9/75.
8/3/75	WBVTR-1 data did not provide sync to ground station	On-Line	One WBVTR-1 head circuit failed to operate. 25% of data lost in data stream. Operation discontinued. Investigation committee formed.

#### APPENDIX B

LANDSAT-2 SPACECRAFT ORBIT REFERENCE TABLES

SPACECRAFT ORBIT REFERENCE TABLES

FROM JULY, 1975 THROUGH DECEMBER, 1976

ORBITS 2221 THROUGH 9890

FLIGHT DAY 160 THROUGH 709

## JUL/1975

	1 GMT	FI IGHT	SPACECRAFT I	REFFRENCE	REF	CYCLE
DATE	DAY		BRBITS	हम् हा १८	DAY	NO.
		160		154=167	12"	8-
1	1185			168=181	13 1	8
2	[ 183 ]	161	2235- 2248		1 14 1	- <del>8</del>
	T-184-		2543 - 53PS	182-195	,	
4	1 185		2263- 2276	194-209	15	8
5	186	<u> </u>	<del>- 2277 - 2290  </del>	210-553	16 1	8
6	187	) 165	2291- 2304	224-237	17	8
<del></del>	1 188	166	<del>2305+23</del> 18	54×4521	<del>г – 18 - г</del>	8
8	189	167 )	2319- 2732	1= 14	1 1	9
9	1 190	168	2333- 2446	15- 28	2 1	9
10	191	169	2347- 2360	29- 42	3 1	9
	1-192	<del></del>	<del>2361 - 2374  </del>	<del>- 470 5</del> 6	<del>, 4</del> T	- •
12	193	171	2375- 2388	57 <b>- 7</b> 0	J 5 1	9
13	19#	72	2389 - 2402	71="84	F	<del>9</del>
14	1 195	173	2403- 2416	85= 98	1 7 1	9
15	1-196		2417- 2430	999112	1	<del></del>
16	197	•	2431= 2444	117-126	1 <b>9</b> 1	9
- 17	T 198	•	2445- 2457	127=139	101	9
18	1 199	177	2458- 2471	140=153	1 11 /	9
19	1 500	<del>178</del>	2485-	154=167	<del>                                     </del>	<del>9</del>
20	201	179	2486- 2499	168=181	13 (	9
- 21	1 505		2500= 2513	182-195	14-1	9
22	203	181	2514- 2527	196=209	15	9
- 23	1 20#	182	2528 2541	210=223	161	<del>- 9</del>
24	205	183	2542- 2555	224-237	1 17 1	9
- 25	1-206-	184 1	<del>2556 - 2569 -</del>	23x=251	187	<del>9</del>
26	1 207	185	2570- 2583	1 = 14	1 1 1	10
-77	1 208	186	2584 - 2597	15= 28	2.1	10
28	1 503	187	2598- 2411	29- 42	3 1	10
79	1 210	188	2617= 2425	\$7# 55	4 1	10
20	1 211	189	2626- 2639	57= 70	1 5 1	10
- 11	1 212	190	2640 2653	71 = 84	6	10

LS-2

# LANDSAT-> AUG-1975

	GMT I	FI IGHT I	SPACECRAFT I	REFERENCE	I REF I	CYCLE
DATE			CRBITS I	BRBITS		NO
,	,					
	<del>213</del>	191	2654 2667 T	15+ 98	<del>1 7 1</del>	10
. 2	21#	192	2668- 2681	99-112	1 8 1	10
3	513	193	- 2652 - 2K95 1	117-126	1 9 1	iö-
	216	194	2696- 2708 1	127=139	10	10
5		195	7709- 2728     S779- 2728	140-153	1 11	
, <u> </u>	218	196	2723- 2736	154=167	12	10
	513	197	2737 2750 1	168-161	131	10
8	250	198	2751- 2764 1	182-195	1 14 1	10
1 <b>9</b>	,	199	2765- 2778	195-209	1 15 1	<del>10</del> -
; <del>;</del>	555	200	2779- 2792	210=223	1 16 1	10
	223	201	2793- 2805 1	274=237	1 17 1	10
1 12	224	505 1	2807= 2820 I	238=251	1 18 1	10
		,				
13	558	203	7821* 283*   2835* 2948	1 = 14 15 = 28	1 1 1	11
1 15	<del></del>	205 1	- 2849 - 2862   - 2849 - 2862	<del>5645</del>	1 <del>3</del> 1	<del>11</del>
•	•	205	2863- 2876	47= 56	1 4 1	11
16	558	,				
17	523	207	2877 - 2890 1	57= 70	5 1	11
18	) 530	208	2891 - 290 4 1	71 = 84	1 6 1	11
19	537	509	2905 - 291X !	N5 ♥ 98	77	11
70	535	210	2919- 2932	99-112	8	11
21	233	211	2933+ 2946 I	114-126	797	11
22	234	212	2947- 2959 1	127+139	1 10 1	11
P3	235	<del>- 213  </del>	<del>~ 2960~ 2973  </del>		<del>  11-</del> 1	
24	536	214 [	2974- 2987	154+167	1 12 1	11
25	237	215	2988 3001 I	16x=181	1-11-1	11.
26	538	216	3002- 3015 1	182-195	1 14 1	11
<del>) 77</del>	1-53 <del>3  </del>	<del>217  </del>	<del>- 3016-3029  </del>	194 <b>=</b> 209	<del> 15-+</del>	
1 28	S+0	: 218	3030- 3043 1	210-223	1 16 1	11
79	741	219	10444 3057 T	274=737	17 1	11
30	242    - <del>24</del> 3		3058= 3071   <del>3072= 3085  </del>	238=251 	18 ₁	11

B-3

#### SEP 1975

ŧ ,		FiliGHT		REFFRENCE	I REF I	CYCLE
UATE	DAY	DAY	BRBITS	BREITS	TOXY	₩.
	<del></del>	722		<del></del>	15-1	12
2	245	553	3100- 3113	29- 42	1 3 1	12
3	548	554	7114- 3127	# <b>7</b> = 56	1 4 1	12
<b>+</b>	247	552	1 141E -851F	57 <b>-</b> 70	f 5 i	12
5	748	559	7142° 3155	71= 84	1 6 1	15
6	543	227	3156- 3169	85 <b>=</b> 98	1 7 I	12
7			~~~ <u>~17</u> 0~~3184~;	445.15	T	15_
, 8	251	229	3184- 3197	117-126	1 9 1	12
		<u> </u>		127¥139	T 10 1	<u>15</u>
10	263	231	7211 - 3224	140=153	1 11 1	12
11	754	535	1225- 324K	154=167	1 17 1	12
12	255	l 533 i	7239• 3252 I	168=181	1 13 (	12
13	526	234		<del>182*</del> 195	T-14-T	15
14	257	235	3267- 3280	196-209	1 15	12
15	758	736	7281 - 3294 T		167	15
16	1 259 1	237	3295- 3308	224=237	i 17 i	12
+7	540		3309* 3472	23X=251	181	12
18	P61		1 9666 •6266	1 = 14	1 1	13
19	565		7337× 3350	15= 28	1 S	<del>13-</del> -
<b>&gt;</b> 0	543	241	7351- 3764	29- 42	1 3 1	13
71	P64"	545	3365- 3378	44= 56	T4T	13
22	1 542	243 1	3379- 3392	57+ 70	I 5 I	13
73	ZA6	544	7393° 3406	71 w 84	6 1	13
24	267	245	3407- 3420 I	25 <b>-</b> 98	7 i	13
<del></del>	P68-	<del>~~~ 246 ~  </del>	<del>34213*3+- </del>	99w112	<del> </del>	<del></del>
P6	269	- '	3435- 3448	113-126	9 (	13
77	270 1	~~~ <del>24</del> 8 T	3449-3461	127=139	10	13
28	271	249 1	3462= 3475	140=153	1 1t i	13
	272	<del> 250</del>	3476# 3489 T	154-167	<del>12  </del> -	13
20	273	251	7490= 3503 I	168-181	13	13

#### BCT, 1975

j l	GMT	FilGHT	SPACECRAFT	I REFFRENCE I	REF	CYCL
DATE	DAY	DAY	STERRE	TERRITE	TOAY	NB.
,						
•	274	<del>  -252  </del>	35044 3517	187-195	14	13
2	275	! 253 I	3518- 3531	1 196+209 1	15 (	13
3	278	254	3532= 3545	1 510+553 T	16	13
4	277	l <u>2</u> 55 i	3546- 3559	1 224+237 1	17 1	13
5	278	256	<del>3560* 357</del> 3	73X-251	18	13
6	279	257	3574- 3587	1 1 14 1	1 1	14
7	280	258 -		<del> </del>	2	14
A	185	259	3602- 3615	1 29- 42 1	3	14
9	585	260	3616- 3629	44 56	4	14
10	283	261	3630- 3643	57= 70 i	5 (	14
11	784	262	7644# 3A57	71 × 84 ;	6	14
12	285	263	3658- 3671	85- 98	7	14
13	286	264	3672* 3685	99=112	8	14
14	287	265	3686- 3699	1 113-126	9	14
15	- 288-	266	3700= 3712	127-139	10	14
16	888 F	1 267 1	3713- 3726	140+153 (	11	14
17	540	268	3727- 3740	154=167	12	* *
18	: <b>291</b>	769	<b>9741- 3754</b>	168=181	13 1	14
13	595	<del>  270  </del>	7755 - 3768	182-195	147	
20	1 293	271	3769- 3782	1 196=209	15	14
71	29#	272	3753- 3796	210-223	16	74
22	295	273	3797- 3810	224=237	17	14
23	<del>  296  </del>	274	3811=-3x24	123A=251!	18 1	14
24	297	275	3825- 3838	1 1= 14	1 1	15
75	<del>  598  </del>	<del>  27<u>6  </u></del>	<del>1839+-</del> 3852	<del>  5</del> ▼-28	2 1	
<b>76</b> (	799	277	3 <u>8</u> 53- 3866	1 29- 42 1	3 1	. –
27	300	<del>  278  </del>	3867- 3xX0	<del> <u>4</u>3•</del> <u>5</u> 61	4-1	15
28	1981	1 279 1	3881- 3894	1 57 <b>=</b> 70 1	5 (	15
- 59	302	<del>780  </del>	3895= 3908	71 = 84	5 1	15
30	303	281	3909- 3922	85- 98	7 1	15

LS-2 B-5

#### NBV - 1975

i	GMT	FITGHT	SRACECRAFT	REFFRENCE	REF	CYCLE
DATE	DAY	DAY	वस्टान्द	BRBITS	DAY	NB
*****	395	283	3937- 3950			
1 2	306	1 284 I		114-126	9 1	15
•	_	· <u> </u>	7951 - 3963	127=139	1 10 1	15
3	307		3964- 3977	140-153	1 11 1	15
, •	1 308	, ,	3978= 3991	154=167	1 12 1	15
5	30		3992- 4005	168-181	ा 🗓	15
1 6	1 310	1 288	4006- 4019	182=195	1 14 1	15
	7 311		#0 <u>20+ +033</u> -1	196=209	151	15
. 8	312		4034- 4047	210=223	16	15
, 9	1 313		4048- 4061	554-537	<del>  17  </del>	15
10	1 314	1 292 1	4062- 4075	238≈251	j 18 j	15
11	1 315	29 <b>3</b>	4076= 4089	7 = 14	1 1	16
12	316	294	4090- 4103	15- 28	1 2 1	16
13	1 317	295-1	4104- 4117	2명="42	13 .1	16
14	1 318	7 296	4118- 4131	43- 56	4 1	16
15	<del>; 319</del>	<del>  297  </del>	<del></del>	<b>ラフ=テロ・</b>	5	— <u>—</u> † 6
16	1 320	298	4146- 4159 1	71 w 84	6	16
17	1 321 1	79 <del>9  </del>	4160= 4173	85= 98	7	16
18	1 355 1	1 000	4174- 4187	99=112	8 (	16
19	1 323 1	301	<del>4188* 4201  </del>	113=126	<del>9</del> T	16
20	1 324	302	-4202- 4214 I	127-139	10 (	16
71	325 1	303	4215- 4228	140=153	11	16
25	326	304 i	4229- 4242	154-167	12	16
73-	1 327 I	305	4243- 4256	168=181	13	16
24	1 328	306	4257- 4270	182-195	14	16
25	329	307	4271= 4284	196=209	15 T	16-
26	1 330	308	4285- 4298	210+223	16	16
- 27 -	331	309	4299- 4312	224=237	17	16
28	382	310 i	4313- 4326	238-251	18	16
75	333	311	4327- 4340	1= 14 1		17
30	1 334 I	312	4341- 4354	15= 28 1	2 1	17

## DEC.1975

	GMT	Filight	SPACECRAFT	REFFRENCE	I REF 1	CYCLE
DATE	DAY	T- DAY	BRBITS	ERBITS	DAY	N8 •
1	335	313	4355= 436 <b>8</b>	24- 45	3	17
2	1 336	314	4369- 4382	43+ 56	1 4 1	17
3	337	315	4383= 4396	57+ 70	5 (	17
4	338	316	4397- 4410	71= 84	6 1	57
5	1 339	317	4411= 4424	85° 98	7-1	17
6	340	l 318 (	4425- 4438	99=112	( A )	17
<del>7</del>	341	319	4439- 4452	117-126	9 1	17
8	342	1 320	4453- 4465	127=139	10 I	17
	7 343	1321	4466 4479	140=153	<u></u>	-17
10	1 344	1 322 1	4480= 4493	154=167	12	17
<del></del>	345	323	4494- 4507	16X=[8]	13	17
12	346	324	4508- 4521	182=195	14	17
13	347	<del>325 i</del>	4622- 4535	196-209-		17
14	348	326	453h= 4549	210-223	16 i	17
15	309	327	455 <del>0-</del> 4567	224-237	17	17
16	350	328	4564- 4577	238-251	18	17
- 17	351	329	4578= 4591	7= 14	1	18
18	352	1 330 1	4592- 4605	15= 28	2	18
- 19-	353	331	4606-4619-	79- 47	3	<del>18</del> -
20	354	332	4620- 4633	47- 56	4	18
	385	333	4634- 4647	57= 70	5 7	18
22	356	1 334 i	4648- 4661	71 = 84	6 1	18
- 23 -	357	335	4662- 4475	#5= 98	7	18
24	358	336	4676= 4689	99=112	, , , , ,	18
<del>25</del>	359		- 4690× 4703-	113-126	<del></del>	<u>+8</u>
26	360	388 1	4704- 4716	127-139	10	18
<del>27</del> -	361	339	4717=-4730-	14n=153 ····		·· - <del>1</del> 8
28	362	340 i	4731- 4744	154=167	12	18
<del></del>	363	3+1	47+5- 4758	168¥181	13	<del>-18</del>
30	1 364	342	4759= 4772	182=195	14	18
-31-	365	3+2    3+3	47734786 <del> </del>		15-r	10 <del>18</del> -

LS-2

# LANDSAT »>

!	GMT	FIIGHT	SPACECRAFT	REFFRENCE	REF	CYCLE
DATE	DAY	DAY	TRATE	THREITS	DAY	N8.
*****		344	4787 - 4×00	7 2 TO = 223	r16 -	
۶	2	345	4801= 4814	224-237	17	1 18
3	3	346	4815- 4828	238-251	18	18
4	#	347	4829- 4842	1 - 14	1	19
5	5	348	4847- 4856	15= 28	7	19
6	6	1 349 1	4857 <b>-</b> 4870	29= 42	3 (	19
7	7	350	4871- 4884	43= 56	4	19
8 (	8	351	4885= 4898	1 57 <b>-</b> 70	5	19
9	-	352	4899- 4919	71 = 84	5	19
10	10		4913- 4926	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	' 7	19
11	11	354	4927- 4940	99=115	8	19
12 1	12		4941= 4954	113-126	9 (	19
13 (	13	356   357	4955- 4967 4968- 4981	127-139	11	19
15	15	• •	4900= 4901 4982= 4995	140=153   	- 12-1	19 <del>19-</del> -
16			4996= 5009	1 168=181		19
17	17		5010- 5023	182=195	13	7.7
18			5024- 5037	196=209	15	19
19	19	362-7	5038= 5h51		ta- 1	19-
20 1	20 I	363	5052- 5065 1	224=237	17 1	19
<del></del>	21	364	<del>5056=</del> _5 <del>079  </del>		— <del>+</del> я-¬	19-
22	55	365	5080= 5093	1 = 14	1 1	50
23	<del>- 23</del>	365	<u> </u>	128	5	50
24	24 (	367	5108- 5121	29- 42	3 1	50
<del>25  </del>	<del>- 25  </del>	368	5122× 5135	47- 56-1	4-1	- 50-
26 1	26	369	5136- 5149	57 <b>-</b> 70	5 I	20
<del>-27 1</del>	_ <del></del>	370 1	5150= 5163 I		6 1	50
28	28   <del>  29  </del>	371	5164- 5177	85= 98 I	7 1	50
<del>29  </del>	30	372 I	5178= 5191 T	99-112	8 1	50
30   <del>31  </del>	30   31	,	5192 <b>-</b> 5205   <del>5206- 5218  </del>	113-126   <del>127-139  </del>	9   <del>10- </del>	<del>50</del>

B-8

## LANDSAT=2 FEB.1976

1	GMT	FIIGHT	SPACECRAFT	REFFRENCE	REF	I CYCLE
DATE	TDAY	T DAY	TREST	FREITS	TOAY	NO.
					****	
1 3	1 35	375	9219 <del>- 5232</del>	1404153	1 11	L. 50
5 ا	1 33	376	5233- 5246	154=167	12	1 50
1 3	3*	377	5247- 5260	168=181	1 13	50
1 4	35	] 378	5261- 5274	182=195	1 14	1 50
5	36	379	5275- 5288	196=209	15	70
1 6	1 27	380	5289- 5302	210=223	1 16	50
7	7 78	381 1	F303- 5716	274-237	17	20
1 8	1 29	382	5317- 5330	238=251	18	20
9	1 40	383	7331 - 5744	7= 14	1 1	51
1 10	41	384 j	5345- 5358	t5= 28	1 5	21
1 15	1 42	385	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	29- 42	3	51
1 12	43	386	5373- 5386	47+ 56	1 4	21
13-	44	387	5387= 5400	57= 70	T-5	21
1 14	45	38E	5401- 5414	71 = 84	1 6	21
1 15	46	389	5415= 5428	प्रद- पृष्ठ	7	21
1 16	47	390	5429- 5442	99-112	) А	21
<del>                                     </del>	<del>1 48</del>	391	5443= 5456	113=126	19	21
18	49	392	5457- 5469	127+139	1 10	21
19	50	393	5470- 5483	140-153	1-11-	71
20	51	394 i	5484= 5497	154-167	1 12	21
<del>                                      </del>	1-62	395	5498× 5511	16X=181	T13	21
1 22	1 53	396	5512- 5525	182=195	1 14	21
73	54	397	5526= 5539	196=209	15	51
24	55	398 j	5540- 5553	210-223	16	21
<del>- 25</del>	156	<del> 399  </del>	- 5554+-5467	224=237	1	
26	F7	400	5568- 5581 I	238=251	1 18	21
<del>  - &gt;7</del>	158	401	5582= <del></del> 5595		† <b>†-</b> -	- 52
28	59	402 1	5596- 5609	15= 28	2	22
	60	403 1	5610* 5623 I	29* 42	3	- 52

LS-2 B-9

			LANDSATOR							
<del></del>	MAR # ( 976									
						· /				
1	I GMT I	FI IGHT I	GRACECRAFT	REFFRENCE	REF	CYCL				
TUATE	1 DAY 1	DAY	BRBITS	PRBITS	DAY	NB •				
				**********						
1	1 61	404	5624- 5637	47= 56	4	25				
i S	1 42 1	405	5638= 5451	1 57 <del>-</del> 70	5	55				
1 3	63	406	5657- 5665	71 = 84	5	52				
1 4	1 64 1	407	5666- 5479	85= 98	7 :	55				
5	65	408	5680- 5693	99=112	<del>  8</del>	72				
1 6	1 66 1	409	5694- 5707	113-126		55				
7 7 8	68	410	5708- 5720	127-139						
<del>                                     </del>	1 -69	411   412	5721= 5734 5735= 5748	140=153	11	55				
1 10	1 70 1	413	5749= 5762	154=167   168=181	12	55 55				
<del>                                     </del>	- 71	<del>- 41+</del>	5763+ 5776	1824195	15					
12	72	415	5777- 5790	196-209	15	: I				
1 13	73	416	5777- 5790   5791- 5804		<u>15</u>					
14	74	417	5805= 5818	224-237	17	55				
15	<del>i 75 i</del>	418	- 5819- 5832	238-251	18-	— 2 <del>2</del>				
1 16	76	419	5833- 5846	1 = 14	1					
1 17	77	420	5847# 5860 T	15= 28	- 2	- 23				
18	78	421	5861- 5974	29= 42	3	- 23				
1 19	79 1	422	5675 <del>≠_5</del> x88	# <b>₹</b> ¥ 56 1	4 1	73				
1 20	80 J	423	5889 <del>-</del> 5902	57 <b>=</b> 70	5 i	23				
71	1 81 1	424	5903- 5916	71= 84 ]	5	53				
1 22	1 85 1	425	5917- 5930	85= 98 I	7 1	53				
73	<del>1 83  </del>	<del>- 426  </del>	<del>- 5931= 5944  </del>	99=112-1	8	53				
24	1 84 [	427	5945- 5958 1	113-126 i	9 1	53				
75	<del>  85  </del>	428	<del></del>	127-139	10	53				
76	86	429	5972- 5985 1	140-153	11 1	23				
1	<del>  87  </del>	<del>*30  </del>	- 5986= 5999 1	154-167	127	- 53				
1 28 1 29	88	431	6000= 6013	168-181	13	23				
30	1 90	432   433	6014- 6027   6028- 6041	182-195   196-209	14 T	53				
1 31	, 90 ( <del>  91  </del>	<del>- 43+ -</del>  -	6053 + 6055     6055 + 6055	<u>510-553</u>	15   <del>- 16  </del>	<del>23</del>				

#### LANDSAT+2

#### APRAISTA

i	GMT :	FI IGHT 1	SPACECRAFT I	REFERENCE	REF	CYCL
DATE	DAY	DAY	BRBITS		DAY	
				*****		,
<u> </u>	92 1	<del>- 435 </del>	6056- 6069	224=237	17-17-	23
1 2	93 1	436	6070- 6083	238=251	18	53
3	9+ 1	437	6084+ 6097	1 - 14		24
4	1 95 I	438	6098= 6111	15- 28	1 2	24
5	96	439 i	6112- 6125	29= 42	3	24
i 6	i 97 i	440 i	6126- 6139	44- 56	. 4	24
7	98	441	6190- 6153	57= 7n	5	24
8	i 99 i	442	6154- 6167 1	71 - 84	6	24
9	1 100 1	443	6168= 6181	85- 98	<b>7</b>	24
1 10	101	444	6182- 6195	99-112	i 8 i	24
1 11	182	445	61969 6209 1	113-126	9 1	24
12	i 103 i	446	6210- 6222	127-139	i 10 i	24
13	104	<del> ++7 i</del>	6223×- 6236-1		r <u>11</u> -1	24
1 14	1 105 1	448	6237- 6250 1	154-167	1 12 i	24
15	106	<del>-++9 ;</del>	6251 - 6264	168-181-	. <u>1</u> 3-	<del>2</del> 4
1 16	107	450 i	6265- 6278	182=195	14 i	24
177	108	451 1	6279= 6292	196-209	15 1	24
1 18	109	452	6293- 6306	210=223	16 1	24
1-19	110	453	6307~ 6320	-224-237	i 17i	
20	111	454	6321- 6334	238=251	18 1	24
21	112	455 -i	6335= 6348	1= 14	,	- 25
i 22	113	456 į	6349- 6362	15= 28	į į	25
73	11+1	457	6363* 6376 T	29- 42	3 1	25
24	115	458	6377- 6390 i	43- 56	i 4 i	25
25	116	45 <del>9</del> 1	6391* 640* 1	57 <b>- 7</b> 0	- 5 i	25
76	117	460 i	6405- 6418	71 = 84	6	25
27	-118 h	<del>461  </del>	-6419+ 643P	85	<del>-</del> -	<del>25</del> -
89	119	462	6433- 6446	99-112	. 8 1	25
79	120	463	5#47* 5460 T	1134126	9 1	25
30	121	464	6461- 6473	127-139	10 i	25

LS-2

#### MAYJTAYA

1	GMT	FI IGHT	SPACECRAFT	REFFRENCE	I REF	CYCLE
DATE	I DAY	DAY	BRBITS	BRBITS	DAY	I N <del>0</del> ∙
	1 122	7465	6474- 6487	140-153	11	25
خ ا	123	i 466 i	6488- 6501	154-167	12	25
3	174	467		16X=181	13	25
1 4	1 125	1 468 1	6516- 6529	1 182-195	14	25
1 5	126	469	6530 6543	196-209	15	
1 6	1 127	1 470 1	6544- 6557	1 210-223	16	25
<del>, , , , , , , , , , , , , , , , , , , </del>	158	<del>                                     </del>	6556#_657 <u>1</u>	224-237	17	25
j 8	1 129	1 472 1	6572- 6585	238-251	18	25
<u>1</u>	130	473	6556- 6599	1 - 1 4	1 1	
1 10	131	1 474 1	E149 =0099	19- 28	1 5 .	
1 11	1.35	<del>+ 75    </del>	6614- 6627	54= 45	3	76
1 12	133	476	6628- 6641	47= 56	4	
1-13	1 13*	<del>                                     </del>	- 66 <del>12+ 6</del> 635	57= 70	5	26-
1 14	1 135	478	6656= 6669	71= 84	6	26
1 15	135	r 479 i	6670= 6683	85- 98	7	26
1 16	1 137	480	6684- 6697	99=112	, 8	26
1 77	1 138	481	658- 6711	113-126	1 10	59 59
1 18	1 139	482	6712- 6724	127-139		
1 19	1 140	1 483 1 1 484 1	6725= 6738 6739= 6752	140=153 154=167	11 12	26 26
1 20	1 1 4 1			• =		
7 71	142	# <b>85</b>	6753- 6766	182=181 *** 1 182=195	13 : 1 14 :	59
1 55	143	486   <del>  487  </del>	6767+ 6780   6781+ 679+	196=209	1 1 <del>5</del> 1	- 26 - 26
1 24	<del>  14#</del>   145	40/ )   488	6795= 6808	210=223	16	56
1 2 <del>5</del>	145   146	1 489   1 489	6809 6872	224=237	17	58
1 26	1 147	1 409 I	6823- 6836 (	238-251	18 1	26
<del>  20</del>	1 147 <del>1 148</del> -	<del>49</del> 1	6837****6850***		<u> </u>	<del></del>
28	· · · · _	1 492	6851= 6864	15= 28	. 2	27
1 29	150	. 49 <del>3 i</del>	6865= 6878	29- 42	3	27
1 30	151	1 494 1	6879- 6892	49 56	4	27
1 31	1 152	<del>  495  </del>	6893* 6906		<del></del>	27

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### LANDSAT+2 JUN-1976

1	1 GMT	FIGHT I	SPACECRAFT	REFFRENCE	REF	CYCLE
1			ORBITS		DAY	. – – .
DAIR	TOAY	t DAI I	OMBILE	i ekeria	1 1077	140.
	1 153	<del>,,</del>	<del>69076920</del>	<del>  710 84</del>	6	27
1 1	•			•	•	•
1 2	1 154	1 497 1	4921= 6934	85-98	7	27
1 3	1 155	•	6935+ 6948	1 99-115	8	27
1 4	1 156		6949- 6962	1 117-126	9	
5	7 157	<u> 500  </u>	6963= 6975	127-139	10	27
1 6	1 158	501	6976= 6989	140=153	11	1 2 <u>7</u>
<del>, , , , , , , , , , , , , , , , , , , </del>	<del>115</del> 9	<del>1 502 1</del>	<del>6990+-7</del> 003	<del>  154*167</del>	15-	
1 8	1 160	503	7004- 7017	168=181	1 13	27
9	161	504	7018- 7031	1X2-195	14	27
1 10	162	505	7032- 7045	1 94-209	1 15	27
111	1163	506	7046# 7n59	210-553	16	27
1 12	1 16#	507	7060- 7073	224=237	17 (	27
1 13	165	508	<del>70747087</del>	23x=251	18	27
14	1 166	i 509 i	7088= 7101	1 = 14	i 1 i	89
15	1 167	510 i	7102-7115	159-28	15	- 28
16	1 168	. 511 i	7116- 7129	1 29- 42	3	28
1 17	1 169	512	7130- 7143	। 44∎ 56	4	
18	1 170	513 i	7144= 7157	j 57 <b>+</b> 70	5	28
1 19	1 171	<del>. 514 i</del>	7158- 7171	719 84	, <u>, , , , , , , , , , , , , , , , , , </u>	- 28
i 20	1 172	1 515 i	7172- 7185	85= 98	. 7 i	28
71	1 173	516	7186- 7199	99-112		28
22	174	517	7200- 7213	117-126	9	28
23	1-175-	<del>i 518 i</del>	<del>7214 7226 </del>	127=139	10	28
24	1 176	519 i	7227- 7240	140-153	1 11	28
75	1 177	. 520 i	7241- 7254	154-167	17	
26	178	521	7255- 7268	168-181	13	28
27	179	<del>5</del> 22	7269=-7282		1 4	58-
28	180	•	7283- 7296	196=209	15 (	28
79-	1 181	<del>. 524 .</del>	7297- 7310	210=223	16	- 28
1 30	1 182		7311- 7324	224-237	17	58



#### JUL 1 976

l	I GMT	FIIGHT I	SPACECRAFT	I REFFRENCE	I REF !	CYCLE
DATE	I DAY	I DAY I	BRBITS	I BRBITS	T DAY	N6 •
<del>,                                    </del>	1 183	526	7325 <del>- 7</del> 448	238-251		
1 5	1 18#	1 527 1	7339- 7352	1 1 = 14	1 1 t	29
3		7 52 <b>8</b> 1	7353= 7366	15= 28	2	29
1 *	1 186	1 529	7367- 7380	1 29- 42	1 3 1	29
5	1 187	1 530 T 1 531 (	7381= 7394 7395= 7408	44 = 56 1 57 = 70	<del>  4  </del>   5	59 64
j 6	188 <del>  189  </del>	1 231 I	7409- 7422	/ 5/= /(/ <del>/ 71= 8</del> 4	) <u>5</u> [	29
1 / 1 8	1 190	i 533 i	7423- 7436	1 85= 98		29
1 B	1 191	1 534 I	7437= 7450	,	<del>'                                    </del>	
1 10	192	. 535 i	7451- 7464	113=126	9 1	29
11	193	536	7455- 7477	127=139	10	29
1 12	19#	i 537 i	7478- 7491	140-153	1 11 1	29
13	1 195	<del>  538  </del>	<del>7492- 75</del> 05-	<u>154-167</u>	12 1	59
1 14	1 196	j 539 j	7506- 7519	168=181	13 1	29
1 15	1 197	<del>1 540 1</del>	7520- 7533	182-195	141	<del></del>
16	1 198	1 541 1	7534- 7547	196-209	15 1	29
17	193	542	7548= 7561	210-223	16	- 59
1 18	1 500	1 543	7562 - 7575	224-237	17	29
19	701	544	7576= 7589		: 18 T	
1 20	1 505	1 545 I	7590= 7603   7604= 7617	! 1= 14  15= 28	! <b>1</b>   	30
1 22	1 203	546 T	7604= 7617 7618= 7631	1 29= 42	;	30
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1 205	548	7637= 7645	49= 56	4 1	30
24	1 506	549	7646- 7659	57= 70	1 5 i	30
25	<del>1 207 -</del>	550	7660 - 7673	71-84	6 1	30
26	208	551	7674- 7687	85 + 98	7 i	30
27	1 209	552	7688- 7701	99=112	r—s i	30
28	015	1 553 1	7702- 7715	113-126	9 1	30
79	1 211	1 554 1	7716- 7728	127-139	101	30
1 30	1 212	1 555 1	7729- 7742	140=153	1 11 1	30
<del>  21                                   </del>	1-213-	<del>  556  </del>	<del>- 7743- 77</del> 56-	<del>  1</del> 54#167	<del>15</del> -1	30

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#### AUG.1976

		FI IGHT !	SPACECRAFT	REFFRENCE	REF	CYCLE
DATE	I DAY	DAY	BRBITS	BRBITS	DAY	NO .
		5 <del>5</del> 7				
1	1.51+1		7757- 7770	1640181	137	30
2	1 515 1	558	7771- 7784	182+195	14 (	30
3	1 519 1	559	7785= 7798 T	196=209	15.1	30
4	1 517 1	560	7799- 7812	510=553	16	30
5	1 518 1	561	7813- 7826	224=237	17	30
6	1 219 1	562	7827- 7840	238=251	18	30
7	1 550 1	563	7841- 7854	1= 14	7-1	31
a	1 551 1	564	7855= 7868	15= 28	1 2 1	31
9	1 555 1	565	7869- 7882	29= 42	3 1	31
10	1 223 1	566	7883- 7896	47- 56	4 1	31
41	1 224 1	567	7897- 7910	57= 70	5 1	31
12	1 552 1	568 j	7911- 7924	71 = 84	1 6 1	31
13	1 526 1	569	7925+ 7938 T	*8 <del>5= 98</del>	7 7	31
4 4	1 227 1	570	7939- 7952	99=112	8 1	31
75	1 558 1	571	7953- 7966	113-126	9-1	31
16	1 553 1	572 i	7967• 7979	127-139	10 i	31
17	1 520 1	<del>- 573  </del>	7980 - 7993 T	140+153	11	31
† 8	1 231 1	574	7994= 8007	154=167	12 1	31
19-	1 535 1	575	8008° 8021		13	31
20	1 533 1	576 I	8022+ 8035	182-195	14	31
-21-	1-234-1	<del>- 577 -  </del>	8036 8049	1964209	15	31 -
22	; 235	578	8050- 8063	210-223	16	31
<del>-&gt;3</del>	<del>  236  </del>	<del>- 579  </del>	8064* 8077 T	224-237	17 1	31
24	1 237 1	580 I	8078- 8091	238-251	18	31
25	1 238 1	581	8092- 8105 T	1 = 14		32
26	239	582	8106- 8119 I	15= 28	ž i	32
27	1 240 1	<del> 583  </del>	8120 - 8133 -		<u>3</u>	35
28	1 241 1	584	8134- 8147	47- 56	4	32 1
-29	1 242 1	585	81489 8161 T	57= 70 1		32-
30	1 243 1	586	8162= 8175	71 = 84	6 1	32
31	1 254 1	<del>- 587 - j</del>	8189 1	<del>- 85</del> ₩ 98		32

LS-2 B-15

#### SEP. 1976

				****		
-		FI IGHT	SPACECRAFT		I REF I	
UATE	DAY	DAY	PYTEND	BRBITS	DAY	N8 •
****	****					
<b>Y</b>	1 545		8190= 8203 T	44 445	_1 \$	35
2	1 546 1	589 _L	8204- 8217 I	117-126	1 9 ;	35
3	1-5+2-1	590	X518- 8230	127-139	101	35
4	1 248 1	591 i	8231- 8244	140=153	1 11 1	35
3	749	592	X245- X258	154-167	1 12	32
6	1 250 1	593	A259- 8272 I	168-181	i 13 i	32
<del>-                                    </del>	1 251	594	8273- 8286	<u> </u>	1-14-1	<u>32</u>
8	1 252 1	595	8287- 8300 I	196=209	i 15 i	32
9	763	596	8301- 8314 I	210-223	1 16 1	35
10	25#	597	8315- 8328	224-237	17	35
-11-	255	598	X329- 8342	238-251	1 18 1	
12	256	599	8343- 8356	1= 14	1 1	33
13-	257 1	500 i	x357- x370	15= 28	T Z	<del>33</del>
94	258	601	8371- 8384	29- 42	3 1	33
15	259	<u>605 i</u>	8385- 8398 T	47- 56	<del>,                                    </del>	33
16	260 I	603	8399- 8412 1	57- 70	5 1	33
-17-	PA1 1	- 60 <del>4</del>	8413= 8426	71 w 84	<del>                                     </del>	33
18	1 262 1	605 1	8427- 8440 1	85= 98	7 1	33
13	1 263 I	<del>- 606  </del>	8441= 8454 T	99=112	<del>                                     </del>	33
20	264	607 1	8455- 8468	113-126	9 1	33
<del>- &gt;1</del>	265	- 608 i	8469= 8481		10	<del>-33</del>
22	266 1	609 1	8482- 8495	140=153	1 11 1	33 I
23	267	610	R#96# 8509 1	154-167	1 12 1	
24	268	611	A510+ 8523	168=181	1 13 1	33 33
25	249 1	612 -	- 2554 <del>- 8437  </del>	182+195	1 13 1	
26	270	613	8538= 8551	196-209	14     15	
77	771	614	8552= 8565	510-553 134-503		33
28	272 1	615	8566- 8579 I	- · · · · <del>-</del>	16 7	33
- 29	273	616		224-237	171	33 (
•	274 1		8550- 8593 I	23X=251	18 1	33
30		617	8594- 8607	1 = 14	1 1 1	34 (

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#### BCY. 1976

	I CMT I	FI IGHT I	SHACECRAFT !	REFERENCE	REF !	CYCLE
		DAY	ORBITS		TOAY	NB .
UATE	TDAY	ו ואט	UNU114 1			
				15= 28		34
	775	618		29- 42	1 3	34
5	1 276 1	619	8622- 8435	439 56	1 -4	34
- 3	1 277 1	620	- 8636- 8649	57• 70	:	
4	1 278 1	621	8650- 8663		•	
5	1 5/2	622	X654- 8677		5	
6	1 580 1	623	8678- 8691	85= 98	1 7	34
<del>7</del>	1 581 1	65#	8697- 8705	99=112	<del>  8</del>	34
8	1 282 1	625 I	8706- 8719	117-126	l ' <del>9</del>	34
9	1 583 1	626	8720= 8732	127=133	10	34
10	1 284 1	627	8733- 8746	140-153	11	34
-11	1 285 1	628	X747= 8760	154-167	17	•
12	286	629	8761- 8774	168=181	13	34
13	1 287 1	630	<del>- 8775- 8788-</del>	187=195	14	<del>1 3</del> 4
14	1 285 1	631	8789- 8802	196=209	ŀ <b>15</b>	34
15	1 289	632	8803- 8816	210=223	T-16	34
16	1 590 1	633	8817- 8830	224-237	1 17	ı 34
17	1 291	534	8831- 8844	248-251	18	34
18	292	635	8845= 8858	1 = 14	1 1	1 35
-19	793	636	#859= 8872	15= 28	1 5	35
20	1 29# 1	637	8873- 8886	29- 42	1 3	35
21	295-1	- 638		44= 56	T	35
25	296	639	8901- 8914	i 57= 70	1 5	1 35
<del>- 23</del> -	-1 297	6+0	#915 8928	71 - 84	6	1 35
24	398 1	641	8929- 8942	1 85= 98	1 7	1 35
<del>&gt;5-</del> -	- <del>295  </del>		- 8943- 8956-	99-112 -	<del>-i8</del>	35
26	1 300 1	643	8957- 8970	113-126	1 9	1 35
-	300	643		<del>  127=13</del> 9***	1-10-	<del>- 35</del>
<del>- 27 -</del>		645	8984-8997	1 140=153	1 11	35
78		646	8998= 9011	1-154-157	<del></del>	=
>9-	1 303 1	647	9012- 9025	1 168=181	1 13	35
30	1 7510 1		90126 9039		114	35
<del>21-</del>	<del>-   305  </del>	648	1966- 7037	F TUNATAD	, 44	,

#### LANDSATOR

#### NBV-1976

	*****					
	I GMT	FI IGHT	SPACECRAFT	REFFRENCE I	REF :	CYCLE
DATE	I DAY	DAY	BRETTS	BRATTS	DAY	NO.
	306	649	90+0- 9053	19:-209	15	35
Ş	307	650	9054- 9067	210-223	16	
3	308	651	9068- 9081	2245237	17	35
4	309	652	9082- 9095	238-251	18	35
5	310	653	9095- 9109	1-14		36
6	1 311	654	9110= 9123	15- 28	2 1	36
	312	655	<del>9124=-9137</del>	<del></del>	- 3	36
Я	1 313	656	9138- 9151	44- 56	4	36
9	31#	657	9155- 9165	57= 70 1	5 1	36
10	J 315	658	9166- 9179	71= 84	6 1	
11	1 316 I	659	9180= 9193	85= 98 [	7	36
12	1 317 1	660 1	9194- 9207 1	99=112	8 (	36
43	1 318	661	9208- 9221	117=176	<u></u>	36
14	1 319 1		9227- 9274	127-139	10 1	36
15	1-320-1		9235- 9248	T#n=153	<u>1</u>	36
16	1 321 1	664	9249- 9262	154=167	15 1	36
77	1.355	- 666	9263= 9276	168-181	131	36
18	1 323 1	646	9277- 9290	182-195 I	14 1	36
19-	1 32# 1	567	9291- 9304	196-209 T	15 1	
50	1 355 1	668	9305- 9318 1	210+223 1	16 i	36
21	376 1		9319- 9332	224=237	17 1	36
22	1 327 1	670	9333- 9346	238-251	18 ı	36
73	328	671	9347= 9460	1-14	1	37
24	1 379 1	672	9361- 9774	15= 28	2 1	37
75	1 <del>-330-1</del>	673	-9375+ 9488	34= 45 T		37
26	371	674	9389- 9402	47- 56	4 1	37
27 28	332     333	675  676 ∣	9403- 9416   9417- 9430	57- 70	5 1	37
-	•			71= 84	<del>6</del> I	37
23	33# 1	677	9431- 9444	×5 ± 98 1	77	37
30	335	678	9445= 9458 1	99-112	8 1	37

#### DEC. 1976

	I GMT	FIZGHT I	SPACECRAFT I	REFFRENCE	I REF I	CYCLE
DATE			BRBITS 1	BRBITS		
				040112		ING •
	326	679	9459- 9472	113-126	9	37 -
ż	327	680	9473- 9485	127=139	1 10 1	37
3	1 336 T	681	9456- 9499	1404153	1 10 1	37
	1 339	682	9500= 9513	154=167	12	37
	340	683	9514- 9527	158*(81	1 17 1	<del>37</del> -
6	1 341	684	9528- 9541	182=195	1 14 1	37
<del></del>	342	685	9542= 9555	196=209	1 15 1	<del>3</del> 7
á	1 343	686 I	9556- 9569	510-553	: 15 : 16 :	
<u> </u>	( 344	687				37
10	1 345	688	9570= 9583   9584= 9597	224-237	17	37
11/ -11	; 345   <del>; 346  </del>	669		238+251	18 1	37
12	1 347 1		9598= 9611	1 4	1 1	38
		690	9612- 9425	15= 28	1 2 1	38
13	1 348	691	9626- 9639	793-42	3-1	38
		692	9640- 9653	43 • 56	1 4 1	38
15	350	693	9654* 9667	57» 7 <u>0</u>	i	38_
16	1 351 1	694	9668- 9681 1		161	38
17	1 352 1	695	9682- 9695	<u>85= 98</u>	7	.38
18	1 353	696	9696- 9709	99-112	1 8 1	38
19	1 35+ 1	6 <del>97  </del>	9710- 9723 I	113-126-	г <del>9-</del> т	38
20	355	69 <b>8</b>	9724- 9736	127=139	10	38
71	1 350	699	9737- 9750 1	14n=153 7	<u>1</u>	38
25	1 357 1	700	9751- 9764	154-167	12	38
73	1 348 1	701 1	<del>~ 9765= 9778</del> ~ [		<u>13</u>	38
24	1 359 1	702	9779= 9792	182-195	14 1	38
<del></del>	1 360	703	<del>- 9793= 9яла  </del>			38
76	1 361 1	70 <del>4</del>	9807- 9820	210=223	16	8E
27	368	705	7851= 9834 T	224#237 7	r <b>17</b>	38
28	1 363 1	796 i	9835= 9848	238-251	18	38
- 29	<del>  36#  </del>	<del>- 707  </del>	<del>- 9849= 9862-1</del>	1 = 14	1	39
20	1 365 1	708 I	9863- 9876	15= 28 1	2 1	39
-21	360	<del>709</del>	9877- 9890 1	<del>29</del> 4-42	3	<del>39</del>

B-19/20

#### APPENDIX C

LANDSAT-2 DOCUMENTS ISSUED THIS REPORT PERIOD

#### APPENDIX C

#### LANDSAT-2 DOCUMENTS ISSUED THIS REPORT PERIOD

No.	Document No.	Title and Date
1	1N23-ERTS-165	WBVTR-2 of Landsat-2; Second Rewind Dropout Anomaly, dated 10/28/75
2	1N23-ERTS-166	Second Periodic Test of RBV in Landsat-2, dated 11/12/75
3	1N23-ERTS-167	Probable Incipient Malfunction of MSS on Landsat-2, dated 11/18/75
4	1N23-ERTS-168	WEVTR-1 in Landsat-2; Attempt to Dislodge Possible Particle in K-1 Relay, dated 1/9/76
5	1N23-ERTS-169	Landsat-2 MSS Line Start Anomaly Investigation; Reference GSFC Malfunction Report #D04940, dated 1/19/76



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